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# (S)-1-Ferrocenyl-3-hydroxy-3-phenylpropan-1-one

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Key indicators: single-crystal X-ray study; T = 296 K; mean  $\sigma$ (C–C) = 0.005 Å; R factor = 0.031; wR factor = 0.066; data-to-parameter ratio = 13.6.

In the title compound,  $[Fe(C_5H_5)(C_{14}H_{13}O_2)]$ , the dihedral angle between the phenyl ring and the unsubstituted cyclopetadienyl ring is 85.0 (2)° while that between the phenyl ring and the substituted cyclopetadienyl ring is 83.6 (2)°. The dihedral angle between the two cyclopenta-1,3-diene rings of the ferrocene unit is 2.2 (2)°. The molecules are stabilized by intermolecular  $O-H\cdots O$  hydrogen-bonding interaction within the crystal lattice.

### **Related literature**

For the preparation, see: Patti & Pedotti (2006*a*); Hashiguchi *et al.* (1995). For use of the title compound in the preparation of chiral diols, see: Patti & Pedotti (2006*b*) and of phosphine ligands, see: Zhang *et al.* (2007).



### **Experimental**

a = 10.0609 (14)  Å
b = 10.6054 (15)  Å
c = 14.335 (2) Å

 $V = 1529.5 (4) \text{ Å}^3$ Z = 4Mo *K*\alpha radiation

## Data collection

Bruker APEXII CCD diffractometer Absorption correction: multi-scan (*SADABS*; Bruker, 2005)  $T_{\rm min} = 0.728, T_{\rm max} = 0.840$ 

#### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.031$   $wR(F^2) = 0.066$  S = 1.062721 reflections 200 parameters H-atom parameters constrained  $\mu = 0.99 \text{ mm}^{-1}$  T = 296 K $0.34 \times 0.28 \times 0.18 \text{ mm}$ 

metal-organic compounds

7586 measured reflections 2721 independent reflections 2424 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.034$ 

 $\begin{array}{l} \Delta \rho_{max} = 0.19 \mbox{ e } \mbox{\AA}^{-3} \\ \Delta \rho_{min} = -0.22 \mbox{ e } \mbox{\AA}^{-3} \\ \mbox{Absolute structure: Flack (1983),} \\ 1146 \mbox{ Friedel pairs} \\ \mbox{Flack parameter: } -0.004 \mbox{ (19)} \end{array}$ 

# Table 1

Hydrogen-bond geometry (Å, °).

$D-\mathrm{H}\cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdot \cdot \cdot A$	$D - H \cdots A$
$O1-H1\cdots O2^i$	0.82	2.04	2.841 (3)	166
Symmetry code: (i)	$x + \frac{1}{2}, -y + \frac{3}{2}, -z$	ζ.		

Data collection: *APEX2* (Bruker, 2008); cell refinement: *SAINT* (Bruker, 2008); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *Mercury* (Macrae *et al.*, 2006) and *ORTEP-3* (Farrugia, 1997).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: PB2052).

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# supporting information

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# (S)-1-Ferrocenyl-3-hydroxy-3-phenylpropan-1-one

# **Ping-An Wang**

# S1. Comment

The title compound, (*S*)-1-ferrocenyl-3-phenyl-3-hydroxypropane- 1-one, was obtained from the catalytic asymmetric transfer hydrogenation of 1-ferrocenyl-3-phenyl-1,3-dione with the mixed solution of Et<sub>3</sub>N and HCOOH by using Noyori's catalyst (Hashiguchi *et al.* 1995) and it was used for the preparation of chiral diols (Patti *et al.* 2006b) and phosphine ligands (Zhang *et al.* 2007).

In the title compound,  $C_{19}H_{18}FeO_2$ , the dihedral angle between the phenyl ring and the plane defined by the cyclopetadienyl ring (C15, C16, C17,C18 and C19) is 85.0°. However, the dihedral angle between the phenyl ring and the plane defined by the second Cp ring (C10, C11, C12, C13 and C14) is 83.6°. The dihedral angle between the two cyclopenta-1,3-diene rings of the ferrocene moiety is 2.21°. The packing of molecules is stabilized by intermolecular O—H···O hydrogen bonds.

