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## 1,3-Alternate conformer 5,11,17,23tetra-*tert*-butyl-25,26,27,28-tetrakis(4methylsulfanylbenzyloxy)-2,8,14,20tetrathiacalix[4]arene

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Key indicators: single-crystal X-ray study; T = 293 K; mean  $\sigma$ (C–C) = 0.004 Å; disorder in main residue; R factor = 0.059; wR factor = 0.172; data-to-parameter ratio = 15.3.

The title thiacalix[4]arene derivative,  $C_{72}H_{80}O_4S_8$ , adopts a 1,3-alternate conformation, where the four 4-methylsulfanylbenzyl groups are located alternately at the two sides of a virtual plane defined by the four bridging S atoms. In the crystal, there are no significant intermolecular interactions present. Some of the peripheral *tert*-butyl and methylsulfanyl groups are disordered over two positions. A region of disordered electron density, occupying voids of *ca* 700 Å<sup>3</sup> for an electron count of 124, was treated using the SQUEEZE routine in *PLATON* [Spek (2009). *Acta Cryst.* D65, 148–155].

#### **Related literature**

For a similar compound adopting a 1,3-alternate conformation, see: Xu *et al.* (2008). For background to thiacalix[4]arene derivatives, see: Kumagai *et al.* (1997); Morohashi *et al.* (2006); Yamato *et al.* (2006). For background to multidentate methylthioethers, see: Maye *et al.* (2005); Lim *et al.* (2007); Yan *et al.* (2010). For the synthesis, see: Morohashi *et al.* (2003).



 $\gamma = 84.762 \ (2)^{\circ}$ V = 3866.4 (5) Å<sup>3</sup>

Mo  $K\alpha$  radiation

 $0.26 \times 0.21 \times 0.15 \text{ mm}$ 

 $\mu = 0.27 \text{ mm}^{-1}$ 

T = 293 K

Z = 2

#### **Experimental**

Crystal data  $C_{72}H_{80}O_4S_8$   $M_r = 1265.84$ Triclinic,  $P\overline{1}$  a = 15.1863 (10) Å b = 15.5795 (11) Å c = 16.9774 (12) Å  $\alpha = 75.473 (2)^{\circ}$  $\beta = 85.686 (2)^{\circ}$ 

#### Data collection

Bruker SMART CCD area-detector<br/>diffractometer14394 measured reflections<br/>14394 independent reflectionsAbsorption correction: multi-scan<br/>(SADABS; Bruker, 2007)<br/> $T_{min} = 0.434, T_{max} = 1.000$ 9034 reflections with  $I > 2\sigma(I)$ 

#### Refinement

 $\begin{array}{ll} R[F^2 > 2\sigma(F^2)] = 0.059 & 244 \mbox{ restraints} \\ WR(F^2) = 0.172 & H\mbox{-atom parameters constrained} \\ S = 0.96 & \Delta\rho_{max} = 0.40 \mbox{ e } {\rm \AA}^{-3} \\ 14394 \mbox{ reflections} & \Delta\rho_{min} = -0.29 \mbox{ e } {\rm \AA}^{-3} \\ 939 \mbox{ parameters} \end{array}$ 

Data collection: *SMART* (Bruker, 2007); cell refinement: *SAINT* (Bruker, 2007); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL* (Sheldrick, 2008); software used to prepare material for publication: *SHELXTL*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: SU2608).

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## supporting information

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# 1,3-Alternate conformer 5,11,17,23-tetra-*tert*-butyl-25,26,27,28-tetrakis(4-methylsulfanylbenzyloxy)-2,8,14,20-tetrathiacalix[4]arene

### Qingsong Gao, Dexun Xie and Delie An

#### S1. Comment

Thiacalix[4]arenes are macrocyclic molecules made up of *p*-substituted phenolic units linked by sulfur atoms *ortho* to the OH functions (Kumagai *et al.*, 1997). The ability of the parent phenolic thiacalix[4]arenes, as well as of their chemically modified derivatives obtained by the substitution of the phenolic H atoms with various types of ligating groups, to bind metal ions is well established (Morohashi *et al.*, 2006). With thiacalix[4]arenes, the substituents frequently immobilize the molecule in a single conformation: cone, partial cone, 1,2- or 1,3-alternate. The ability to control inter-particle spatial properties of nanoparticle assemblies is one of the major challenges for the design and understanding of functional nanostructures. As a molecular linker, multidentate thioethers have been exploited for such control (Maye *et al.*, 2005). The viability of inter-particle linkages *via* coordination of the methylthio groups of arylethynes to gold surfaces was demonstrated recently in our laboratory (Lim *et al.*, 2007; Yan *et al.*, 2010). Multi-functional groups is the common characteristic of these molecular linkers. The 1,3-alternate conformer thiacalixarene derivative is an ideal molecular linker for assembling nanoparticle clusters. With this in mind, we synthesized the title compound, the first example of a thiacalix[4]arene derivative containing multidentate methylthioethers, and we report herein on its crystal structure.

The molecular structure of the title molecule is shown in Fig 1. The macrocycle adopts a 1,3-alternate conformation in which four substituent groups are located alternately above and below the virtual plane defined by four bridging sulfur atoms, S1-S4. The 1,3-alternate conformation thus appears to be regular and two pairs of opposite phenolic units are almost parallel to each other, but the substituent groups are inclined to one another. Comparable conformations were found in methyl ester derivatives (Xu *et al.*, 2008), whereas the title tetra-benzyl ether derivative is much more distorted as a result of increased steric hindrance.

The plane defined by the substitutional aromatic ring on O4 atom (r.m.s. deviation 0.0177 Å) was chosen as a reference plane. The plane defined by the other substitutional aromatic rings on O atoms (O1, O2 and O3) make dihedral angles of 87.83 (11), 76.84 (11) and 71.78 (13) °, respectively, with this reference plane, whereas the four aromatic rings on the skeleton make dihedral angles of 83.52 (8), 76.20 (8), 84.47 (8) and 83.09 (8) °, respectively, with this reference plane. The conformations of the benzyl ether chains are extended and deviate from the plane defined by four bridging sulfur atoms. Atoms C41, C49, C57 and C65 point towards the exterior of the macrocycle and the torsion angles around the O1 —C41, C49—O2, C57—O3 and C65—O4 bonds deviate from ideal *syn* or *anti* values by more than 70°.

In the crystal, there are no significant intermolecular interactions present.

#### **S2. Experimental**

A mixture of *p*-tetra-*tert*-butylthiacalix[4]arene (360 mg, 0.50 mmol) and  $Cs_2CO_3$  (1.30 g, 4.00 mmol) in anhydrous acetone (50 ml) was heated at refluxed for 30 min. Then a solution of 4-methylthiobenzyl bromide (864 mg, 4.00 mmol) in acetone (10 ml) was added and the mixture heated at reflux for 2 h. After cooling the reaction mixture, it was filtered.

The filtrate was concentrated and the residue was purified by column chromatography from petroleum ether/dichloromethane (4:1, v/v) to give 410 mg (65%) of compound I as a white solid: M.p. 513~516 K; MS(ESI) m/z: 1283.1  $[M+H_2O]^+$ . Spectroscopic data for the title compound is available in the archived CIF. Colourless crystals of the title compound, suitable for X-ray diffraction analysis, were obtained by slow diffusion of petroleum ether into a chloroform solution at 298 K.

#### **S3. Refinement**

Some of the peripheral -SCH<sub>3</sub> and *t*-butyl groups are disordered over two positions. These include the S-CH<sub>3</sub> groups involving atoms S5-C48, S6-C56, S7-C64 and S8-C72, and the *t*-butyl groups involving atoms C18-C20, C28-C30 and C38-C40; details are available in the archived CIF. A region of disordered electron density occupying voids of ca. 700 Å<sup>3</sup>, for an electron count of 124, was treated using the SQUEEZE routine in PLATON (Spek, 2009). It was not taken into consideration during refinement. The C-bound H atoms were positioned geometrically and allowed to ride on their parent atoms: C—H = 0.93-0.97 Å with  $U_{iso}(H) = 1.5U_{eq}(C)$  for methyl H atoms and  $= 1.2U_{eq}(C)$  for other H atoms.



#### Figure 1

A view of the molecular structure of the title compound, with atom labelling. Displacement ellipsoids are drawn at the 50% probability level. Only the major components of the disordered peripheral groups are shown.

5,11,17,23-Tetra-tert-butyl-25,26,27,28-tetrakis(4-methylsulfanylbenzyloxy)-2,8,14,20-tetrathiacalix[4]arene

Z = 2

F(000) = 1344

 $\theta = 4.4 - 45.1^{\circ}$ 

 $\mu = 0.27 \text{ mm}^{-1}$ 

T = 293 K

 $R_{\rm int} = 0.000$ 

 $h = -18 \rightarrow 18$  $k = -18 \rightarrow 18$ 

 $l = 0 \rightarrow 20$ 

 $D_{\rm x} = 1.087 {\rm Mg} {\rm m}^{-3}$ 

Prismatic, colourless  $0.26 \times 0.21 \times 0.15 \text{ mm}$ 

14394 measured reflections

 $\theta_{\text{max}} = 25.5^{\circ}, \ \theta_{\text{min}} = 1.4^{\circ}$ 

14394 independent reflections

9034 reflections with  $I > 2\sigma(I)$ 

Mo *K* $\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 4356 reflections

#### Crystal data

 $C_{72}H_{80}O_4S_8$   $M_r = 1265.84$ Triclinic,  $P\overline{1}$ Hall symbol: -P 1 a = 15.1863 (10) Å b = 15.5795 (11) Å c = 16.9774 (12) Å  $a = 75.473 (2)^{\circ}$   $\beta = 85.686 (2)^{\circ}$   $\gamma = 84.762 (2)^{\circ}$  $V = 3866.4 (5) \text{ Å}^3$ 

#### Data collection

Bruker SMART CCD area-detector diffractometer Radiation source: fine-focus sealed tube Graphite monochromator phi and  $\omega$  scans Absorption correction: multi-scan (*SADABS*; Bruker, 2007)  $T_{\min} = 0.434, T_{\max} = 1.000$ 

#### Refinement

Refinement on $F^2$ Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.059$ $wP(F^2) = 0.172$	Secondary atom site location: difference Fourier map Hydrogen site location: inferred from
$WR(F^2) = 0.172$ S = 0.96 14394 reflections 939 parameters	H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.1009P)^2]$ where $P = (F_o^2 + 2F_o^2)/3$
244 restraints Primary atom site location: structure-invariant direct methods	$(\Delta/\sigma)_{\rm max} = 0.004$ $\Delta\rho_{\rm max} = 0.40 \text{ e } \text{\AA}^{-3}$ $\Delta\rho_{\rm min} = -0.29 \text{ e } \text{\AA}^{-3}$

#### Special details

Experimental. Spectroscopic data for the title compound:

<sup>1</sup>H NMR (400 MHz, CDCl<sub>3</sub>): 7.12 (s, 8H), 7.05 (d, J = 8.4 Hz, 8H), 6.92 (d, J = 8.4 Hz, 8H), 5.04 (s, 8H), 2.48 (s, 12H, SCH<sub>3</sub>), 0.86 (s, 36H); <sup>13</sup>C NMR (100 MHz, CDCl<sub>3</sub>): 156.89 (C), 146.15 (C), 136.67 (C), 134.87 (C), 129.26 (CH), 128.57 (C), 127.69 (CH), 126.95 (CH), 70.65 (CH<sub>2</sub>), 33.86 (C), 30.73 (CH<sub>3</sub>), 16.31 (SCH<sub>3</sub>).

