

4-Diphenylphosphanyl-8-methyl-1,5-naphthyridine

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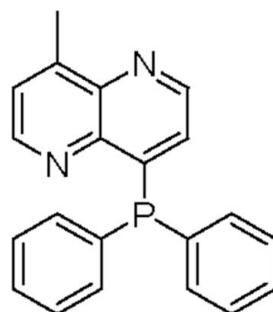
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Key indicators: single-crystal X-ray study; $T = 293\text{ K}$; mean $\sigma(\text{C}-\text{C}) = 0.004\text{ \AA}$; R factor = 0.050; wR factor = 0.155; data-to-parameter ratio = 14.9.

In the title compound, $C_{21}H_{17}N_2P$, the dihedral angles between the 1,5-naphthyridine ring system (r.m.s. deviation = 0.005 \AA) and the phenyl rings are $89.18(8)$ and $77.39(8)^\circ$. The phenyl rings are almost perpendicular, making a dihedral angle of $88.12(8)^\circ$. The only possible intermolecular interaction is a very weak aromatic $\pi-\pi$ stacking interaction [centroid–centroid separation = $3.898(2)\text{ \AA}$].

Related literature

For further synthetic details and background to the role of the title compound as an intermediate in the synthesis of OLED materials, see: Chen *et al.* (2012).



Experimental

Crystal data

$C_{21}H_{17}N_2P$
 $M_r = 328.34$
Triclinic, $P\bar{1}$
 $a = 7.2320(14)\text{ \AA}$
 $b = 7.4470(15)\text{ \AA}$
 $c = 16.780(3)\text{ \AA}$
 $\alpha = 99.78(3)^\circ$
 $\beta = 93.35(3)^\circ$

$\gamma = 98.58(3)^\circ$
 $V = 877.4(3)\text{ \AA}^3$
 $Z = 2$
Mo $K\alpha$ radiation
 $\mu = 0.16\text{ mm}^{-1}$
 $T = 293\text{ K}$
 $0.30 \times 0.20 \times 0.10\text{ mm}$

Data collection

Enraf–Nonius CAD-4
diffractometer
Absorption correction: ψ scan
(North *et al.*, 1968)
 $T_{\min} = 0.954$, $T_{\max} = 0.984$
3500 measured reflections

3224 independent reflections
2285 reflections with $I > 2\sigma(I)$
 $R_{\text{int}} = 0.023$
3 standard reflections every 200
reflections
intensity decay: 1%

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.050$
 $wR(F^2) = 0.155$
 $S = 1.00$
3224 reflections

217 parameters
H-atom parameters constrained
 $\Delta\rho_{\max} = 0.17\text{ e \AA}^{-3}$
 $\Delta\rho_{\min} = -0.23\text{ e \AA}^{-3}$

Data collection: *CAD-4 EXPRESS* (Enraf–Nonius, 1994); cell refinement: *CAD-4 EXPRESS*; data reduction: *XCAD4* (Harms & Wocadlo, 1995); program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXTL*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HB7082).

References

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Enraf–Nonius (1994). *CAD-4 EXPRESS*. Enraf–Nonius, Delft, The Netherlands.
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supporting information

Acta Cryst. (2013). E69, o928 [doi:10.1107/S1600536813013196]

4-Diphenylphosphanyl-8-methyl-1,5-naphthyridine

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S1. Comment

The title compound, (I), is an intermediate for manufacturing OLED materials (Chen *et al.*, 2012). We now report its crystal structure (Fig. 1).