# S2. Experimental

A mixture of  $[RuCl_2(</>p-cymene)]_2$  (20.0 mg, 0.030 mmol) and (1</>S,2</>S)-[</>N-(tosyl)- 1,2-diphenylethylendiamine](22.5 mg, 0.061 mmol) in 2-propanol (1.0 cm<sup>3</sup>) was heated at 80°C for 30 min under argon, then the solvent wasremoved under vacuum. the mixed solution of Et<sub>3</sub>N and HCOOH (1.5 cm<sup>3</sup>) and 1-ferrocenyl-3-phenyl- 1,3-dione (0.34 g,1.2 mmol) were added to the Ru-complex and the mixture stirred at 50°C while monitoring the reaction progress by thinlayer chromatography. After 1.0 h, the solution was diluted with water (3.0 cm<sup>3</sup>) and extracted with ethyl acetate (2×,20.0 cm<sup>3</sup>). The organic layer was washed with brine (2×, 10.0 cm<sup>3</sup>), dried over Na<sub>2</sub>SO<sub>4</sub> and taken to dryness undervacuum. The residue was purified on silica gel column to give the title compound (0.31 g, 92% yield), and also produced(1</>S,3</>S)-1-ferrocenyl-3-phenyl- 1,3-dihydroxypropane (11.6 mg, 3.5% yield). The melting point and thespectroscopic data of the title compound were consisted with the reported literature (Patti & Pedotti, 2006a).

# S3. Refinement

All H atoms were placed in calculated positions and refined as riding, with C—H = 0.93–0.98Å and with  $U_{iso}(H) = 1.2U_{eq}(C)$ ; with  $U_{iso}(H) = 1.5U_{eq}(O)$ .



# Figure 1

The molecular structure of the title compound, showing the atom-labelling scheme. Displacement ellipsoids are drawn at the 50% probability level. Hydrogen atoms are drawn as spheres of arbitrary radius.

## (S)-1-Ferrocenyl-3-hydroxy-3-phenylpropan-1-one

Crystal data

 $[Fe(C_5H_5)(C_{14}H_{13}O_2)]$   $M_r = 334.18$ Orthorhombic,  $P2_12_12_1$ Hall symbol: P 2ac 2ab a = 10.0609 (14) Å b = 10.6054 (15) Å c = 14.335 (2) Å  $V = 1529.5 (4) Å^3$ Z = 4

## Data collection

Bruker APEXII CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator  $\varphi$  and  $\omega$  scans Absorption correction: multi-scan (*SADABS*; Bruker, 2005)  $T_{\min} = 0.728, T_{\max} = 0.840$ 

## Refinement

Refinement on  $F^2$ Least-squares matrix: full  $R[F^2 > 2\sigma(F^2)] = 0.031$  $wR(F^2) = 0.066$ S = 1.06 F(000) = 696  $D_x = 1.451 \text{ Mg m}^{-3}$ Mo K\alpha radiation, \lambda = 0.71073 \mathbf{A} Cell parameters from 2427 reflections  $\theta = 2.5-23.9^{\circ}$   $\mu = 0.99 \text{ mm}^{-1}$  T = 296 KBlock, orange-red  $0.34 \times 0.28 \times 0.18 \text{ mm}$ 

7586 measured reflections 2721 independent reflections 2424 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.034$  $\theta_{max} = 25.1^{\circ}, \ \theta_{min} = 2.4^{\circ}$  $h = -8 \rightarrow 12$  $k = -12 \rightarrow 12$  $l = -17 \rightarrow 14$ 

2721 reflections200 parameters0 restraintsPrimary atom site location: structure-invariant direct methods

Secondary atom site location: difference Fourier	$(\Delta/\sigma)_{\rm max} < 0.001$
map	$\Delta \rho_{\rm max} = 0.19 \text{ e}  \text{\AA}^{-3}$
Hydrogen site location: inferred from	$\Delta \rho_{\rm min} = -0.22  \mathrm{e}  \mathrm{\AA}^{-3}$
neighbouring sites	Absolute structure: Flack (1983), 1146 Friedel
H-atom parameters constrained	pairs
$w = 1/[\sigma^2(F_o^2) + (0.0253P)^2]$	Absolute structure parameter: -0.004 (19)
where $P = (F_0^2 + 2F_c^2)/3$	- · · · · ·

# Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\hat{A}^2)$ 

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$
Fe1	0.11375 (4)	0.33401 (4)	0.18512 (2)	0.03633 (12)
O1	0.57703 (19)	0.63931 (19)	0.04641 (14)	0.0539 (6)
H1	0.6135	0.7011	0.0234	0.081*
O2	0.1578 (2)	0.62907 (17)	0.03540 (14)	0.0533 (6)
C1	0.4265 (3)	0.6868 (3)	0.2293 (2)	0.0549 (8)
H1A	0.4579	0.6046	0.2348	0.066*
C2	0.4006 (4)	0.7564 (4)	0.3096 (2)	0.0698 (10)
H2	0.4136	0.7208	0.3682	0.084*
C3	0.3556 (4)	0.8786 (4)	0.3014 (3)	0.0771 (12)
Н3	0.3384	0.9258	0.3548	0.092*
C4	0.3361 (4)	0.9309 (4)	0.2153 (3)	0.0760 (12)
H4	0.3062	1.0136	0.2100	0.091*
C5	0.3611 (3)	0.8600 (3)	0.1359 (2)	0.0572 (9)
H5	0.3471	0.8956	0.0774	0.069*
C6	0.4066 (3)	0.7371 (3)	0.14234 (18)	0.0394 (7)
C7	0.4371 (3)	0.6624 (3)	0.05389 (18)	0.0420 (6)
H7	0.4081	0.7114	-0.0004	0.050*
C8	0.3721 (3)	0.5344 (2)	0.05076 (18)	0.0405 (6)
H8A	0.4048	0.4901	-0.0038	0.049*
H8B	0.4005	0.4871	0.1052	0.049*
C9	0.2226 (3)	0.5330 (3)	0.04789 (17)	0.0382 (7)
C10	0.1570 (3)	0.4105 (3)	0.05858 (18)	0.0364 (7)
C11	0.2179 (3)	0.2888 (3)	0.06855 (18)	0.0397 (7)
H11	0.3134	0.2712	0.0657	0.048*
C12	0.1172 (4)	0.1992 (3)	0.08209 (17)	0.0472 (8)
H12	0.1309	0.1086	0.0918	0.057*
C13	-0.0068 (4)	0.2617 (3)	0.08331 (19)	0.0510 (9)
H13	-0.0936	0.2220	0.0930	0.061*
C14	0.0165 (3)	0.3913 (3)	0.06844 (19)	0.0460 (8)

H14	-0.0517	0.4572	0.0656	0.055*	
C15	0.0302 (4)	0.4278 (4)	0.2937 (2)	0.0614 (11)	
H15	-0.0459	0.4851	0.2894	0.074*	
C16	0.0229 (4)	0.2989 (4)	0.3087 (2)	0.0697 (12)	
H16	-0.0583	0.2494	0.3181	0.084*	
C17	0.1545 (5)	0.2528 (4)	0.3103 (2)	0.0751 (13)	
H17	0.1818	0.1652	0.3208	0.090*	
C18	0.2385 (3)	0.3553 (4)	0.2957 (2)	0.0682 (11)	
H18	0.3358	0.3520	0.2932	0.082*	
C19	0.1618 (4)	0.4624 (4)	0.2855 (2)	0.0570 (9)	
H19	0.1950	0.5480	0.2746	0.068*	

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
Fe1	0.0403 (2)	0.0419 (2)	0.02675 (18)	-0.0006 (2)	0.00075 (19)	-0.00136 (19)
01	0.0498 (13)	0.0496 (14)	0.0624 (13)	-0.0068 (10)	0.0158 (10)	0.0073 (11)
O2	0.0576 (14)	0.0395 (12)	0.0629 (14)	0.0074 (11)	-0.0070 (11)	0.0096 (10)
C1	0.061 (2)	0.056 (2)	0.0474 (17)	-0.0109 (18)	-0.0026 (15)	0.0007 (17)
C2	0.067 (2)	0.098 (3)	0.0443 (19)	-0.024 (2)	-0.005 (2)	-0.002 (2)
C3	0.053 (2)	0.104 (3)	0.074 (3)	-0.011 (2)	0.004 (2)	-0.044 (2)
C4	0.063 (2)	0.065 (2)	0.100 (3)	0.009 (2)	-0.016 (2)	-0.036 (2)
C5	0.058 (2)	0.052 (2)	0.061 (2)	0.0040 (18)	-0.0118 (17)	-0.0081 (16)
C6	0.0406 (18)	0.0392 (15)	0.0385 (15)	-0.0068 (14)	-0.0006 (13)	-0.0025 (12)
C7	0.0494 (17)	0.0373 (15)	0.0392 (14)	0.0004 (15)	0.0046 (13)	0.0062 (15)
C8	0.0461 (17)	0.0339 (14)	0.0414 (15)	-0.0008 (15)	0.0053 (15)	-0.0015 (12)
C9	0.0529 (18)	0.0401 (17)	0.0215 (13)	0.0033 (15)	-0.0007 (13)	-0.0018 (12)
C10	0.0486 (19)	0.0374 (15)	0.0233 (14)	-0.0020 (14)	-0.0010 (13)	0.0013 (12)
C11	0.0526 (19)	0.0377 (17)	0.0289 (15)	0.0038 (15)	0.0048 (14)	-0.0011 (12)
C12	0.074 (2)	0.0366 (15)	0.0312 (14)	-0.0089 (19)	0.0015 (16)	-0.0028 (11)
C13	0.061 (2)	0.057 (2)	0.0347 (18)	-0.0235 (18)	-0.0100 (16)	0.0012 (15)
C14	0.0437 (18)	0.061 (2)	0.0331 (17)	-0.0048 (16)	-0.0093 (15)	0.0033 (15)
C15	0.062 (2)	0.082 (3)	0.040 (2)	0.022 (2)	0.0048 (17)	-0.0185 (18)
C16	0.079 (3)	0.098 (3)	0.0317 (17)	-0.039 (2)	0.018 (2)	-0.007 (2)
C17	0.140 (4)	0.059 (2)	0.0259 (17)	0.028 (3)	-0.006 (2)	0.0069 (18)
C18	0.054 (2)	0.121 (4)	0.0298 (18)	0.008 (2)	-0.0092 (14)	-0.011 (2)
C19	0.072 (2)	0.062 (2)	0.0368 (18)	-0.010 (2)	-0.0026 (15)	-0.0132 (15)