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

	x	у	Ζ	$U_{\rm iso}$ */ $U_{\rm eq}$	Occ. (<1)
<u>S1</u>	0.94198 (4)	0.90174 (4)	0.09861 (4)	0.05036 (19)	
S2	0.92245 (5)	0.55348 (5)	0.07790 (5)	0.0582 (2)	
S3	0.55404 (5)	0.59267 (5)	0.09846 (5)	0.0631 (2)	
S4	0.57286 (4)	0.93527 (5)	0.13515 (4)	0.0541 (2)	
S5	1.3408 (4)	0.7583 (4)	-0.0886 (7)	0.1079 (15)	0.70
<b>S</b> 6	0.7412 (5)	0.5926 (7)	0.5541 (5)	0.1038 (18)	0.50
S7	0.7645 (7)	0.8754 (7)	-0.3436 (5)	0.101 (2)	0.50
S8	0.5403 (5)	1.1277 (5)	0.4157 (3)	0.0949 (13)	0.55
C48	1.3875 (3)	0.6516 (4)	-0.0944 (4)	0.0867 (19)	0.65
H48A	1.3728	0.6089	-0.0448	0.130*	0.65
H48B	1.4507	0.6526	-0.1023	0.130*	0.65
H48C	1.3644	0.6355	-0.1394	0.130*	0.65
C56	0.7113 (9)	0.7107 (9)	0.5414 (10)	0.122 (4)	0.50
H56A	0.7601	0.7438	0.5151	0.184*	0.50
H56B	0.6971	0.7227	0.5939	0.184*	0.50
H56C	0.6608	0.7279	0.5087	0.184*	0.50
C64	0.6894 (8)	0.9425 (8)	-0.4157 (6)	0.118 (4)	0.50
H64A	0.6667	0.9941	-0.3974	0.177*	0.50
H64B	0.6413	0.9084	-0.4203	0.177*	0.50
H64C	0.7203	0.9606	-0.4679	0.177*	0.50
C72	0.5345 (9)	1.2383 (7)	0.3516 (8)	0.119 (3)	0.60
H72D	0.5930	1.2584	0.3398	0.179*	0.60
H72E	0.4987	1.2772	0.3789	0.179*	0.60
H72F	0.5086	1.2385	0.3016	0.179*	0.60
S5′	1.3463 (11)	0.7406 (12)	-0.0752 (17)	0.1084 (16)	0.30
S6'	0.7109 (6)	0.6042 (8)	0.5530 (6)	0.122 (3)	0.50
S7′	0.7480 (8)	0.8905 (8)	-0.3466 (5)	0.117 (3)	0.50
S8′	0.5571 (8)	1.1460 (8)	0.4075 (6)	0.140 (4)	0.45
C48′	1.3332 (13)	0.6556 (10)	-0.1267 (10)	0.138 (5)	0.35
H48D	1.3409	0.5983	-0.0894	0.207*	0.35
H48E	1.3766	0.6597	-0.1714	0.207*	0.35
H48F	1.2749	0.6635	-0.1470	0.207*	0.35
C56′	0.7588 (10)	0.7043 (10)	0.5410 (10)	0.138 (5)	0.50
H56D	0.7428	0.7439	0.4901	0.208*	0.50
H56E	0.8220	0.6935	0.5412	0.208*	0.50
H56F	0.7379	0.7307	0.5850	0.208*	0.50
C64′	0.6973 (10)	0.9922 (8)	-0.4005 (8)	0.143 (5)	0.50
H64D	0.6341	0.9911	-0.3922	0.215*	0.50
H64E	0.7136	1.0011	-0.4576	0.215*	0.50
H64F	0.7164	1.0399	-0.3812	0.215*	0.50
C72′	0.5716 (15)	1.2563 (14)	0.3432 (17)	0.174 (11)	0.40
H72A	0.6305	1.2720	0.3472	0.260*	0.40
H72B	0.5294	1.2984	0.3607	0.260*	0.40
H72C	0.5627	1.2568	0.2877	0.260*	0.40
01	0.89430 (12)	0.76024 (13)	0.01849 (11)	0.0584 (5)	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(\hat{A}^2)$ 

O2	0.74105 (12)	0.60108 (12)	0.15708 (10)	0.0515 (4)	
03	0.61701 (11)	0.78218 (12)	0.04810 (10)	0.0482 (4)	
04	0.75495 (12)	0.85942 (12)	0.18907 (11)	0.0554 (5)	
C1	0.94462 (15)	0.78558 (16)	0.14019 (15)	0.0422 (6)	
C2	0.97394 (16)	0.75315 (17)	0.21775 (15)	0.0475 (6)	
H2	0.9865	0.7933	0.2470	0.057*	
C3	0.98546 (16)	0.66224 (18)	0.25391 (15)	0.0478 (6)	
C4	0.96376 (16)	0.60604(17)	0.20888(16)	0.0486 (6)	
H4	0.9686	0 5451	0.2319	0.058*	
C5	0.93484(15)	0.63659(16)	0.13047(15)	0.0433 (6)	
C6	0.92664(15)	0.72676 (16)	0.09419(14)	0.0410(6)	
C7	1 01959 (18)	0.72070(10) 0.6293(2)	0.34044(16)	0.0410(0) 0.0604(8)	
C8	1.0129 (3)	0.5297(2)	0.3732(2)	0.0004(0) 0.1042(13)	
U8 H8A	0.0520	0.5297 (5)	0.3752 (2)	0.1042 (13)	
	1.0361	0.5105	0.3760	0.156*	
	1.0301	0.3110	0.4204	0.156*	
	1.0403	0.4987	0.3372 0.2262(2)	$0.130^{\circ}$	
	1.1108 (2)	0.0489 (3)	0.3303 (2)	0.1014 (15)	
H9A LIOD	1.1306	0.6166	0.3016	0.152*	
H9B	1.1387	0.6309	0.3900	0.152*	
H9C	1.1220	0./115	0.3148	0.152*	
C10	0.9657 (3)	0.6748 (3)	0.3990 (2)	0.1032 (13)	
H10A	0.9707	0.7378	0.3814	0.155*	
H10B	0.9876	0.6529	0.4526	0.155*	
H10C	0.9048	0.6625	0.4004	0.155*	
C11	0.81713 (17)	0.57302 (16)	0.03584 (16)	0.0468 (6)	
C12	0.81386 (18)	0.56067 (17)	-0.04176 (16)	0.0513 (7)	
H12	0.8667	0.5513	-0.0709	0.062*	
C13	0.73439 (19)	0.56175 (18)	-0.07774 (16)	0.0536 (7)	
C14	0.65774 (18)	0.57739 (19)	-0.03304 (16)	0.0545 (7)	
H14	0.6035	0.5799	-0.0559	0.065*	
C15	0.65889 (17)	0.58959 (17)	0.04548 (16)	0.0494 (6)	
C16	0.73887 (17)	0.58747 (16)	0.08053 (15)	0.0455 (6)	
C17	0.7309 (2)	0.5441 (2)	-0.16228 (19)	0.0693 (9)	
C18	0.8077 (14)	0.5946 (9)	-0.2193 (10)	0.079 (3)	0.50
H18A	0.8642	0.5692	-0.1993	0.119*	0.50
H18B	0.8012	0.6565	-0.2193	0.119*	0.50
H18C	0.8042	0.5885	-0.2739	0.119*	0.50
C19	0.7130 (6)	0.4463 (7)	-0.1505(7)	0.099 (3)	0.60
H19A	0.7058	0.4348	-0.2026	0.148*	0.60
H19B	0.6599	0.4340	-0.1166	0.148*	0.60
H19C	0 7619	0 4089	-0.1251	0 148*	0.60
C20	0.6510(10)	0.6081 (7)	-0.2097(9)	0.081(3)	0.50
H20A	0.6626	0.6692	-0.2167	0.121*	0.50
H20R	0.5962	0.5966	-0.1784	0.121*	0.50
H20C	0.6471	0.5962	-0.2621	0.121*	0.50
C18′	0.0771 0.8117(15)	0.5702	-0.2147(12)	0.121 0.005 (5)	0.50
	0.80/1	0.5009 (9)	-0.2650	0.073 (3)	0.50
	0.0041	0.5475	-0.1997	0.143	0.50
1110E	0.0000	0.5239	-0.100/	0.145	0.50