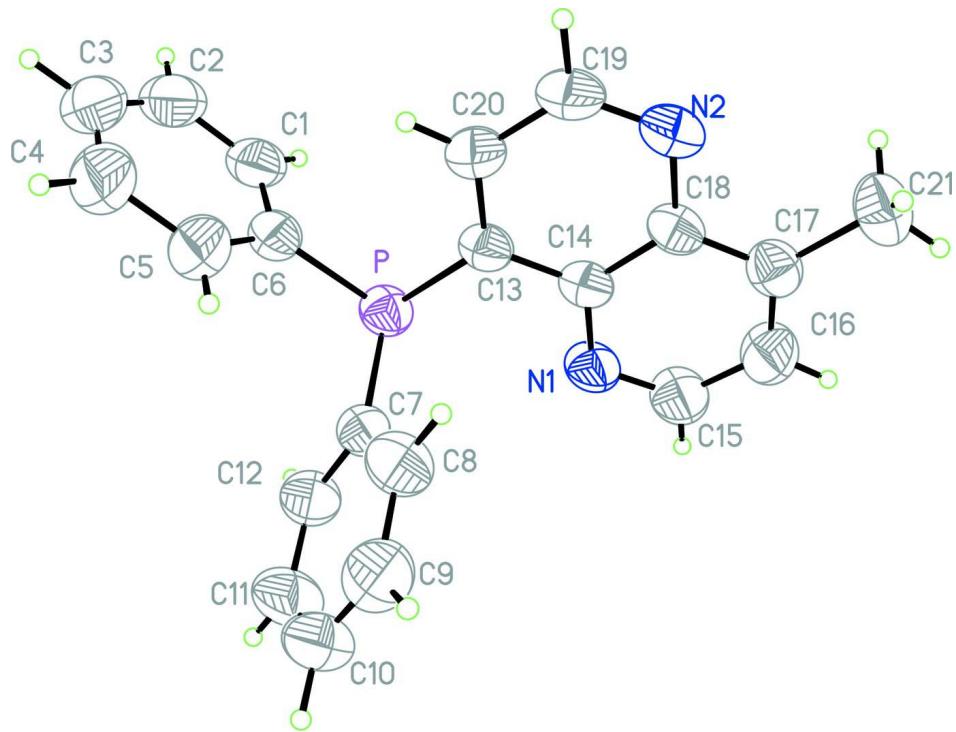
The 1,5-naphthyridine ring system is nearly planar with an r.m.s. deviation of 0.005 Å; its mean plane is oriented with respect to the two phenyl rings at 89.18 (8) and 77.39 (8)°. The two phenyl rings are twisted to each other with a dihedral angle of 88.12 (8)°. The crystal packing of the molecules in the crystal is influenced by van der Waals forces (Fig. 2).

S2. Experimental

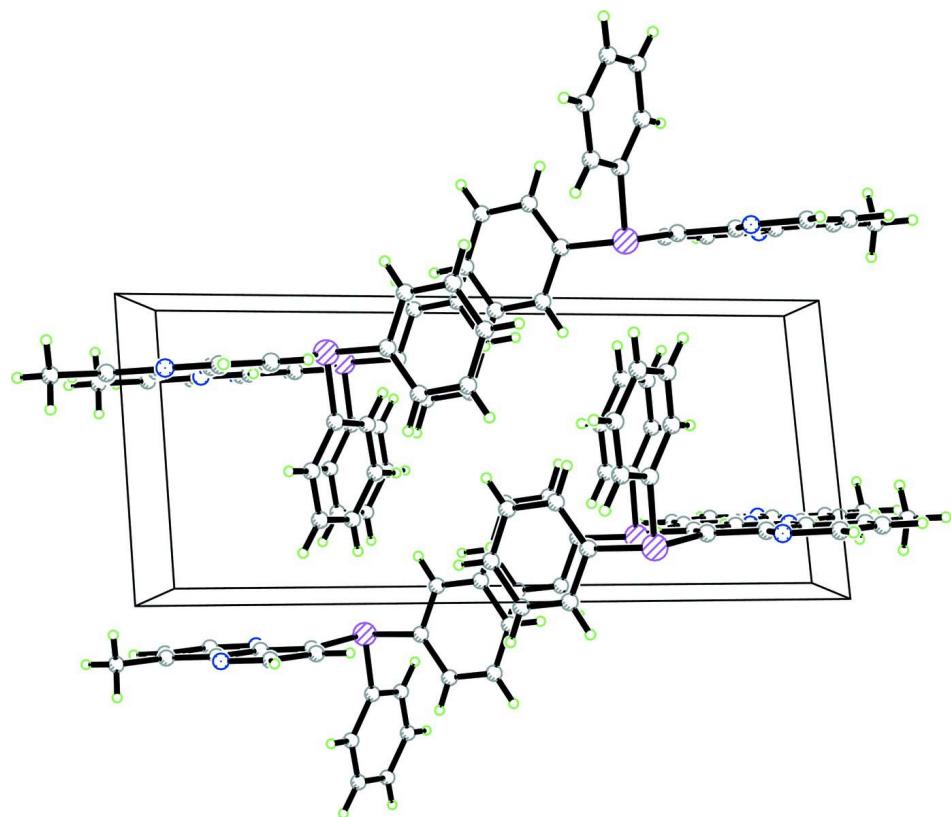
The title compound was synthesized according to the published procedure (Chen *et al.*, 2012). Yellow blocks were obtained by dissolving it (0.5 g) in tetrahydrofuran (20 ml) and evaporating the solvent slowly at room temperature for about 5 d.