Geometric parameters (Å, °)

Fe1—C16	2.028 (3)	С7—С8	1.508 (4)	
Fe1—C15	2.029 (3)	C7—H7	0.9800	
Fe1—C11	2.030 (3)	C8—C9	1.504 (4)	
Fe1—C14	2.031 (3)	C8—H8A	0.9700	
Fe1—C17	2.032 (3)	C8—H8B	0.9700	
Fe1—C10	2.034 (3)	C9—C10	1.466 (4)	
Fe1—C18	2.034 (3)	C10—C14	1.435 (4)	
Fe1—C19	2.038 (3)	C10—C11	1.436 (4)	

Fe1—C13	2.047 (3)	C11—C12	1.402 (4)
Fe1—C12	2.056 (3)	C11—H11	0.9800
01—C7	1.433 (3)	C12—C13	1.413 (5)
01—H1	0.8200	C12—H12	0.9800
О2—С9	1.223 (3)	C13—C14	1.410 (4)
C1-C6	1 371 (4)	C13—H13	0.9800
C1 - C2	1.371(1) 1 392 (4)	C14—H14	0.9800
C1—H1A	0.9300	C15-C19	1 379 (5)
$C^2$ $C^3$	1 377 (5)	C15 $C16$	1.375(5)
C2 U2	1.377(3)	C15_H15	1.580 (5)
$C_2$ — $I_1$ 2	0.9300	C15 $-115$	1.412(5)
$C_3 = U_2$	1.508 (5)		1.412(3)
С3—Н3	0.9300	C10—H10	0.9800
C4—C5	1.388 (4)		1.393 (5)
С4—Н4	0.9300	C1/—H17	0.9800
C5—C6	1.385 (4)	C18—C19	1.381 (5)
С5—Н5	0.9300	C18—H18	0.9800
C6—C7	1.526 (4)	C19—H19	0.9800
C16—Fe1—C15	39.94 (15)	C9—C8—C7	116.3 (2)
C16—Fe1—C11	155.28 (15)	С9—С8—Н8А	108.2
C15—Fe1—C11	163.96 (14)	C7—C8—H8A	108.2
C16—Fe1—C14	123.86 (16)	C9—C8—H8B	108.2
C15—Fe1— $C14$	106 59 (13)	C7 - C8 - H8B	108.2
C11—Fe1— $C14$	68 99 (13)	H8A - C8 - H8B	107.4
C16—Fe1— $C17$	40.70 (16)	$0^{2}-0^{2}-0^{10}$	107.4 120.9(3)
C15 Fe1 $C17$	40.70 (10) 67 20 (15)	$O_2 = C_2 = C_1 O_2$	120.9(3) 122.0(3)
C13 - Fc1 - C17	171.29(13)	$C_{2} = C_{3} = C_{3}$	122.0(3)
C11—Fe1— $C17$	121.31(14) 162.04(16)	C10 - C9 - C8	117.1(2)
C14—FeI— $C17$	162.04 (16)	C14 $C10$ $C11$	100.5(3)
C16—Fe1—C10	101.55 (15)	C14-C10-C9	125.5 (5)
CI5—FeI—CI0	125.25 (14)	C11_C10_C9	127.9 (3)
CII—Fel—Cl0	41.39 (10)	C14—C10—Fel	69.21 (17)
C14—Fe1—C10	41.34 (12)	C11—C10—Fel	69.15 (16)
C17—Fe1—C10	155.97 (17)	C9—C10—Fe1	122.89 (19)
C16—Fe1—C18	67.55 (15)	C12—C11—C10	108.3 (3)
C15—Fe1—C18	66.67 (15)	C12—C11—Fe1	70.94 (16)
C11—Fe1—C18	110.42 (14)	C10-C11-Fe1	69.46 (16)
C14—Fe1—C18	154.93 (16)	C12—C11—H11	125.8
C17—Fe1—C18	40.05 (15)	C10-C11-H11	125.8
C10-Fe1-C18	121.24 (14)	Fe1—C11—H11	125.8
C16—Fe1—C19	67.24 (14)	C11—C12—C13	108.8 (3)
C15—Fe1—C19	39.62 (13)	C11—C12—Fe1	68.93 (15)
C11—Fe1—C19	128.06 (13)	C13—C12—Fe1	69.50 (17)
C14—Fe1—C19	119.70 (14)	C11—C12—H12	125.6
C17—Fe1—C19	67.18 (15)	C13—C12—H12	125.6
C10—Fe1—C19	108.20 (13)	Fe1—C12—H12	125.6
C18—Fe1—C19	39.65 (14)	C14-C13-C12	108.0(3)
C16—Fe1— $C13$	106 68 (14)	C14—C13—Fe1	69 16 (19)