H18F	0.8235	0.6222	-0.2240	0.143*	0.50
C19′	0.7610 (10)	0.4428 (12)	-0.1482 (11)	0.112 (5)	0.40
H19D	0.7581	0.4249	-0.1981	0.169*	0.40
H19E	0.7226	0.4089	-0.1068	0.169*	0.40
H19F	0.8207	0.4325	-0.1312	0.169*	0.40
C20′	0.6462 (10)	0.5704 (7)	-0.1996 (9)	0.087 (3)	0.50
H20D	0.6358	0.6339	-0.2119	0.131*	0.50
H20E	0.5997	0.5438	-0.1625	0.131*	0.50
H20F	0.6471	0.5507	-0.2489	0.131*	0.50
C21	0.55120 (16)	0.67324 (18)	0.15619 (15)	0.0480 (6)	
C22	0.51071 (17)	0.64880 (19)	0.23451 (16)	0.0524 (7)	
H22	0.4942	0.5910	0.2547	0.063*	
C23	0.49475 (16)	0.70917 (19)	0.28255 (15)	0.0506 (7)	
C24	0.52130 (16)	0.79369 (19)	0.25020 (15)	0.0485 (6)	
H24	0.5121	0.8350	0.2817	0.058*	
C25	0.56121 (15)	0.81970 (17)	0.17237 (15)	0.0448 (6)	
C26	0.57623 (15)	0.75879 (17)	0.12452 (14)	0.0432 (6)	
C27	0.4468 (2)	0.6825 (2)	0.36633 (17)	0.0648 (8)	
C28	0.4834 (8)	0.5980 (8)	0.4150 (7)	0.078 (3)	0.55
H28A	0.4491	0.5821	0.4657	0.118*	0.55
H28B	0.5436	0.6033	0.4257	0.118*	0.55
H28C	0.4817	0.5528	0.3859	0.118*	0.55
C29	0.4863 (8)	0.7236 (9)	0.4259 (8)	0.120 (4)	0.50
H29A	0.4622	0.6988	0.4800	0.180*	0.50
H29B	0.4723	0.7867	0.4117	0.180*	0.50
H29C	0.5494	0.7113	0.4240	0.180*	0.50
C30	0.3469 (7)	0.6736 (6)	0.3514 (6)	0.063 (2)	0.55
H30A	0.3438	0.6265	0.3247	0.095*	0.55
H30B	0.3228	0.7284	0.3176	0.095*	0.55
H30C	0.3135	0.6604	0.4027	0.095*	0.55
C28′	0.4615 (12)	0.5716 (11)	0.4032 (12)	0.107 (6)	0.45
H28D	0.5218	0.5519	0.3921	0.161*	0.45
H28E	0.4227	0.5428	0.3776	0.161*	0.45
H28F	0.4482	0.5569	0.4610	0.161*	0.45
C29′	0.4421 (7)	0.7589 (7)	0.4124 (7)	0.096 (3)	0.50
H29D	0.4133	0.7393	0.4654	0.144*	0.50
H29E	0.4092	0.8105	0.3818	0.144*	0.50
H29F	0.5010	0.7735	0.4180	0.144*	0.50
C30′	0.3535 (11)	0.7105 (9)	0.3632 (10)	0.100 (5)	0.45
H30D	0.3283	0.6887	0.3225	0.150*	0.45
H30E	0.3459	0.7743	0.3498	0.150*	0.45
H30F	0.3242	0.6872	0.4154	0.150*	0.45
C31	0.67539 (16)	0.94933 (16)	0.07791 (16)	0.0457 (6)	
C32	0.67360 (17)	1.00449 (17)	0.00043 (17)	0.0520 (7)	
H32	0.6191	1.0264	-0.0209	0.062*	
C33	0.75021 (17)	1.02849 (17)	-0.04684 (16)	0.0506 (7)	
C34	0.82966 (16)	0.99078 (16)	-0.01344 (16)	0.0465 (6)	
H34	0.8823	1.0034	-0.0443	0.056*	

C35	0.83338 (15)	0.93503 (15)	0.06423 (16)	0.0424 (6)	
C36	0.75657 (16)	0.91547 (15)	0.11223 (15)	0.0424 (6)	
C37	0.7462 (2)	1.0937 (2)	-0.13094 (19)	0.0690 (9)	
C38	0.8285 (5)	1.1254 (7)	-0.1654 (6)	0.100 (3)	0.50
H38A	0.8696	1.0759	-0.1697	0.151*	0.50
H38B	0.8513	1,1579	-0.1313	0.151*	0.50
H38C	0.8203	1.1637	-0.2187	0.151*	0.50
C39	0.6820 (5)	1 1826 (4)	-0.1164(4)	0.0743(19)	0.50
H39A	0.6760	1 2258	-0.1675	0.112*	0.50
H39B	0.7086	1 2082	-0.0790	0.112*	0.50
H39C	0.6245	1 1645	-0.0944	0.112*	0.50
C40	0.6215	1.0612 (6)	-0.1841(6)	0.077(3)	0.50
H40A	0.6291	1.0590	-0.1605	0.116*	0.00
H40R	0.0291	1.0028	-0.1884	0.116*	0.00
	0.6888	1.0020	-0.2374	0.116*	0.00
C38'	0.0888	1.1010	-0.1017(4)	$0.110^{\circ}$	0.00
11200	0.8304 (0)	1.0505 (0)	0.1917 (4)	0.092 (2)	0.50
П30D 1120E	0.8247	0.9931	-0.1898	0.138*	0.50
ПЭ0Е 1120Е	0.8807	1.0020	-0.1722	0.138	0.50
П30Г С20/	0.8200	1.0912	-0.2409	0.138	0.50
U39 1120D	0.7743 (8)	1.1780 (5)	-0.1287(5)	0.110 (3)	0.50
H39D	0.7749	1.21/1	-0.1826	0.100*	0.50
H39E	0.8327	1.1709	-0.1087	0.166*	0.50
H39F	0.7339	1.2046	-0.0933	0.166*	0.50
C40'	0.6673 (10)	1.0938 (10)	-0.1712 (10)	0.093 (5)	0.40
H40D	0.6777	1.1173	-0.2288	0.140*	0.40
H40E	0.6210	1.1301	-0.1509	0.140*	0.40
H40F	0.6500	1.0341	-0.1611	0.140*	0.40
C41	0.9429 (2)	0.7617 (3)	-0.05348 (19)	0.0923 (12)	
H41A	0.9234	0.8159	-0.0924	0.111*	
H41B	0.9263	0.7125	-0.0733	0.111*	
C42	1.04093 (19)	0.7569 (2)	-0.05638 (16)	0.0562 (7)	
C43	1.0881 (2)	0.8287 (2)	-0.0609(2)	0.0734 (9)	
H43	1.0571	0.8819	-0.0570	0.088*	
C44	1.1777 (2)	0.8264 (2)	-0.0708(2)	0.0770 (9)	
H44	1.2062	0.8780	-0.0755	0.092*	
C45	1.2255 (2)	0.7502 (2)	-0.07393 (19)	0.0663 (8)	
C46	1.1828 (2)	0.6758 (2)	-0.0680(2)	0.0847 (11)	
H46	1.2149	0.6226	-0.0702	0.102*	
C47	1.0911 (2)	0.6795 (2)	-0.0585 (2)	0.0836 (10)	
H47	1.0627	0.6278	-0.0534	0.100*	
C49	0.7374 (2)	0.5227 (2)	0.22128 (18)	0.0722 (9)	
H49A	0.7884	0.4819	0.2158	0.087*	
H49B	0.6844	0.4935	0.2185	0.087*	
C50	0.73654 (19)	0.5463 (2)	0.30111 (16)	0.0590 (7)	
C51	0.7421 (2)	0.4787 (2)	0.3715 (2)	0.0797 (10)	
H51	0.7469	0.4199	0.3679	0.096*	
C52	0.7408 (3)	0.4970 (3)	0.4467 (2)	0.0885 (11)	
H52	0.7463	0.4504	0.4929	0.106*	

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C53	0.7316 (2)	0.5822 (3)	0.45457 (18)	0.0762 (10)
C54	0.7265 (2)	0.6505 (2)	0.38446 (18)	0.0738 (9)
H54	0.7215	0.7093	0.3884	0.089*
C55	0.7288 (2)	0.6322 (2)	0.30871 (17)	0.0635 (8)
H55	0.7250	0.6789	0.2623	0.076*
C57	0.55681 (18)	0.8144 (2)	-0.01567 (16)	0.0621 (8)
H57A	0.5263	0.8702	-0.0101	0.074*
H57B	0.5129	0.7718	-0.0119	0.074*
C58	0.60755 (17)	0.82777 (18)	-0.09687 (15)	0.0498 (6)
C59	0.69751 (18)	0.8091 (2)	-0.10537 (17)	0.0595 (8)
Н59	0.7297	0.7851	-0.0594	0.071*
C60	0.7401 (2)	0.8257 (2)	-0.18123 (18)	0.0677 (9)
H60	0.8009	0.8121	-0.1860	0.081*
C61	0.6942 (2)	0.8625 (2)	-0.25093 (17)	0.0671 (8)
C62	0.6036 (2)	0.8789 (2)	-0.24219 (18)	0.0712 (9)
H62	0.5710	0.9016	-0.2881	0.085*
C63	0.56160 (19)	0.8621 (2)	-0.16682 (18)	0.0613 (8)
H63	0.5005	0.8739	-0.1621	0.074*
C65	0.7901 (2)	0.8914 (2)	0.25194 (18)	0.0726 (9)
H65A	0.8429	0.9217	0.2296	0.087*
H65B	0.8078	0.8408	0.2955	0.087*
C66	0.7271 (2)	0.9535 (2)	0.28716 (18)	0.0674 (8)
C67	0.7308 (4)	1.0429 (3)	0.2639 (3)	0.1251 (17)
H67	0.7725	1.0668	0.2233	0.150*
C68	0.6738 (4)	1.1006 (3)	0.2991 (3)	0.1278 (18)
H68	0.6770	1.1617	0.2802	0.153*
C69	0.6153 (3)	1.0692 (3)	0.3591 (2)	0.0833 (10)
C70	0.6075 (3)	0.9797 (3)	0.3810 (2)	0.0950 (12)
H70	0.5643	0.9567	0.4204	0.114*
C71	0.6625 (3)	0.9227 (3)	0.3458 (2)	0.0841 (10)
H71	0.6556	0.8620	0.3623	0.101*

Atomic displacement parameters  $(Å^2)$ 

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
S1	0.0351 (3)	0.0425 (4)	0.0712 (5)	-0.0045 (3)	-0.0091 (3)	-0.0073 (3)
S2	0.0531 (4)	0.0521 (4)	0.0765 (5)	0.0083 (3)	-0.0126 (4)	-0.0308 (4)
S3	0.0511 (4)	0.0731 (5)	0.0756 (5)	-0.0196 (4)	0.0114 (4)	-0.0365 (4)
S4	0.0399 (4)	0.0493 (4)	0.0695 (5)	0.0021 (3)	0.0070 (3)	-0.0126 (3)
S5	0.0590 (11)	0.091 (3)	0.175 (4)	-0.0079 (15)	0.0024 (14)	-0.037 (3)
S6	0.135 (5)	0.135 (3)	0.0394 (16)	0.007 (3)	-0.019 (3)	-0.0198 (15)
<b>S</b> 7	0.095 (3)	0.167 (5)	0.043 (2)	-0.012 (4)	0.0104 (16)	-0.031 (3)
<b>S</b> 8	0.108 (2)	0.119 (3)	0.0641 (16)	0.021 (3)	-0.0073 (16)	-0.0442 (16)
C48	0.039 (3)	0.095 (4)	0.123 (5)	0.021 (3)	-0.015 (3)	-0.029 (3)
C56	0.137 (9)	0.165 (9)	0.080 (6)	-0.016 (7)	-0.008(7)	-0.057 (6)
C64	0.134 (7)	0.149 (8)	0.054 (5)	-0.018 (7)	-0.003 (5)	0.008 (5)
C72	0.137 (7)	0.102 (6)	0.127 (6)	-0.001 (5)	0.010 (6)	-0.049 (5)
S5′	0.0595 (13)	0.092 (3)	0.175 (4)	-0.0095 (18)	0.0015 (16)	-0.037 (3)