S3. Refinement

H atoms were positioned geometrically and refined as riding groups, with C—H = 0.93 Å for aromatic H, and constrained to ride on their parent atoms, with $U_{\text{iso}}(\text{H}) = xU_{\text{eq}}(\text{C})$, where $x = 1.2$ for aromatic H, and $x = 1.5$ for other H.

**Figure 1**

The molecular structure of (I), with displacement ellipsoids drawn at the 50% probability level.

**Figure 2**

A packing diagram of (I).

4-Diphenylphosphanyl-8-methyl-1,5-naphthyridine

Crystal data

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 $M_r = 328.34$
Triclinic, $P\bar{1}$
Hall symbol: -P 1
 $a = 7.2320 (14) \text{ \AA}$
 $b = 7.4470 (15) \text{ \AA}$
 $c = 16.780 (3) \text{ \AA}$
 $\alpha = 99.78 (3)^\circ$
 $\beta = 93.35 (3)^\circ$
 $\gamma = 98.58 (3)^\circ$
 $V = 877.4 (3) \text{ \AA}^3$

$Z = 2$
 $F(000) = 344$
 $D_x = 1.243 \text{ Mg m}^{-3}$
Mo $K\alpha$ radiation, $\lambda = 0.71073 \text{ \AA}$
Cell parameters from 25 reflections
 $\theta = 10\text{--}14^\circ$
 $\mu = 0.16 \text{ mm}^{-1}$
 $T = 293 \text{ K}$
Block, yellow
 $0.30 \times 0.20 \times 0.10 \text{ mm}$

Data collection

Enraf–Nonius CAD-4
diffractometer

Radiation source: fine-focus sealed tube

Graphite monochromator

$\omega/2\theta$ scans

Absorption correction: ψ scan
(North *et al.*, 1968)

$T_{\min} = 0.954$, $T_{\max} = 0.984$

3500 measured reflections

3224 independent reflections
2285 reflections with $I > 2\sigma(I)$
 $R_{\text{int}} = 0.023$
 $\theta_{\max} = 25.4^\circ$, $\theta_{\min} = 1.2^\circ$
 $h = 0 \rightarrow 8$
 $k = -8 \rightarrow 8$
 $l = -20 \rightarrow 20$
3 standard reflections every 200 reflections
intensity decay: 1%

*Refinement*Refinement on F^2

Least-squares matrix: full

 $R[F^2 > 2\sigma(F^2)] = 0.050$ $wR(F^2) = 0.155$ $S = 1.00$

3224 reflections

217 parameters

0 restraints

Primary atom site location: structure-invariant
direct methodsSecondary atom site location: difference Fourier
mapHydrogen site location: inferred from
neighbouring sites

H-atom parameters constrained

 $w = 1/[\sigma^2(F_o^2) + (0.096P)^2]$
where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{\max} = 0.001$ $\Delta\rho_{\max} = 0.17 \text{ e } \text{\AA}^{-3}$ $\Delta\rho_{\min} = -0.23 \text{ e } \text{\AA}^{-3}$ *Special details*