C15—Fe1—C13	119.02 (15)	C12-C13-Fe1	70 21 (18)
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C11—Fe1—C13	68.29 (12)	C14—C13—H13	126.0
C14—Fe1—C13	40.47 (11)	С12—С13—Н13	126.0
C17—Fe1—C13	126.19 (16)	Fe1—C13—H13	126.0
C10—Fe1—C13	68.90 (12)	C13—C14—C10	108.4 (3)
C18—Fe1—C13	164 30 (16)	C13—C14—Fe1	70 37 (19)
C19—Fe1—C13	153 36 (15)	C10-C14-Fe1	69 45 (17)
C16—Fe1— $C12$	120.49(13)	$C_{13}$ $C_{14}$ $H_{14}$	125.8
$C_{10} = 101 = C_{12}$	120.49(15) 154.01(15)	$C_{10}$ $C_{14}$ $H_{14}$	125.8
C13 - Fe1 - C12	134.01(13)		125.8
CII - FeI - CI2	40.13 (11)	FeI—CI4—HI4	125.8
CI4—FeI—CI2	6/.96 (13)		109.1 (4)
C17—Fel—C12	109.65 (14)	C19—C15—Fel	70.6 (2)
C10—Fe1—C12	68.47 (11)	C16—C15—Fe1	70.0 (2)
C18—Fe1—C12	128.76 (15)	C19—C15—H15	125.5
C19—Fe1—C12	165.30 (15)	C16—C15—H15	125.5
C13—Fe1—C12	40.29 (14)	Fe1—C15—H15	125.5
С7—О1—Н1	109.5	C15—C16—C17	107.1 (3)
C6—C1—C2	121.2 (3)	C15-C16-Fe1	70.1 (2)
C6—C1—H1A	119.4	C17—C16—Fe1	69.8 (2)
C2—C1—H1A	119.4	C15—C16—H16	126.4
C3—C2—C1	119.4 (3)	С17—С16—Н16	126.4
$C_3 - C_2 - H_2$	120.3	Fe1—C16—H16	126.4
C1 - C2 - H2	120.3	$C_{18}$ $C_{17}$ $C_{16}$	107.3(3)
$C_1 C_2 C_2$	120.3	$C_{18}$ $C_{17}$ $E_{21}$	70.0(2)
$C_{4} = C_{3} = C_{2}$	120.4 (5)	$C_{16} = C_{17} = F_{c1}$	70.0(2)
$C_4 = C_3 = H_3$	119.8	C10 - C17 - Fe1	09.3(2)
C2—C3—H3	119.8	C16_C17_H17	120.4
C3—C4—C5	119.7 (3)	С16—С17—Н17	126.4
C3—C4—H4	120.2	Fe1—C17—H17	126.4
C5—C4—H4	120.2	C19—C18—C17	108.6 (3)
C6—C5—C4	121.0 (3)	C19—C18—Fe1	70.34 (18)
С6—С5—Н5	119.5	C17—C18—Fe1	69.9 (2)
C4—C5—H5	119.5	C19—C18—H18	125.7
C1—C6—C5	118.4 (3)	C17—C18—H18	125.7
C1—C6—C7	121.6 (3)	Fe1-C18-H18	125.7
C5—C6—C7	120.0 (2)	C15—C19—C18	108.0 (4)
O1—C7—C8	105.7 (2)	C15—C19—Fe1	69.8 (2)
01	110.4 (2)	C18—C19—Fe1	70.01 (19)
C8-C7-C6	113.9 (2)	$C_{15} - C_{19} - H_{19}$	126.0
01_C7_H7	108.9	C18 - C19 - H19	126.0
	108.0	Fal C10 H10	126.0
$C_{6}$ $C_{7}$ $H_{7}$	108.9	101-019-1119	120.0
С0—С/—Н/	108.9		
C( C1 C2 C2	0.9 (5)		11(2(2)
$C_0 - C_1 - C_2 - C_3$	-0.8(3)	C9-C10-C14-Fel	-116.3 (3)
C1—C2—C3—C4	0.2 (6)	C16—Fe1—C14—C13	-/5.3 (3)
C2—C3—C4—C5	0.4 (6)	C15—Fe1—C14—C13	-115.5 (2)
C3—C4—C5—C6	-0.5 (5)	C11—Fe1—C14—C13	80.8 (2)
C2-C1-C6-C5	0.7 (5)	C17—Fe1—C14—C13	-48.3 (6)
C2—C1—C6—C7	178.8 (3)	C10—Fe1—C14—C13	119.5 (3)
C4—C5—C6—C1	-0.1 (5)	C18—Fe1—C14—C13	174.3 (3)