S6′	0.135 (5)	0.177 (6)	0.056 (2)	-0.021 (4)	0.000 (3)	-0.029(3)
S7′	0.122 (5)	0.152 (4)	0.057 (2)	0.019 (3)	0.024 (2)	-0.005(2)
S8′	0.159 (6)	0.146 (6)	0.137 (5)	-0.001 (4)	0.007 (3)	-0.083 (4)
C48′	0.182 (10)	0.106 (8)	0.129 (9)	-0.016 (8)	0.038 (8)	-0.048 (7)
C56′	0.163 (10)	0.179 (9)	0.089 (7)	-0.013 (8)	-0.005 (8)	-0.064 (6)
C64′	0.173 (9)	0.127 (8)	0.106 (8)	-0.023 (7)	0.009 (6)	0.013 (6)
C72′	0.178 (14)	0.166 (13)	0.180 (13)	0.000 (9)	-0.003 (9)	-0.056 (9)
01	0.0476 (11)	0.0799 (14)	0.0445 (11)	0.0093 (9)	-0.0129 (9)	-0.0113 (9)
O2	0.0602 (11)	0.0554 (11)	0.0418 (10)	-0.0062 (9)	-0.0020 (8)	-0.0172 (8)
O3	0.0394 (9)	0.0626 (11)	0.0409 (10)	-0.0054 (8)	0.0035 (8)	-0.0106 (8)
04	0.0515 (11)	0.0623 (12)	0.0476 (11)	-0.0014 (9)	-0.0024 (9)	-0.0056(9)
C1	0.0311 (12)	0.0451 (14)	0.0496 (15)	-0.0011 (10)	-0.0043 (11)	-0.0101 (11)
C2	0.0410 (14)	0.0534 (16)	0.0506 (16)	-0.0024 (12)	-0.0082(12)	-0.0160 (12)
C3	0.0381 (14)	0.0607 (17)	0.0433 (14)	0.0025 (12)	-0.0055 (11)	-0.0117 (13)
C4	0.0439 (14)	0.0442 (15)	0.0536 (16)	0.0030 (12)	-0.0050(12)	-0.0059(12)
C5	0.0381 (13)	0.0429 (14)	0.0500 (15)	0.0031 (11)	-0.0071 (11)	-0.0143 (12)
C6	0.0313 (12)	0.0483 (15)	0.0429 (14)	0.0001 (11)	-0.0041 (10)	-0.0110 (11)
C7	0.0507 (16)	0.079 (2)	0.0449 (16)	0.0031 (15)	-0.0125(13)	-0.0036(14)
C8	0.126 (3)	0.105(3)	0.066 (2)	-0.009(2)	-0.021(2)	0.012 (2)
C9	0.066 (2)	0.150 (4)	0.078(2)	-0.014(2)	-0.0329(19)	0.004 (2)
C10	0.107(3)	0.147 (4)	0.055(2)	0.019 (3)	-0.009(2)	-0.033(2)
C11	0.0506 (15)	0.0406 (14)	0.0527 (16)	-0.0048(12)	-0.0048(13)	-0.0171(12)
C12	0.0526 (16)	0.0503 (16)	0.0545 (16)	-0.0058(13)	0.0058 (13)	-0.0213(13)
C13	0.0592 (17)	0.0534 (16)	0.0524 (16)	-0.0065(13)	-0.0007(14)	-0.0210(13)
C14	0.0511 (16)	0.0656 (18)	0.0531 (16)	-0.0071(14)	-0.0069(13)	-0.0242(14)
C15	0.0513 (16)	0.0484(15)	0.0513 (16)	-0.0064(12)	0.0015 (13)	-0.0178(12)
C16	0.0523 (16)	0.0412 (14)	0.0448 (15)	-0.0061(12)	-0.0003(12)	-0.0138(11)
C17	0.074 (2)	0.085 (2)	0.0605 (19)	-0.0099(18)	-0.0001(17)	-0.0375(17)
C18	0.094 (6)	0.100 (8)	0.046 (4)	-0.006 (7)	0.012 (4)	-0.030 (5)
C19	0.118 (6)	0.102 (5)	0.100 (5)	-0.004(5)	-0.028(5)	-0.065(4)
C20	0.093 (5)	0.095 (6)	0.061 (5)	-0.002(5)	-0.017(4)	-0.029(5)
C18′	0.102 (7)	0.110 (9)	0.083 (7)	-0.019(7)	0.007 (5)	-0.041(7)
C19′	0.143(10)	0.117 (8)	0.101 (8)	-0.020(8)	0.001 (8)	-0.071(6)
C20′	0.096 (6)	0.108 (7)	0.069 (5)	-0.015 (6)	-0.019 (4)	-0.038(5)
C21	0.0399 (14)	0.0571 (17)	0.0487 (15)	-0.0077(12)	0.0011 (12)	-0.0156(12)
C22	0.0465 (15)	0.0551 (17)	0.0519 (16)	-0.0114 (13)	0.0041 (13)	-0.0057(13)
C23	0.0389 (14)	0.0682 (19)	0.0425 (14)	-0.0038 (13)	0.0006 (11)	-0.0105 (13)
C24	0.0389 (14)	0.0627 (18)	0.0449 (15)	0.0000 (12)	0.0012 (12)	-0.0172(13)
C25	0.0329 (13)	0.0538 (16)	0.0464 (15)	-0.0013 (11)	-0.0017 (11)	-0.0107(12)
C26	0.0306 (12)	0.0554 (16)	0.0407 (14)	-0.0043(11)	0.0049 (11)	-0.0083(12)
C27	0.0577 (18)	0.088 (2)	0.0436 (16)	-0.0090 (16)	0.0098 (14)	-0.0090(15)
C28	0.075 (5)	0.090 (6)	0.051 (4)	-0.001 (5)	0.007 (4)	0.015 (4)
C29	0.143 (8)	0.148 (9)	0.070 (6)	-0.033(7)	0.037 (6)	-0.033 (6)
C30	0.042 (3)	0.087 (6)	0.049 (4)	-0.005(4)	0.010 (3)	0.003 (4)
C28′	0.118 (10)	0.100 (9)	0.084 (8)	-0.001 (7)	0.015 (7)	0.005 (6)
C29′	0.110 (7)	0.120 (7)	0.064 (5)	-0.028(5)	0.030 (5)	-0.038(5)
C30′	0.083 (7)	0.112 (9)	0.085 (7)	0.008 (7)	0.018 (5)	0.001 (6)
C31	0.0368 (13)	0.0401(14)	0.0599 (17)	-0.0021(11)	-0.0015(12)	-0.0123(12)
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C32	0.0381 (14)	0.0443 (15)	0.0677 (18)	-0.0015 (12)	-0.0080 (13)	-0.0021 (13)
C33	0.0462 (15)	0.0424 (15)	0.0587 (17)	-0.0123 (12)	-0.0104 (13)	0.0012 (12)
C34	0.0380 (13)	0.0410 (14)	0.0570 (16)	-0.0083 (11)	0.0004 (12)	-0.0045 (12)
C35	0.0350 (13)	0.0339 (13)	0.0593 (16)	-0.0024 (10)	-0.0071 (12)	-0.0119 (12)
C36	0.0434 (14)	0.0355 (13)	0.0477 (15)	-0.0004 (11)	-0.0055 (12)	-0.0093 (11)
C37	0.0621 (19)	0.065 (2)	0.069 (2)	-0.0211 (16)	-0.0154 (16)	0.0133 (16)
C38	0.061 (4)	0.118 (6)	0.089 (5)	-0.018 (5)	0.000 (4)	0.039 (5)
C39	0.093 (5)	0.048 (3)	0.071 (4)	0.007 (3)	-0.021 (4)	0.007 (3)
C40	0.107 (7)	0.067 (4)	0.054 (4)	-0.006 (4)	-0.016 (4)	-0.004 (3)
C38′	0.095 (5)	0.107 (6)	0.061 (4)	0.005 (5)	-0.013 (4)	0.001 (4)
C39′	0.161 (7)	0.070 (5)	0.085 (5)	-0.021 (5)	0.000 (5)	0.012 (4)
C40′	0.065 (6)	0.108 (9)	0.089 (8)	-0.010 (6)	-0.021 (5)	0.015 (7)
C41	0.062 (2)	0.162 (4)	0.0470 (19)	-0.015 (2)	-0.0070 (16)	-0.011 (2)
C42	0.0555 (17)	0.071 (2)	0.0429 (15)	-0.0130 (15)	-0.0041 (13)	-0.0116 (14)
C43	0.071 (2)	0.069 (2)	0.083 (2)	0.0003 (18)	0.0100 (18)	-0.0301 (17)
C44	0.067 (2)	0.067 (2)	0.106 (3)	-0.0133 (17)	0.0039 (19)	-0.0374 (19)
C45	0.0644 (19)	0.0563 (19)	0.076 (2)	-0.0111 (16)	0.0012 (16)	-0.0114 (15)
C46	0.070 (2)	0.054 (2)	0.132 (3)	-0.0011 (17)	0.004 (2)	-0.030 (2)
C47	0.084 (3)	0.060 (2)	0.110 (3)	-0.0286 (19)	0.007 (2)	-0.0222 (19)
C49	0.099 (3)	0.061 (2)	0.0546 (18)	-0.0098 (17)	-0.0013 (17)	-0.0103 (15)
C50	0.0586 (17)	0.071 (2)	0.0445 (16)	-0.0104 (15)	-0.0009 (13)	-0.0068 (14)
C51	0.104 (3)	0.069 (2)	0.060 (2)	-0.0149 (19)	-0.0018 (19)	-0.0024 (17)
C52	0.101 (3)	0.103 (3)	0.050 (2)	-0.021 (2)	-0.0058 (18)	0.008 (2)
C53	0.076 (2)	0.107 (3)	0.0442 (18)	-0.013 (2)	-0.0002 (15)	-0.0153 (18)
C54	0.086 (2)	0.083 (2)	0.0519 (19)	-0.0030 (18)	-0.0057 (16)	-0.0177 (17)
C55	0.074 (2)	0.070 (2)	0.0438 (16)	0.0010 (16)	-0.0058 (14)	-0.0099 (14)
C57	0.0465 (16)	0.082 (2)	0.0534 (17)	0.0003 (15)	-0.0019 (13)	-0.0102 (15)
C58	0.0492 (16)	0.0563 (16)	0.0424 (15)	-0.0047 (13)	-0.0014 (12)	-0.0094 (12)
C59	0.0503 (17)	0.077 (2)	0.0464 (16)	0.0027 (14)	-0.0018 (13)	-0.0093 (14)
C60	0.0531 (17)	0.096 (2)	0.0527 (18)	0.0003 (16)	0.0019 (14)	-0.0193 (16)
C61	0.075 (2)	0.083 (2)	0.0451 (17)	-0.0056 (17)	-0.0005 (15)	-0.0204 (15)
C62	0.078 (2)	0.091 (2)	0.0457 (17)	-0.0085 (18)	-0.0139 (16)	-0.0142 (16)
C63	0.0510 (16)	0.074 (2)	0.0609 (19)	-0.0034 (14)	-0.0106 (14)	-0.0180 (15)
C65	0.0573 (18)	0.108 (3)	0.0528 (18)	0.0022 (18)	-0.0069 (15)	-0.0219 (17)
C66	0.066 (2)	0.087 (2)	0.0519 (18)	-0.0102 (18)	-0.0030 (15)	-0.0192 (17)
C67	0.159 (5)	0.109 (4)	0.104 (3)	-0.037 (3)	0.060 (3)	-0.031 (3)
C68	0.178 (5)	0.085 (3)	0.115 (4)	-0.014 (3)	0.039 (4)	-0.028 (3)
C69	0.092 (3)	0.099 (3)	0.066 (2)	0.002 (2)	-0.009 (2)	-0.036 (2)
C70	0.087 (3)	0.128 (4)	0.071 (2)	-0.010 (3)	0.018 (2)	-0.033 (2)
C71	0.093 (3)	0.085 (2)	0.072 (2)	-0.008 (2)	0.011 (2)	-0.0201 (19)