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted R -factor wR and goodness of fit S are based on F^2 , conventional R -factors R are based on F , with F set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating R -factors(gt) etc. and is not relevant to the choice of reflections for refinement. R -factors based on F^2 are statistically about twice as large as those based on F , and R -factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\AA^2)

| | <i>x</i> | <i>y</i> | <i>z</i> | $U_{\text{iso}}^*/U_{\text{eq}}$ |
|------|--------------|-------------|--------------|----------------------------------|
| P | 0.18105 (10) | 0.17196 (9) | 0.71974 (4) | 0.0529 (2) |
| N1 | 0.2284 (3) | 0.3164 (3) | 0.89550 (13) | 0.0603 (6) |
| C1 | -0.0068 (5) | -0.0965 (4) | 0.59708 (17) | 0.0711 (8) |
| H1B | -0.1116 | -0.0650 | 0.6223 | 0.085* |
| N2 | 0.2453 (3) | -0.1579 (3) | 0.92992 (13) | 0.0569 (6) |
| C2 | -0.0308 (6) | -0.2312 (5) | 0.5287 (2) | 0.0906 (11) |
| H2B | -0.1507 | -0.2917 | 0.5087 | 0.109* |
| C3 | 0.1213 (7) | -0.2762 (5) | 0.4901 (2) | 0.0976 (13) |
| H3A | 0.1048 | -0.3655 | 0.4432 | 0.117* |
| C4 | 0.2974 (6) | -0.1907 (5) | 0.5202 (2) | 0.0914 (11) |
| H4A | 0.4009 | -0.2230 | 0.4942 | 0.110* |
| C5 | 0.3227 (5) | -0.0553 (4) | 0.58980 (18) | 0.0734 (8) |
| H5A | 0.4433 | 0.0028 | 0.6098 | 0.088* |
| C6 | 0.1710 (4) | -0.0060 (3) | 0.62951 (15) | 0.0579 (7) |
| C7 | 0.4103 (3) | 0.3111 (3) | 0.71826 (14) | 0.0501 (6) |
| C8 | 0.5758 (4) | 0.2855 (4) | 0.75679 (17) | 0.0644 (7) |
| H8A | 0.5754 | 0.1889 | 0.7854 | 0.077* |
| C9 | 0.7416 (4) | 0.4013 (4) | 0.75339 (19) | 0.0757 (8) |
| H9A | 0.8516 | 0.3842 | 0.7806 | 0.091* |
| C10 | 0.7445 (5) | 0.5412 (4) | 0.7101 (2) | 0.0822 (10) |
| H10A | 0.8568 | 0.6181 | 0.7071 | 0.099* |
| C11 | 0.5835 (5) | 0.5682 (4) | 0.6713 (2) | 0.0844 (10) |
| H11A | 0.5859 | 0.6635 | 0.6419 | 0.101* |
| C12 | 0.4175 (4) | 0.4557 (3) | 0.67539 (17) | 0.0652 (7) |
| H12A | 0.3080 | 0.4764 | 0.6491 | 0.078* |

| | | | | |
|------|------------|-------------|--------------|------------|
| C13 | 0.2210 (3) | 0.0390 (3) | 0.79998 (14) | 0.0476 (6) |
| C14 | 0.2313 (3) | 0.1306 (3) | 0.88168 (14) | 0.0468 (6) |
| C15 | 0.2393 (5) | 0.3962 (4) | 0.97172 (18) | 0.0744 (9) |
| H15A | 0.2379 | 0.5226 | 0.9827 | 0.089* |
| C16 | 0.2527 (4) | 0.3065 (4) | 1.03778 (18) | 0.0736 (8) |
| H16A | 0.2609 | 0.3736 | 1.0903 | 0.088* |
| C17 | 0.2539 (3) | 0.1222 (4) | 1.02590 (15) | 0.0557 (6) |
| C18 | 0.2437 (3) | 0.0284 (3) | 0.94493 (15) | 0.0478 (6) |
| C19 | 0.2366 (4) | -0.2382 (3) | 0.85361 (17) | 0.0638 (7) |
| H19A | 0.2389 | -0.3645 | 0.8426 | 0.077* |
| C20 | 0.2241 (4) | -0.1471 (3) | 0.78760 (16) | 0.0576 (6) |
| H20A | 0.2179 | -0.2133 | 0.7350 | 0.069* |
| C21 | 0.2657 (4) | 0.0179 (4) | 1.09549 (16) | 0.0724 (8) |
| H21A | 0.2718 | 0.1022 | 1.1460 | 0.109* |
| H21B | 0.3761 | -0.0394 | 1.0935 | 0.109* |
| H21C | 0.1565 | -0.0752 | 1.0911 | 0.109* |