C4—C5—C6—C7	-178.2(3)	C19—Fe1—C14—C13	-156.5(2)
C1—C6—C7—O1	-65.9 (4)	C12—Fe1—C14—C13	37.5 (2)
C5—C6—C7—O1	112.2 (3)	C16—Fe1—C14—C10	165.20 (19)
C1—C6—C7—C8	52.7 (4)	C15—Fe1—C14—C10	125.0 (2)
C5—C6—C7—C8	-129.2(3)	C11—Fe1—C14—C10	-38.73(18)
01 - C7 - C8 - C9	-1742(2)	C17—Fe1—C14—C10	-167.8(4)
C6-C7-C8-C9	64 5 (3)	C18—Fe1—C14—C10	54 8 (4)
C7 - C8 - C9 - O2	101(4)	C19 - Fe1 - C14 - C10	84.0 (2)
C7 - C8 - C9 - C10	-1713(2)	$C_{13}$ $E_{e1}$ $C_{14}$ $C_{10}$	-1195(3)
$0^{2}-0^{9}-0^{10}-0^{14}$	-89(4)	C12 - Fe1 - C14 - C10	-820(2)
$C_{2} = C_{2} = C_{10} = C_{14}$	(4)	$C_{12}$ $C_{14}$ $C_{15}$ $C_{10}$	110.8(4)
$C_{3} = C_{3} = C_{10} = C_{14}$	172.3(3) 176.2(2)	$C_{11} = C_{12} = C_{13} = C_{13}$	-45.4 (6)
02 - 09 - 010 - 011	170.5(5)	C14  Fe1  C15  C19	-43.4(0)
$C_{8} = C_{9} = C_{10} = C_{11}$	-2.3(4)	C14—FeI—C15—C19	-110.8(2)
02-09-010-Fel	-95.6 (3)	C17—FeI—C15—C19	81.1 (3)
C8—C9—C10—Fel	85.8 (3)	C10—Fe1—C15—C19	-75.3(3)
C16—Fe1—C10—C14	-42.1 (5)	C18—Fe1—C15—C19	37.5 (2)
C15—Fe1—C10—C14	-74.1 (2)	C13—Fe1—C15—C19	-158.9 (2)
C11—Fe1—C10—C14	118.0 (3)	C12—Fe1—C15—C19	169.6 (3)
C17—Fe1—C10—C14	170.8 (3)	C11—Fe1—C15—C16	-165.2 (4)
C18—Fe1—C10—C14	-156.1 (2)	C14—Fe1—C15—C16	123.4 (3)
C19—Fe1—C10—C14	-114.6 (2)	C17—Fe1—C15—C16	-38.7 (2)
C13—Fe1—C10—C14	37.26 (19)	C10—Fe1—C15—C16	164.9 (2)
C12—Fe1—C10—C14	80.7 (2)	C18—Fe1—C15—C16	-82.4 (3)
C16—Fe1—C10—C11	-160.1 (4)	C19—Fe1—C15—C16	-119.8 (4)
C15—Fe1—C10—C11	168.0 (2)	C13—Fe1—C15—C16	81.3 (3)
C14—Fe1—C10—C11	-118.0(3)	C12—Fe1—C15—C16	49.8 (4)
C17—Fe1—C10—C11	52.9 (4)	C19—C15—C16—C17	0.4 (5)
C18—Fe1—C10—C11	85.9 (2)	Fe1—C15—C16—C17	60.3 (3)
C19—Fe1—C10—C11	127.47 (19)	C19—C15—C16—Fe1	-59.9 (3)
C13—Fe1—C10—C11	-80.69(19)	C11—Fe1—C16—C15	170.3 (3)
C12—Fe1—C10—C11	-37.30(18)	C14—Fe1—C16—C15	-74.6(3)
$C_{16}$ Fe1 $-C_{10}$ C9	77 5 (5)	C17—Fe1—C16—C15	117.8(3)
$C_{15}$ = $F_{e1}$ = $C_{10}$ = $C_{9}$	45.5(3)	C10—Fe1—C16—C15	-424(5)
$C_{11}$ $E_{e1}$ $C_{10}$ $C_{9}$	-1225(3)	C18 - Fe1 - C16 - C15	80.0 (3)
$C_{14}$ Ee1 $C_{10}$ $C_{9}$	122.5(3)	$C_{10}$ Fe1 $C_{16}$ $C_{15}$	36.9(2)
C17 - Fe1 - C10 - C9	-69.6(4)	$C_{13}$ $E_{e1}$ $C_{16}$ $C_{15}$	-1155(2)
C18 = C10 = C9	-36.6(3)	$C_{13}$ $C_{14}$ $C_{16}$ $C_{15}$ $C_{15}$	-157.1(2)
$C_{10} = F_{c1} = C_{10} = C_{9}$	50.0(3)	$C_{12}$ $C_{10}$ $C_{13}$ $C_{15}$ $C_{15}$ $C_{15}$ $C_{15}$ $C_{17}$ $C_{$	137.1(2)
C19 - Fe1 - C10 - C9	5.0(5)	C13 - Fe1 - C10 - C17	-117.8(3)
C13 - Fe1 - C10 - C9	150.8 (5)	CII - FeI - CIO - CI7	52.5 (4) 1(7 ( (2)
C12—FeI—C10—C9	-159.8 (3)	C14—FeI— $C16$ — $C17$	167.6 (2)
C14—C10—C11—C12	1.1 (3)	C10—Fe1—C16—C17	-160.2 (4)
C9—C10—C11—C12	1/6.7 (3)	C18—FeI—C16—C17	-37.8 (2)
Fe1—C10—C11—C12	60.56 (18)	C19—Fe1—C16—C17	-80.9 (2)
C14—C10—C11—Fe1	-59.4 (2)	C13—Fe1—C16—C17	126.7 (2)
C9—C10—C11—Fe1	116.1 (3)	C12—Fe1—C16—C17	85.0 (3)
C16—Fe1—C11—C12	46.0 (4)	C15—C16—C17—C18	-0.3 (5)
C15—Fe1—C11—C12	-157.1 (5)	Fe1-C16-C17-C18	60.1 (3)
C14—Fe1—C11—C12	-80.3(2)	C15-C16-C17-Fe1	-60.5 (3)