Geometric parameters (Å, °)

S1—C1	1.768 (3)	C23—C24	1.378 (4)	
S1—C35	1.779 (2)	C23—C27	1.526 (4)	
S2—C11	1.770 (3)	C24—C25	1.390 (3)	
S2—C5	1.777 (3)	C24—H24	0.9300	
S3—C15	1.772 (3)	C25—C26	1.390 (4)	

S3—C21	1.772 (3)	C27—C30′	1.445 (16)
S4—C25	1.773 (3)	C27—C28	1.454 (12)
S4—C31	1.773 (3)	C27—C29	1.510 (14)
S5—C45	1.762 (8)	C27—C29′	1.574 (12)
S5—C48	1.769 (8)	С27—С30	1.580 (10)
S6—C53	1.756 (9)	C27—C28′	1.683 (17)
S6—C56	1.816 (14)	C28—H28A	0.9600
S7—C64	1.800 (12)	C28—H28B	0.9600
S7—C61	1.811 (9)	C28—H28C	0.9600
S8—C69	1 773 (7)	C29—H29A	0 9600
\$8—C72	1 791 (11)	C29—H29B	0.9600
C48—H48A	0.9600	$C_{29}$ H29D	0.9600
$C_{48}$ HASB	0.9600	$C_{2}$ $H_{2}$ $C_{3}$ $H_{3}$ $A$	0.9600
$C_{48} = H_{48}C$	0.9000	C30 H30R	0.9000
$C_{40}$	0.9000	C30—1130B	0.9000
C50—H50A	0.9600		0.9600
С56—Н56В	0.9600	C28—H28D	0.9600
С56—Н56С	0.9600	C28'—H28E	0.9600
C64—H64A	0.9600	C28'—H28F	0.9600
C64—H64B	0.9600	C29'—H29D	0.9600
C64—H64C	0.9600	С29′—Н29Е	0.9600
C72—H72D	0.9600	C29′—H29F	0.9600
С72—Н72Е	0.9600	C30'—H30D	0.9600
C72—H72F	0.9600	C30'—H30E	0.9600
S5'—C48'	1.792 (19)	C30′—H30F	0.9600
S5'—C45	1.827 (17)	C31—C32	1.380 (3)
S6'—C56'	1.740 (14)	C31—C36	1.405 (3)
S6′—C53	1.787 (10)	C32—C33	1.388 (4)
S7′—C61	1.734 (10)	С32—Н32	0.9300
S7'—C64'	1.760 (13)	C33—C34	1.389 (3)
S8′—C69	1.756 (10)	C33—C37	1.532 (4)
S8'—C72'	1.812 (17)	C34—C35	1.387 (3)
C48′—H48D	0.9600	C34—H34	0.9300
C48′—H48E	0.9600	C35—C36	1.384 (3)
C48′—H48F	0.9600	C37—C38	1 416 (8)
C56'—H56D	0.9600	C37 - C40'	1 423 (16)
C56'—H56E	0.9600	$C_{37}$ $C_{39'}$	1.123(10) 1.437(9)
C56'—H56E	0.9600	$C_{37} - C_{40}$	1.497(9)
C64' H64D	0.9600	$C_{37}$ $C_{30}$	1.500(11) 1.678(7)
C64' = H64E	0.9000	$C_{37} = C_{39}$	1.078(7) 1.733(0)
C64' = H64E	0.9000	$C_{29} = H_{29} \Lambda$	1.733 (9)
$C_{04} = H_{04}$	0.9000	C30—II30A	0.9000
C72/_H/2A	0.9600	C38—H38B	0.9600
C72 H72B	0.9600		0.9600
C/2 - H/2C	0.9600	Сээ—НээА	0.9600
01	1.570 (3)	С39—Н39В	0.9600
01	1.375 (4)	С39—Н39С	0.9600
O2—C16	1.371 (3)	C40—H40A	0.9600
O2—C49	1.421 (3)	C40—H40B	0.9600
O3—C26	1.372 (3)	C40—H40C	0.9600

O3—C57	1.433 (3)	C38'—H38D	0.9600
O4—C36	1.376 (3)	С38′—Н38Е	0.9600
O4—C65	1.440 (4)	C38′—H38F	0.9600
C1—C2	1.379 (3)	C39′—H39D	0.9600
C1—C6	1.400 (3)	С39′—Н39Е	0.9600
C2—C3	1.396 (4)	C39′—H39F	0.9600
С2—Н2	0.9300	C40'—H40D	0.9600
C3—C4	1.373 (4)	C40′—H40E	0.9600
С3—С7	1.542 (4)	C40′—H40F	0.9600
C4—C5	1.387 (3)	C41—C42	1.482 (4)
C4—H4	0.9300	C41—H41A	0.9700
C5—C6	1.384 (3)	C41—H41B	0.9700
C7—C10	1.512 (5)	C42—C43	1.366 (4)
С7—С8	1.522 (5)	C42—C47	1.373 (4)
С7—С9	1.527 (4)	C43—C44	1.357 (4)
C8—H8A	0.9600	C43—H43	0.9300
C8—H8B	0.9600	C44—C45	1.345 (4)
C8—H8C	0.9600	C44—H44	0.9300
С9—Н9А	0.9600	C45—C46	1.357 (4)
С9—Н9В	0.9600	C46—C47	1.388 (5)
С9—Н9С	0.9600	C46—H46	0.9300
С10—Н10А	0.9600	С47—Н47	0.9300
C10—H10B	0.9600	C49—C50	1.489 (4)
C10—H10C	0.9600	C49—H49A	0.9700
C11—C12	1.383 (4)	C49—H49B	0.9700
C11—C16	1.393 (4)	C50—C55	1.371 (4)
C12-C13	1 390 (4)	C50—C51	1 382 (4)
C12—H12	0.9300	C51—C52	1.374 (5)
C13—C14	1.378 (4)	C51—H51	0.9300
C13—C17	1.533 (4)	C52—C53	1.361 (5)
C14—C15	1.395 (4)	C52—H52	0.9300
C14—H14	0.9300	C53—C54	1.385 (5)
C15—C16	1.386 (4)	C54—C55	1.383 (4)
C17—C20′	1.457 (14)	C54—H54	0.9300
C17—C18′	1.46(2)	C55—H55	0.9300
C17 - C19	1.534(11)	C57—C58	1 504 (4)
C17—C19′	1.566 (18)	C57—H57A	0.9700
C17 - C18	1 592 (18)	C57—H57B	0.9700
C17 - C20	1 624 (13)	C58—C59	1 375 (4)
C18—H18A	0.9600	C58—C63	1 386 (4)
C18—H18B	0.9600	$C_{59}$ $C_{60}$	1.300(1) 1.372(4)
C18 - H18C	0.9600	C59—H59	0.9300
C19—H19A	0.9600	C60-C61	1 388 (4)
C19—H19B	0.9600	C60—H60	0.9300
C19—H19C	0.9600	C61-C62	1 380 (4)
С20—Н20А	0.9600	C62 - C63	1 361 (4)
C20_H20B	0.9600	C62_H62	0.0300
C20 H20C	0.9600	C63 H63	0.0300
$C_{20} = 1120C$	0.2000	0051105	0.2500