Atomic displacement parameters (\AA^2)

| | U^{11} | U^{22} | U^{33} | U^{12} | U^{13} | U^{23} |
|-----|-------------|-------------|-------------|--------------|--------------|-------------|
| P | 0.0594 (4) | 0.0457 (4) | 0.0574 (4) | 0.0135 (3) | 0.0070 (3) | 0.0149 (3) |
| N1 | 0.0850 (16) | 0.0364 (11) | 0.0630 (14) | 0.0140 (10) | 0.0175 (12) | 0.0113 (10) |
| C1 | 0.086 (2) | 0.0568 (16) | 0.0678 (18) | -0.0071 (15) | -0.0020 (16) | 0.0218 (14) |
| N2 | 0.0624 (14) | 0.0436 (11) | 0.0676 (14) | 0.0070 (10) | 0.0070 (11) | 0.0191 (10) |
| C2 | 0.124 (3) | 0.066 (2) | 0.070 (2) | -0.022 (2) | -0.013 (2) | 0.0194 (17) |
| C3 | 0.166 (4) | 0.0558 (19) | 0.061 (2) | -0.009 (2) | 0.003 (2) | 0.0081 (15) |
| C4 | 0.136 (3) | 0.065 (2) | 0.077 (2) | 0.024 (2) | 0.029 (2) | 0.0121 (17) |
| C5 | 0.091 (2) | 0.0604 (17) | 0.0681 (18) | 0.0135 (15) | 0.0148 (16) | 0.0055 (14) |
| C6 | 0.0759 (18) | 0.0475 (14) | 0.0505 (14) | 0.0035 (13) | 0.0023 (13) | 0.0162 (11) |
| C7 | 0.0615 (15) | 0.0364 (12) | 0.0539 (14) | 0.0121 (11) | 0.0124 (12) | 0.0061 (10) |
| C8 | 0.0623 (17) | 0.0624 (17) | 0.0735 (18) | 0.0144 (14) | 0.0100 (14) | 0.0214 (14) |
| C9 | 0.0608 (18) | 0.087 (2) | 0.076 (2) | 0.0133 (16) | 0.0077 (15) | 0.0024 (17) |
| C10 | 0.082 (2) | 0.069 (2) | 0.088 (2) | -0.0125 (17) | 0.0211 (19) | 0.0113 (17) |
| C11 | 0.100 (3) | 0.0589 (18) | 0.096 (2) | -0.0019 (17) | 0.017 (2) | 0.0296 (17) |
| C12 | 0.0796 (19) | 0.0476 (14) | 0.0709 (18) | 0.0105 (14) | 0.0071 (14) | 0.0175 (13) |
| C13 | 0.0499 (14) | 0.0399 (12) | 0.0547 (14) | 0.0068 (10) | 0.0084 (11) | 0.0121 (10) |
| C14 | 0.0460 (13) | 0.0402 (12) | 0.0560 (14) | 0.0065 (10) | 0.0102 (11) | 0.0121 (10) |
| C15 | 0.113 (3) | 0.0438 (15) | 0.0681 (18) | 0.0187 (15) | 0.0194 (17) | 0.0057 (13) |
| C16 | 0.098 (2) | 0.0628 (18) | 0.0591 (17) | 0.0169 (16) | 0.0137 (16) | 0.0018 (14) |
| C17 | 0.0519 (15) | 0.0614 (16) | 0.0563 (15) | 0.0096 (12) | 0.0090 (12) | 0.0152 (12) |
| C18 | 0.0437 (13) | 0.0456 (13) | 0.0576 (14) | 0.0082 (10) | 0.0116 (11) | 0.0158 (11) |
| C19 | 0.082 (2) | 0.0361 (13) | 0.0733 (18) | 0.0077 (12) | 0.0043 (15) | 0.0130 (12) |
| C20 | 0.0713 (17) | 0.0409 (13) | 0.0591 (15) | 0.0070 (12) | 0.0045 (13) | 0.0072 (11) |
| C21 | 0.0725 (19) | 0.090 (2) | 0.0609 (17) | 0.0143 (16) | 0.0112 (14) | 0.0279 (15) |