C17—Fe1—C11—C12	83.4 (3)	C16—Fe1—C17—C18	-118.2 (3)
C10—Fe1—C11—C12	-119.0(2)	C15—Fe1—C17—C18	-80.2 (2)
C18—Fe1—C11—C12	126.5 (2)	C11—Fe1—C17—C18	84.7 (2)
C19—Fe1—C11—C12	167.8 (2)	C14—Fe1—C17—C18	-153.5 (4)
C13—Fe1—C11—C12	-36.72 (19)	C10—Fe1—C17—C18	46.5 (4)
C16—Fe1—C11—C10	165.0 (3)	C19—Fe1—C17—C18	-37.1(2)
C15—Fe1—C11—C10	-38.1(6)	C13—Fe1—C17—C18	169.5 (2)
C14—Fe1—C11—C10	38.68 (18)	C12—Fe1—C17—C18	127.5(2)
$C_{17}$ —Fe1—C11—C10	-157.6(2)	C15—Fe1— $C17$ — $C16$	380(2)
$C_{18}$ Fe1 $-C_{11}$ $-C_{10}$	-1145(2)	C11 - Fe1 - C17 - C16	-1571(2)
C19—Fe1— $C11$ — $C10$	-732(2)	C14—Fe1— $C17$ — $C16$	-353(6)
$C_{13}$ $F_{e1}$ $C_{11}$ $C_{10}$	82 28 (19)	C10 - Fe1 - C17 - C16	164.7(3)
$C_{12}$ Fe1 $C_{11}$ $C_{10}$	1100(2)	$C_{10} = 10^{-1} C_{17} = C_{10}$	104.7(3) 118.2(3)
$C_{12}$ $C_{11}$ $C_{12}$ $C_{13}$	-1.5(3)	$C_{10} = Fe_1 = C_17 = C_{10}$	110.2(3)
$E_{10}$ $C_{11}$ $C_{12}$ $C_{13}$	1.5 (5) 58 18 (10)	C13 = Fe1 = C17 = C16	-722(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	50 (2 (10)	C13 - Fe1 - C17 - C10	-72.2(3)
C10-C11-C12-Fel	-59.05(19)	C12 - FeI - C17 - C10	-114.3(2)
C16—FeI— $C12$ — $C11$	-159.55 (19)	C16 - C17 - C18 - C19	0.2 (4)
CI5—FeI—CI2—CII	165.8 (3)	FeI-CI/CI8CI9	59.9 (2)
C14—Fel—C12—C11	83.1 (2)	C16—C17—C18—Fel	-59.8 (3)
C17—Fe1—C12—C11	-115.9 (2)	C16—Fe1—C18—C19	-80.9 (2)
C10—Fe1—C12—C11	38.44 (16)	C15—Fe1—C18—C19	-37.4 (2)
C18—Fe1—C12—C11	-75.0 (2)	C11—Fe1—C18—C19	125.6 (2)
C19—Fe1—C12—C11	-41.2 (5)	C14—Fe1—C18—C19	41.7 (4)
C13—Fe1—C12—C11	120.8 (2)	C17—Fe1—C18—C19	-119.4 (3)
C16—Fe1—C12—C13	79.7 (2)	C10—Fe1—C18—C19	80.8 (2)
C15—Fe1—C12—C13	45.0 (4)	C13—Fe1—C18—C19	-152.1 (5)
C11—Fe1—C12—C13	-120.8 (2)	C12—Fe1—C18—C19	167.19 (19)
C14—Fe1—C12—C13	-37.68 (18)	C16—Fe1—C18—C17	38.4 (2)
C17—Fe1—C12—C13	123.3 (2)	C15—Fe1—C18—C17	81.9 (2)
C10—Fe1—C12—C13	-82.36 (19)	C11—Fe1—C18—C17	-115.1 (2)
C18—Fe1—C12—C13	164.2 (2)	C14—Fe1—C18—C17	161.1 (3)
C19—Fe1—C12—C13	-161.9(5)	C10—Fe1—C18—C17	-159.8 (2)
C11—C12—C13—C14	1.2 (3)	C19—Fe1—C18—C17	119.4 (3)
Fe1—C12—C13—C14	59.0 (2)	C13—Fe1—C18—C17	-32.8(6)
C11—C12—C13—Fe1	-57.84 (18)	C12—Fe1—C18—C17	-73.4(3)
C16—Fe1—C13—C14	123.0 (2)	C16—C15—C19—C18	-0.3(4)
C15—Fe1—C13—C14	81.5 (2)	Fe1—C15—C19—C18	-59.8(2)
C11—Fe1—C13—C14	-82.6(2)	C16-C15-C19-Fe1	59.6 (3)
$C_{17}$ —Fe1—C13—C14	163.4(2)	C17 - C18 - C19 - C15	0.0(4)
$C_{10}$ Fe1 $C_{13}$ $C_{14}$	-380(2)	Fe1-C18-C19-C15	597(2)
$C_{18}$ Fe1 $C_{13}$ $C_{14}$	-1710(4)	C17 - C18 - C19 - Fe1	-59.7(2)
C19—Fe1—C13—C14	50 7 (4)	C16 = Fe1 = C19 = C15	-37.2(2)
$C_{12}$ Fe1— $C_{13}$ — $C_{14}$	-1192(3)	$C_{11}$ Fe1 $C_{19}$ $C_{15}$	165.5(2)
$C16_Fe1_C13_C12$	-117.2(3)	C14—Fe1—C19—C15	80.0(2)
$C_{15} = F_{e1} = C_{13} = C_{12}$	-150.25(10)	$C_{17} = C_{19} = C_{19} = C_{15}$	-815(2)
$C_{13}$ $C_{13}$ $C_{13}$ $C_{13}$ $C_{12}$ $C_{12}$ $C_{12}$ $C_{12}$ $C_{12}$ $C_{12}$ $C_{12}$ $C_{13}$ $C$	36.58(16)	$C_{17}$ $-r_{C1}$ $-C_{17}$ $-C_{15}$ $C_{10}$ $C_{15}$ $C_{10}$ $C_{15}$	1227(3)
C11 = 101 = C13 = C12 $C14 = E_{0}1 = C13 = C12$	110.2(2)	$C_{10}$ $C_{10}$ $C_{10}$ $C_{10}$ $C_{10}$ $C_{10}$ $C_{15}$	123.7(2) -1180(2)
$C_{17} = C_{17} = C$	-774(3)	$C_{10}$ $-r_{c1}$ $-C_{19}$ $-C_{13}$	110.9(3)
$U_1 - U_1 $	-//.4(Z)	UI3-FEI-UI3-UI3	44./(4)