# supporting information

C18′—H18D	0.9600	C65—C66	1.498 (4)
C18′—H18E	0.9600	С65—Н65А	0.9700
C18′—H18F	0.9600	С65—Н65В	0.9700
C19′—H19D	0.9600	C66—C67	1.354 (5)
C19′—H19E	0.9600	C66—C71	1.373 (5)
C19′—H19F	0.9600	C67—C68	1.402 (6)
C20′—H20D	0.9600	С67—Н67	0.9300
C20′—H20E	0.9600	C68—C69	1.325 (6)
C20′—H20F	0.9600	С68—Н68	0.9300
C21—C26	1.383 (4)	C69—C70	1.364 (5)
C21—C22	1.399 (4)	C70—C71	1.376 (5)
C22—C23	1.386 (4)	С70—Н70	0.9300
C22—H22	0.9300	С71—Н71	0.9300
C1—S1—C35	106.14 (11)	С27—С30—Н30В	109.5
C11—S2—C5	108.71 (11)	С27—С30—Н30С	109.5
C15—S3—C21	108.63 (12)	C27—C28′—H28D	109.5
C25—S4—C31	108.22 (11)	C27—C28′—H28E	109.5
C45—S5—C48	106.3 (4)	H28D—C28′—H28E	109.5
C53—S6—C56	100.8 (7)	C27—C28′—H28F	109.5
C64—S7—C61	100.0 (6)	H28D—C28'—H28F	109.5
C69—S8—C72	102.6 (6)	H28E—C28'—H28F	109.5
C48′—S5′—C45	82.1 (9)	C27—C29′—H29D	109.5
C56'—S6'—C53	102.5 (8)	С27—С29′—Н29Е	109.5
C61—S7′—C64′	107.7 (8)	H29D—C29′—H29E	109.5
C69—S8′—C72′	107.6 (11)	C27—C29′—H29F	109.5
S5'—C48'—H48D	109.5	H29D—C29′—H29F	109.5
S5'—C48'—H48E	109.5	H29E—C29′—H29F	109.5
H48D—C48′—H48E	109.5	C27—C30′—H30D	109.5
S5'—C48'—H48F	109.5	С27—С30′—Н30Е	109.5
H48D—C48′—H48F	109.5	H30D—C30′—H30E	109.5
H48E—C48′—H48F	109.5	C27—C30′—H30F	109.5
S6'—C56'—H56D	109.5	H30D—C30′—H30F	109.5
S6'—C56'—H56E	109.5	H30E—C30'—H30F	109.5
H56D—C56′—H56E	109.5	C32—C31—C36	120.3 (2)
S6'—C56'—H56F	109.5	C32—C31—S4	117.03 (18)
H56D—C56'—H56F	109.5	C36—C31—S4	122.17 (19)
H56E—C56'—H56F	109.5	C31—C32—C33	122.4 (2)
S7'—C64'—H64D	109.5	С31—С32—Н32	118.8
S7'—C64'—H64E	109.5	С33—С32—Н32	118.8
H64D—C64′—H64E	109.5	C32—C33—C34	116.4 (2)
S7'—C64'—H64F	109.5	C32—C33—C37	121.2 (2)
H64D—C64′—H64F	109.5	C34—C33—C37	122.5 (2)
H64E—C64′—H64F	109.5	C35—C34—C33	122.4 (2)
S8'—C72'—H72A	109.5	С35—С34—Н34	118.8
S8'—C72'—H72B	109.5	С33—С34—Н34	118.8
H72A—C72′—H72B	109.5	C36—C35—C34	120.5 (2)
S8'—C72'—H72C	109.5	C36—C35—S1	124.13 (19)

H72A—C72′—H72C	109.5	C34—C35—S1	115.11 (18)
H72B—C72′—H72C	109.5	O4—C36—C35	123.7 (2)
C6—O1—C41	124.3 (2)	O4—C36—C31	118.2 (2)
C16—O2—C49	114.5 (2)	C35—C36—C31	117.9 (2)
C26—O3—C57	113.88 (18)	C38—C37—C40′	128.2 (8)
C36—O4—C65	116.4 (2)	C38—C37—C39′	56.3 (6)
C2—C1—C6	120.1 (2)	C40′—C37—C39′	117.1 (7)
C2—C1—S1	117.5 (2)	C38—C37—C40	117.8 (7)
C6—C1—S1	122.04 (19)	C40′—C37—C40	25.5 (7)
C1—C2—C3	122.3 (2)	C39′—C37—C40	135.4 (5)
C1—C2—H2	118.8	C38—C37—C33	115.0 (4)
С3—С2—Н2	118.8	C40′—C37—C33	114.3 (7)
C4—C3—C2	116.4 (2)	C39′—C37—C33	110.9 (4)
C4—C3—C7	123.2 (2)	C40—C37—C33	110.3 (4)
C2—C3—C7	120.3 (3)	C38—C37—C39	106.5 (6)
C3—C4—C5	122.6 (2)	C40′—C37—C39	74.4 (6)
C3—C4—H4	118.7	C39′—C37—C39	52.7 (5)
С5—С4—Н4	118.7	C40—C37—C39	99.8 (4)
C6—C5—C4	120.4 (2)	C33—C37—C39	105.5 (3)
C6—C5—S2	123.38 (19)	C38—C37—C38′	45.7 (5)
C4—C5—S2	115.79 (18)	C40′—C37—C38′	105.0 (7)
O1—C6—C5	122.5 (2)	C39′—C37—C38′	101.7 (6)
O1—C6—C1	119.2 (2)	C40—C37—C38′	82.6 (5)
C5—C6—C1	118.0 (2)	C33—C37—C38′	106.2 (3)
C10—C7—C8	107.3 (3)	C39—C37—C38′	145.1 (4)
С10—С7—С9	110.5 (3)	С37—С38—Н38А	109.5
C8—C7—C9	108.6 (3)	С37—С38—Н38В	109.5
C10—C7—C3	110.8 (2)	С37—С38—Н38С	109.5
C8—C7—C3	111.5 (3)	С37—С39—Н39А	109.5
C9—C7—C3	108.1 (2)	С37—С39—Н39В	109.5
C7—C8—H8A	109.5	С37—С39—Н39С	109.5
C7—C8—H8B	109.5	С37—С40—Н40А	109.5
H8A—C8—H8B	109.5	С37—С40—Н40В	109.5
С7—С8—Н8С	109.5	С37—С40—Н40С	109.5
H8A—C8—H8C	109.5	C37—C38′—H38D	109.5
H8B—C8—H8C	109.5	С37—С38′—Н38Е	109.5
С7—С9—Н9А	109.5	H38D—C38′—H38E	109.5
С7—С9—Н9В	109.5	C37—C38′—H38F	109.5
Н9А—С9—Н9В	109.5	H38D—C38′—H38F	109.5
С7—С9—Н9С	109.5	H38E—C38′—H38F	109.5
Н9А—С9—Н9С	109.5	C37—C39′—H39D	109.5
H9B—C9—H9C	109.5	C37—C39′—H39E	109.5
C7—C10—H10A	109.5	H39D—C39′—H39E	109.5
C7—C10—H10B	109.5	C37—C39′—H39F	109.5
H10A—C10—H10B	109.5	H39D—C39′—H39F	109.5
C7—C10—H10C	109.5	H39E—C39′—H39F	109.5
H10A—C10—H10C	109.5	C37—C40′—H40D	109.5
H10B—C10—H10C	109.5	C37—C40′—H40E	109.5

C12—C11—C16	119.9 (2)	H40D—C40′—H40E	109.5
C12—C11—S2	116.2 (2)	C37—C40′—H40F	109.5
C16—C11—S2	123.2 (2)	H40D—C40′—H40F	109.5
C11—C12—C13	122.3 (2)	H40E—C40'—H40F	109.5
C11—C12—H12	118.8	O1—C41—C42	120.6 (3)
C13—C12—H12	118.8	01—C41—H41A	107.2
C14-C13-C12	116.9 (2)	C42—C41—H41A	107.2
C14-C13-C17	120.9(3)	01-C41-H41B	107.2
C12-C13-C17	122.2 (3)	C42—C41—H41B	107.2
C13 - C14 - C15	122.1(3)	H41A - C41 - H41B	106.8
C13 - C14 - H14	119.0	$C_{43}$ $C_{42}$ $C_{47}$	1151(3)
C15 - C14 - H14	119.0	$C_{43}$ $C_{42}$ $C_{41}$	123.2(3)
$C_{16}$ $-C_{15}$ $-C_{14}$	120.1.(2)	C47 - C42 - C41	123.2(3) 121.6(3)
C16-C15-S3	120.1(2) 124.2(2)	C44 - C43 - C42	121.0(3) 123.4(3)
C14-C15-S3	127.2(2) 1152(2)	C44 - C43 - H43	118.3
02-C16-C15	113.2(2) 120.7(2)	C42 - C43 - H43	118.3
02 - C16 - C11	120.7(2)	$C_{42} = C_{43} = \Pi_{43}$	120.4(3)
$C_{15} = C_{16} = C_{11}$	120.0(2) 118.7(2)	$C_{45} = C_{44} = C_{45}$	120.4 (5)
$C_{13} - C_{10} - C_{11}$	116.7(2) 117.0(10)	$C_{43} = C_{44} = H_{44}$	119.0
$C_{20} = C_{17} = C_{18}$	117.9(10) 114.7(6)	C43 - C44 - n44	119.0
$C_{20} = C_{17} = C_{13}$	114.7(0) 115.0(8)	$C_{44} = C_{43} = C_{40}$	119.1(3) 115.1(2)
$C_{18} = C_{17} = C_{13}$	115.0 (8)	C44 - C45 - S5	113.1(3) 125.7(2)
$C_{20} = C_{17} = C_{19}$	89.5 (0) 108.1 (7)	C40 - C43 - S3	123.7(3)
C18 - C17 - C19	108.1 (7)	C44 - C45 - S5'	122.0(0)
C13 - C17 - C19	108.0 (5)	$C46-C45-S5^{\circ}$	118.5 (6)
$C_{20} - C_{17} - C_{19}$	114.6 (8)	S5-C45-S5'	10.0(10)
	86.7 (8)	C45—C46—C47	119.6 (3)
$C13 - C17 - C19^{\prime}$	103.6 (7)	C45—C46—H46	120.2
C19—C17—C19 <sup>7</sup>	27.2 (6)	C47—C46—H46	120.2
C20'-C17-C18	110.2 (9)	C42—C47—C46	122.2 (3)
C18′—C17—C18	18.6 (9)	C42—C47—H47	118.9
C13—C17—C18	107.7 (7)	С46—С47—Н47	118.9
C19—C17—C18	126.3 (7)	O2—C49—C50	109.5 (3)
C19′—C17—C18	105.3 (9)	O2—C49—H49A	109.8
C20'—C17—C20	20.8 (7)	С50—С49—Н49А	109.8
C18′—C17—C20	107.1 (9)	O2—C49—H49B	109.8
C13—C17—C20	108.8 (5)	С50—С49—Н49В	109.8
C19—C17—C20	109.9 (6)	H49A—C49—H49B	108.2
C19′—C17—C20	134.2 (8)	C55—C50—C51	117.9 (3)
C18—C17—C20	94.8 (9)	C55—C50—C49	123.2 (3)
C17—C18—H18A	109.5	C51—C50—C49	118.9 (3)
C17—C18—H18B	109.5	C52—C51—C50	121.2 (4)
C17—C18—H18C	109.5	C52—C51—H51	119.4
С17—С19—Н19А	109.5	C50—C51—H51	119.4
C17—C19—H19B	109.5	C53—C52—C51	121.2 (3)
С17—С19—Н19С	109.5	С53—С52—Н52	119.4
C17—C20—H20A	109.5	C51—C52—H52	119.4
С17—С20—Н20В	109.5	C52—C53—C54	118.2 (3)
С17—С20—Н20С	109.5	C52—C53—S6	114.4 (4)