Geometric parameters (\AA , $\text{^{\circ}}$)

| | | | |
|------------|-------------|--------------|-------------|
| P—C7 | 1.823 (3) | C9—C10 | 1.367 (4) |
| P—C6 | 1.825 (3) | C9—H9A | 0.9300 |
| P—C13 | 1.836 (2) | C10—C11 | 1.358 (5) |
| N1—C15 | 1.308 (3) | C10—H10A | 0.9300 |
| N1—C14 | 1.367 (3) | C11—C12 | 1.369 (4) |
| C1—C2 | 1.374 (4) | C11—H11A | 0.9300 |
| C1—C6 | 1.392 (4) | C12—H12A | 0.9300 |
| C1—H1B | 0.9300 | C13—C20 | 1.370 (3) |
| N2—C19 | 1.312 (3) | C13—C14 | 1.416 (3) |
| N2—C18 | 1.369 (3) | C14—C18 | 1.413 (3) |
| C2—C3 | 1.364 (5) | C15—C16 | 1.394 (4) |
| C2—H2B | 0.9300 | C15—H15A | 0.9300 |
| C3—C4 | 1.362 (5) | C16—C17 | 1.355 (4) |
| C3—H3A | 0.9300 | C16—H16A | 0.9300 |
| C4—C5 | 1.391 (4) | C17—C18 | 1.411 (3) |
| C4—H4A | 0.9300 | C17—C21 | 1.513 (3) |
| C5—C6 | 1.380 (4) | C19—C20 | 1.399 (3) |
| C5—H5A | 0.9300 | C19—H19A | 0.9300 |
| C7—C8 | 1.381 (4) | C20—H20A | 0.9300 |
| C7—C12 | 1.390 (3) | C21—H21A | 0.9600 |
| C8—C9 | 1.379 (4) | C21—H21B | 0.9600 |
| C8—H8A | 0.9300 | C21—H21C | 0.9600 |
| | | | |
| C7—P—C6 | 102.31 (12) | C10—C11—H11A | 119.8 |
| C7—P—C13 | 102.97 (11) | C12—C11—H11A | 119.8 |
| C6—P—C13 | 100.69 (11) | C11—C12—C7 | 121.0 (3) |
| C15—N1—C14 | 115.8 (2) | C11—C12—H12A | 119.5 |
| C2—C1—C6 | 121.5 (3) | C7—C12—H12A | 119.5 |
| C2—C1—H1B | 119.3 | C20—C13—C14 | 116.6 (2) |
| C6—C1—H1B | 119.3 | C20—C13—P | 125.1 (2) |
| C19—N2—C18 | 116.9 (2) | C14—C13—P | 117.97 (16) |
| C3—C2—C1 | 119.9 (3) | N1—C14—C18 | 122.9 (2) |
| C3—C2—H2B | 120.0 | N1—C14—C13 | 117.7 (2) |
| C1—C2—H2B | 120.0 | C18—C14—C13 | 119.5 (2) |
| C4—C3—C2 | 120.2 (3) | N1—C15—C16 | 125.1 (2) |
| C4—C3—H3A | 119.9 | N1—C15—H15A | 117.4 |
| C2—C3—H3A | 119.9 | C16—C15—H15A | 117.4 |
| C3—C4—C5 | 120.1 (4) | C17—C16—C15 | 120.3 (3) |
| C3—C4—H4A | 119.9 | C17—C16—H16A | 119.8 |
| C5—C4—H4A | 119.9 | C15—C16—H16A | 119.8 |
| C6—C5—C4 | 120.8 (3) | C16—C17—C18 | 117.2 (2) |
| C6—C5—H5A | 119.6 | C16—C17—C21 | 122.4 (3) |
| C4—C5—H5A | 119.6 | C18—C17—C21 | 120.4 (2) |
| C5—C6—C1 | 117.5 (3) | N2—C18—C17 | 119.3 (2) |
| C5—C6—P | 125.9 (2) | N2—C18—C14 | 122.1 (2) |
| C1—C6—P | 116.6 (2) | C17—C18—C14 | 118.6 (2) |