C10—Fe1—C13—C12	81.19 (18)	C12—Fe1—C19—C15	-161.9 (4)	
C18—Fe1—C13—C12	-51.8 (6)	C16—Fe1—C19—C18	81.8 (2)	
C19—Fe1—C13—C12	169.9 (3)	C15—Fe1—C19—C18	118.9 (3)	
C12—C13—C14—C10	-0.5 (4)	C11—Fe1—C19—C18	-75.5 (3)	
Fe1-C13-C14-C10	59.2 (2)	C14—Fe1—C19—C18	-161.1 (2)	
C12-C13-C14-Fe1	-59.7 (2)	C17—Fe1—C19—C18	37.5 (2)	
C11—C10—C14—C13	-0.4 (4)	C10—Fe1—C19—C18	-117.3 (2)	
C9-C10-C14-C13	-176.1 (2)	C13—Fe1—C19—C18	163.6 (3)	
Fe1-C10-C14-C13	-59.8 (2)	C12—Fe1—C19—C18	-42.9 (6)	
C11—C10—C14—Fe1	59.4 (2)			

Hydrogen-bond geometry (Å, °)

D—H···A	<i>D</i> —Н	H···A	$D \cdots A$	D—H···A
01—H1…O2 <sup>i</sup>	0.82	2.04	2.841 (3)	166

Symmetry code: (i) x+1/2, -y+3/2, -z.