C17—C18′—H18D	109.5	C54—C53—S6	126.9 (5)
C17—C18′—H18E	109.5	C52—C53—S6'	120.3 (5)
H18D—C18′—H18E	109.5	C54—C53—S6'	120.9 (5)
C17—C18′—H18F	109.5	S6—C53—S6'	15.5 (5)
H18D—C18′—H18F	109.5	C55—C54—C53	120.7 (3)
H18E—C18′—H18F	109.5	С55—С54—Н54	119.7
C17—C19′—H19D	109.5	С53—С54—Н54	119.7
C17—C19′—H19E	109.5	C50—C55—C54	120.9 (3)
H19D—C19′—H19E	109.5	С50—С55—Н55	119.5
C17—C19′—H19F	109.5	С54—С55—Н55	119.5
H19D—C19′—H19F	109.5	03	109.3 (2)
H19E—C19'—H19F	109.5	O3—C57—H57A	109.8
C17—C20′—H20D	109.5	C58—C57—H57A	109.8
C17—C20′—H20E	109.5	O3—C57—H57B	109.8
$H_{20} - C_{20} - H_{20} F$	109.5	C58-C57-H57B	109.8
C17 - C20' - H20F	109.5	H57A-C57-H57B	109.0
$H_{20} - C_{20} - H_{20} F$	109.5	C59-C58-C63	118.2(2)
$H_{20F} = C_{20} = H_{20F}$	109.5	$C_{59} = C_{58} = C_{57}$	123.4(2)
$C_{26} = C_{21} = C_{22}$	120.6(2)	$C_{63}$ $C_{58}$ $C_{57}$	123.4(2) 1184(2)
$C_{26} = C_{21} = C_{22}$	123.6(2)	C60 - C59 - C58	120.4(2)
$C_{20} = C_{21} = S_{3}$	125.0(2) 1153(2)	C60 - C59 - C58	110.4 (5)
$C_{22} = C_{21} = S_{3}$	113.3(2) 121.2(3)	$C_{58}$ $C_{59}$ $H_{59}$	119.0
$C_{23} = C_{22} = C_{21}$	119.4	$C_{59} - C_{60} - C_{61}$	117.0 121.2(3)
$C_{23} = C_{22} = H_{22}$	119.4	$C_{59} = C_{60} = H_{60}$	110 4
$C_{24}$ $C_{23}$ $C_{22}$	117.4 117.2(2)	$C_{61}$ $C_{60}$ $H_{60}$	119.4
$C_{24} = C_{23} = C_{27}$	117.2(2) 1224(3)	C62 - C61 - C60	119.4
$C_{24} = C_{23} = C_{27}$	122.4(3) 120.4(3)	C62 - C61 - S7'	1201(3)
$C_{22} = C_{23} = C_{24} = C_{25}$	120.7(3)	C60-C61-S7'	120.1(4) 121 8 (4)
$C_{23}$ $C_{24}$ $H_{24}$	118 7	C62 - C61 - S7	121.0(1) 128.9(4)
$C_{25} = C_{24} = H_{24}$	118.7	C60 - C61 - S7	120.9(4) 1129(4)
$C_{26}$ $C_{25}$ $C_{24}$ $C_{26}$ $C_{25}$ $C_{24}$	119.6 (2)	S7'-C61-S7	102.7(1)
$C_{26} = C_{25} = S_{4}$	123 81 (19)	$C_{63}$ $C_{62}$ $C_{61}$	10.2(7) 1204(3)
$C_{24}$ $C_{25}$ $S_{4}$	1157(2)	C63 - C62 - H62	119.8
$03-C^{2}6-C^{2}1$	1205(2)	$C_{61}$ $C_{62}$ $H_{62}$	119.8
$03 - C^{26} - C^{25}$	120.8(2)	C62 - C63 - C58	117.0 121.6 (3)
$C_{21}$ $C_{26}$ $C_{25}$	120.0(2) 118.7(2)	C62 - C63 - H63	119.2
$C_{20} = C_{20} = C_{20}$	1247(8)	$C_{58}$ — $C_{63}$ —H63	119.2
$C_{30}' - C_{27} - C_{29}$	1084(8)	04-C65-C66	119.2 114 4 (2)
$C_{28} = C_{27} = C_{29}$	85 6 (7)	04-C65-H65A	108 7
$C_{30}' - C_{27} - C_{23}$	111.6(7)	C66—C65—H65A	108.7
$C_{28} - C_{27} - C_{23}$	112.3 (5)	O4-C65-H65B	108.7
$C_{29} - C_{27} - C_{23}$	110.4 (5)	C66—C65—H65B	108.7
$C_{30}' - C_{27} - C_{29}'$	79.6 (7)	H65A—C65—H65B	107.6
$C_{28} = C_{27} = C_{29}'$	112.4 (7)	C67 - C66 - C71	115.9 (3)
$C_{29} - C_{27} - C_{29}'$	31.4 (5)	C67—C66—C65	122.3 (3)
$C_{23}$ $C_{27}$ $C_{29}'$	111.6 (5)	C71—C66—C65	121.7(3)
$C_{30}' - C_{27} - C_{30}$	25.2 (6)	C66—C67—C68	122.2(4)
C28—C27—C30	108.9 (6)	C66—C67—H67	118.9
	(~)		

C29—C27—C30	130.7 (6)	С68—С67—Н67	118.9
C23—C27—C30	106.8 (4)	C69—C68—C67	120.8 (4)
C29′—C27—C30	104.2 (6)	С69—С68—Н68	119.6
C30'—C27—C28'	110.4 (9)	C67—C68—H68	119.6
C28—C27—C28′	21.6 (9)	C68—C69—C70	118.0 (4)
C29—C27—C28′	106.3 (8)	C68—C69—S8′	117.1 (6)
C23—C27—C28′	109.6 (7)	C70—C69—S8′	124.8 (5)
C29'—C27—C28'	129.6 (8)	C68—C69—S8	129.1 (5)
C30—C27—C28′	90.2 (7)	C70—C69—S8	112.8 (4)
C27—C28—H28A	109.5	S8′—C69—S8	12.7 (7)
C27—C28—H28B	109.5	C69—C70—C71	121.3 (4)
C27—C28—H28C	109.5	С69—С70—Н70	119.4
C27—C29—H29A	109.5	C71—C70—H70	119.4
C27—C29—H29B	109.5	C66-C71-C70	121.6 (4)
C27—C29—H29C	109.5	C66—C71—H71	119.2
C27—C30—H30A	109.5	C70-C71-H71	119.2
	107.0		119.2
C35 = S1 = C1 = C2	-128 12 (19)	C1 - S1 - C35 - C34	-1331(2)
$C_{35}$ $S_{1}$ $C_{1}$ $C_{2}$	58 3 (2)	$C_{65} - C_{4} - C_{36} - C_{35}$	70.1(3)
C6-C1-C2-C3	-11(4)	C65 - 04 - C36 - C31	-1151(3)
$S_1 - C_1 - C_2 - C_3$	-17475(19)	$C_{34}$ $C_{35}$ $C_{36}$ $C_{91}$	178.6(2)
C1 - C2 - C3 - C4	-1.7(4)	S1-C35-C36-O4	-7.8(4)
C1 - C2 - C3 - C7	1.7(4) 179 2 (2)	$C_{34}$ $C_{35}$ $C_{36}$ $C_{31}$	38(4)
$C_{2}^{2} - C_{3}^{2} - C_{4}^{2} - C_{5}^{5}$	$\frac{179.2}{2}(2)$	\$1_C35_C36_C31	177 35 (19)
$C_2 = C_3 = C_4 = C_5$	-1787(2)	$C_{32}^{32}$ $C_{31}^{31}$ $C_{36}^{36}$ $O_{4}^{4}$	-178.8(2)
$C_{1}^{3} = C_{1}^{4} = C_{2}^{5} = C_{1}^{5}$	176.7(2)	84 C31 C36 O4	0.2(3)
$C_{3} = C_{4} = C_{5} = C_{0}$	172.9(2)	$C_{32} = C_{31} = C_{30} = C_{4}$	-3.7(4)
$C_{3} - C_{4} - C_{5} - S_{2}$	-564(2)	84 C21 C26 C25	-175.60(10)
$C_{11} = S_2 = C_5 = C_6$	30.4(2)	$C_{22}$ $C_{23}$ $C_{27}$ $C_{28}$	175.09(19)
$C_{11} = S_2 = C_3 = C_4$	-70.4(4)	$C_{32} = C_{33} = C_{37} = C_{38}$	100.4(7)
C41 = 01 = C6 = C3	-79.4(4)	$C_{34} = C_{33} = C_{37} = C_{38}$	-11.2(8)
C41 = 01 = C6 = C1	100.7(3)	$C_{32} = C_{33} = C_{37} = C_{40}$	-28.2(8)
$C_4 - C_5 - C_6 - O_1$	-1/0.8(2)	$C_{34} = C_{33} = C_{37} = C_{40}$	152.5 (7)
$S_2 = C_3 = C_0 = 01$	10.8(3)	$C_{32} = C_{33} = C_{37} = C_{39}$	100.8(0)
$C_{4} = C_{5} = C_{6} = C_{1}$	-2.7(3)	$C_{34} = C_{33} = C_{37} = C_{39}$	-72.7(7)
$S_2 - C_3 - C_6 - C_1$	-1/5.14(18)	$C_{32} = C_{33} = C_{37} = C_{40}$	-55.5 (5)
$C_2 = C_1 = C_6 = O_1$	1/7.5(2)	$C_{34} = C_{33} = C_{37} = C_{40}$	125.0 (5)
SI = CI = C6 = OI	-9.1(3)	$C_{32} = C_{33} = C_{37} = C_{39}$	51.4 (4)
$C_2 = C_1 = C_6 = C_5$	3.3 (3)	$C_{34} = C_{33} = C_{37} = C_{39}$	-128.1(4)
SI_CI_C6_C5	1/6.64 (1/)	$C_{32} = C_{33} = C_{37} = C_{38}$	-143.4(4)
C4—C3—C7—C10	-127.8 (3)	C34—C33—C37—C38	37.0 (5)
C2—C3—C7—C10	51.3 (4)	C6—O1—C41—C42	-21.9 (5)
C4—C3—C7—C8	-8.4 (4)	01-C41-C42-C43	-80.9 (5)
C2—C3—C7—C8	170.7 (3)	O1—C41—C42—C47	102.2 (4)
C4—C3—C7—C9	110.9 (3)	C47—C42—C43—C44	3.1 (5)
C2—C3—C7—C9	-70.0 (3)	C41—C42—C43—C44	-174.0 (3)
C5—S2—C11—C12	139.5 (2)	C42—C43—C44—C45	-2.3 (6)
C5—S2—C11—C16	-49.6 (2)	C43—C44—C45—C46	0.8 (5)
C16—C11—C12—C13	-0.2 (4)	C43—C44—C45—S5	179.0 (5)