| | | | |
|----------------|--------------|-----------------|--------------|
| C8—C7—C12 | 117.7 (2) | N2—C19—C20 | 124.6 (2) |
| C8—C7—P | 125.38 (19) | N2—C19—H19A | 117.7 |
| C12—C7—P | 116.9 (2) | C20—C19—H19A | 117.7 |
| C9—C8—C7 | 120.8 (3) | C13—C20—C19 | 120.4 (2) |
| C9—C8—H8A | 119.6 | C13—C20—H20A | 119.8 |
| C7—C8—H8A | 119.6 | C19—C20—H20A | 119.8 |
| C10—C9—C8 | 120.1 (3) | C17—C21—H21A | 109.5 |
| C10—C9—H9A | 120.0 | C17—C21—H21B | 109.5 |
| C8—C9—H9A | 120.0 | H21A—C21—H21B | 109.5 |
| C11—C10—C9 | 120.0 (3) | C17—C21—H21C | 109.5 |
| C11—C10—H10A | 120.0 | H21A—C21—H21C | 109.5 |
| C9—C10—H10A | 120.0 | H21B—C21—H21C | 109.5 |
| C10—C11—C12 | 120.4 (3) | | |
| | | | |
| C6—C1—C2—C3 | -1.3 (5) | C7—P—C13—C14 | 76.6 (2) |
| C1—C2—C3—C4 | 1.4 (5) | C6—P—C13—C14 | -178.00 (19) |
| C2—C3—C4—C5 | -0.9 (5) | C15—N1—C14—C18 | 0.5 (4) |
| C3—C4—C5—C6 | 0.3 (5) | C15—N1—C14—C13 | -179.6 (2) |
| C4—C5—C6—C1 | -0.2 (4) | C20—C13—C14—N1 | -180.0 (2) |
| C4—C5—C6—P | -178.5 (2) | P—C13—C14—N1 | -6.0 (3) |
| C2—C1—C6—C5 | 0.7 (4) | C20—C13—C14—C18 | -0.1 (3) |
| C2—C1—C6—P | 179.2 (2) | P—C13—C14—C18 | 173.91 (17) |
| C7—P—C6—C5 | 19.7 (3) | C14—N1—C15—C16 | -0.2 (5) |
| C13—P—C6—C5 | -86.2 (2) | N1—C15—C16—C17 | -0.5 (5) |
| C7—P—C6—C1 | -158.59 (19) | C15—C16—C17—C18 | 0.9 (4) |
| C13—P—C6—C1 | 95.5 (2) | C15—C16—C17—C21 | -179.2 (3) |
| C6—P—C7—C8 | -91.8 (2) | C19—N2—C18—C17 | -179.6 (2) |
| C13—P—C7—C8 | 12.4 (2) | C19—N2—C18—C14 | 0.7 (3) |
| C6—P—C7—C12 | 88.9 (2) | C16—C17—C18—N2 | 179.7 (2) |
| C13—P—C7—C12 | -166.89 (19) | C21—C17—C18—N2 | -0.2 (3) |
| C12—C7—C8—C9 | 0.7 (4) | C16—C17—C18—C14 | -0.6 (4) |
| P—C7—C8—C9 | -178.5 (2) | C21—C17—C18—C14 | 179.5 (2) |
| C7—C8—C9—C10 | -1.4 (4) | N1—C14—C18—N2 | 179.6 (2) |
| C8—C9—C10—C11 | 1.0 (5) | C13—C14—C18—N2 | -0.3 (3) |
| C9—C10—C11—C12 | 0.0 (5) | N1—C14—C18—C17 | -0.1 (4) |
| C10—C11—C12—C7 | -0.7 (5) | C13—C14—C18—C17 | 180.0 (2) |
| C8—C7—C12—C11 | 0.3 (4) | C18—N2—C19—C20 | -0.7 (4) |
| P—C7—C12—C11 | 179.6 (2) | C14—C13—C20—C19 | 0.1 (4) |
| C7—P—C13—C20 | -110.0 (2) | P—C13—C20—C19 | -173.4 (2) |
| C6—P—C13—C20 | -4.6 (3) | N2—C19—C20—C13 | 0.3 (4) |