S2—C11—C12—C13	171.0 (2)	C43—C44—C45—S5'	-172.7 (11)
C11—C12—C13—C14	1.1 (4)	C48—S5—C45—C44	-177.8 (5)
C11—C12—C13—C17	-177.4 (3)	C48—S5—C45—C46	0.4 (8)
C12—C13—C14—C15	-1.5 (4)	C48—S5—C45—S5'	47 (6)
C17—C13—C14—C15	177.0 (3)	C48′—S5′—C45—C44	-153.6(7)
C13—C14—C15—C16	0.9 (4)	C48'—S5'—C45—C46	32.9 (13)
C13—C14—C15—S3	-171.2 (2)	C48'—S5'—C45—S5	-105(7)
C21—S3—C15—C16	46.1 (3)	C44—C45—C46—C47	-0.3 (6)
C21—S3—C15—C14	-142.2(2)	S5-C45-C46-C47	-178.3(5)
C49—O2—C16—C15	89.0 (3)	S5'-C45-C46-C47	173.4 (11)
C49 - 02 - C16 - C11	-92.3(3)	C43 - C42 - C47 - C46	-2.6(5)
C14-C15-C16-O2	178.7 (2)	C41 - C42 - C47 - C46	174.6(3)
S3-C15-C16-O2	-99(4)	C45-C46-C47-C42	13(6)
C14-C15-C16-C11	0.0(4)	$C_{16} = 0^{2} = C_{49} = C_{50}$	-1777(2)
S3-C15-C16-C11	1714(2)	02-C49-C50-C55	78(4)
$C_{12}$ $C_{11}$ $C_{16}$ $C_{10}$ $C$	-1791(2)	02 - C49 - C50 - C51	-1735(3)
$S_{2}^{2}$ $C_{11}^{11}$ $C_{16}^{16}$ $O_{2}^{2}$	103(3)	$C_{5} = C_{5} = C_{5$	-0.6(5)
$C_{12}$ $C_{11}$ $C_{16}$ $C_{15}$	-0.3(4)	$C_{49} = C_{50} = C_{51} = C_{52}$	-1794(3)
$S_{2}^{2}$	-170.97(19)	$C_{50} = C_{51} = C_{52} = C_{53}$	18(6)
$C_{14}$ $C_{13}$ $C_{17}$ $C_{20'}$	170(7)	$C_{51}$ $C_{52}$ $C_{53}$ $C_{54}$	-21(6)
C12 - C13 - C17 - C20'	-164.6(6)	$C_{51} = C_{52} = C_{53} = C_{54}$	-174.7(4)
$C_{12} = C_{13} = C_{17} = C_{20}$	158 5 (7)	$C_{51} = C_{52} = C_{53} = S_{6}$	169.2(4)
$C_{12}$ $C_{13}$ $C_{17}$ $C_{18}$	-23.1(8)	$C_{56} = 86 = C_{53} = C_{50}$	-173.0(5)
$C_{12} = C_{13} = C_{17} = C_{18}$	-80.8(5)	$C_{50} = S_{50} = C_{53} = C_{52}$	173.0(3)
$C_{12} = C_{13} = C_{17} = C_{19}$	00.8 (5) 07.6 (5)	$C_{50} = S_{50} = C_{53} = C_{54}$	-57(3)
$C_{12} = C_{13} = C_{17} = C_{19}$	-108.7(7)	$C_{50} = S_{50} = C_{53} = S_{50}$	150.9 (6)
$C_{14} = C_{13} = C_{17} = C_{19}$	100.7(7)	$C_{50} = 30 = C_{53} = C_{52}$	-38.0(8)
$C_{12} = C_{13} = C_{17} = C_{19}$	140.1(7)	$C_{50} = 30 = C_{53} = C_{54}$	-38.0(8)
C12 - C12 - C17 - C18	140.1(7)	$C_{50} = 0 = 0.053 = 0.050$	19(3)
C12 - C13 - C17 - C18	-41.5(7)	$C_{32} = C_{33} = C_{54} = C_{55}$	1.4(5)
C12 - C13 - C17 - C20	38.3 (0) 142.1 (C)	50-053-054-055	1/2.9 (4)
C12-C13-C17-C20	-143.1(0)	50 - 0.53 - 0.54 - 0.55	-169.8(4)
C15 - S3 - C21 - C26	49.1 (2)	$C_{51} = C_{50} = C_{55} = C_{54}$	-0.1(5)
C15 - S3 - C21 - C22	-138.9(2)	C49 - C50 - C55 - C54	1/8.6(3)
$C_{20} = C_{21} = C_{22} = C_{23}$	-0.2(4)	$C_{3} = C_{3} = C_{3} = C_{3} = C_{3}$	-0.3(5)
$S_{3}$ $C_{21}$ $C_{22}$ $C_{23}$	-1/2.4(2)	$C_{26} = 0_{3} = C_{57} = C_{58}$	-1/3.4(2)
$C_{21} = C_{22} = C_{23} = C_{24}$	-0.7(4)	03 - 057 - 058 - 059	1.3 (4)
$C_{21} = C_{22} = C_{23} = C_{27}$	1//.2(2)	03-05/-058-063	-1//.6(2)
C22—C23—C24—C25	1.0 (4)	C63—C58—C59—C60	1.1 (5)
C27—C23—C24—C25	-1/6.8(2)	C57—C58—C59—C60	-177.8(3)
C23—C24—C25—C26	-0.6 (4)	C58—C59—C60—C61	0.7 (5)
C23—C24—C25—S4	169.39 (19)	C59—C60—C61—C62	-2.4 (5)
C31—S4—C25—C26	-47.7 (2)	C59—C60—C61—S7'	175.8 (5)
C31—S4—C25—C24	142.83 (19)	C59—C60—C61—S7	-178.5 (4)
C57—O3—C26—C21	89.2 (3)	C64′—S7′—C61—C62	38.4 (9)
C57—O3—C26—C25	-92.4 (3)	C64'—S7'—C61—C60	-139.8 (7)
C22—C21—C26—O3	179.1 (2)	C64'—S7'—C61—S7	-171 (4)
S3—C21—C26—O3	-9.3 (3)	C64—S7—C61—C62	15.1 (9)
C22—C21—C26—C25	0.7 (4)	C64—S7—C61—C60	-169.4(5)

S3—C21—C26—C25	172.24 (18)	C64—S7—C61—S7′	-17 (3)
C24—C25—C26—O3	-178.8 (2)	C60—C61—C62—C63	2.3 (5)
S4—C25—C26—O3	12.1 (3)	S7'—C61—C62—C63	-176.0 (5)
C24—C25—C26—C21	-0.3 (4)	S7—C61—C62—C63	177.6 (5)
S4—C25—C26—C21	-169.42 (18)	C61—C62—C63—C58	-0.4 (5)
C24—C23—C27—C30'	80.8 (7)	C59—C58—C63—C62	-1.3 (5)
C22—C23—C27—C30′	-97.1 (7)	C57—C58—C63—C62	177.7 (3)
C24—C23—C27—C28	-133.6 (6)	C36—O4—C65—C66	81.3 (3)
C22—C23—C27—C28	48.6 (6)	O4—C65—C66—C67	-99.8 (4)
C24—C23—C27—C29	-39.9 (6)	O4—C65—C66—C71	81.0 (4)
C22—C23—C27—C29	142.3 (6)	C71—C66—C67—C68	1.7 (7)
C24—C23—C27—C29′	-6.3 (6)	C65—C66—C67—C68	-177.6 (4)
C22—C23—C27—C29′	175.9 (5)	C66—C67—C68—C69	2.2 (8)
C24—C23—C27—C30	107.0 (5)	C67—C68—C69—C70	-5.1 (7)
C22—C23—C27—C30	-70.8 (5)	C67—C68—C69—S8′	172.1 (6)
C24—C23—C27—C28′	-156.6 (7)	C67—C68—C69—S8	177.0 (5)
C22—C23—C27—C28′	25.6 (7)	C72'—S8'—C69—C68	15.4 (12)
C25—S4—C31—C32	128.5 (2)	C72'—S8'—C69—C70	-167.7 (10)
C25—S4—C31—C36	-59.2 (2)	C72'—S8'—C69—S8	-147 (3)
C36—C31—C32—C33	0.4 (4)	C72—S8—C69—C68	19.2 (8)
S4—C31—C32—C33	172.8 (2)	C72—S8—C69—C70	-158.8 (6)
C31—C32—C33—C34	2.8 (4)	C72—S8—C69—S8′	39 (2)
C31—C32—C33—C37	-176.8 (3)	C68—C69—C70—C71	4.2 (6)
C32—C33—C34—C35	-2.7 (4)	S8'—C69—C70—C71	-172.7 (5)
C37—C33—C34—C35	176.9 (3)	S8—C69—C70—C71	-177.6 (4)
C33—C34—C35—C36	-0.6 (4)	C67—C66—C71—C70	-2.6 (6)
C33—C34—C35—S1	-174.7 (2)	C65—C66—C71—C70	176.7 (3)
C1—S1—C35—C36	53.0 (2)	C69—C70—C71—C66	-0.3 (6)