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Crystal structure of 2-[9-(2-hydroxyphenyl)-1,8-dioxo-1,2,3,4,5,6,7,8,9,10decahydroacridin-10-yl]acetic acid

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The title compound, $C_{21}H_{21}NO_5$, crystallizes with two molecules in the asymmetric unit. In each molecule, the central 1,4-dihydropyridine ring adopts a shallow sofa conformations (with the C atom bearing the phenol ring as the flap), whereas the pendant cyclohexene rings both have twisted-boat conformations. Each molecule features an intramolecular $O-H\cdots O$ hydrogen bond, which closes an S(8) ring. In the crystal, the molecules are linked by $O-H\cdots O$, $C-H\cdots O$ and $C-H\cdots \pi$ interactions, forming a three-dimensional network.

Keywords: crystal structure; acridines; acetic acid; hydrogen bonding; C— $H \cdots \pi$ interactions.

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1. Related literature

For the industrial and pharmaceutical applications of acridine compounds, see: Szymanska *et al.* (2000); Fox & Chanon (1988); Groundwater & Munawar (1997); Cane *et al.* (1991).



2. Experimental

2.1. Crystal data

 $\begin{array}{l} C_{21}H_{21}NO_5\\ M_r = 367.39\\ Monoclinic, P2_1/n\\ a = 19.4735 \ (7) \ \mathring{A}\\ b = 8.9773 \ (4) \ \mathring{A}\\ c = 20.3414 \ (8) \ \mathring{A}\\ \beta = 91.619 \ (3)^\circ \end{array}$

2.2. Data collection

Agilent Xcalibur (Eos, Gemini)
diffractometer
Absorption correction: multi-scan
(CrysAlis PRO; Agilent, 2014)
$T_{\rm min} = 0.901, T_{\rm max} = 1.000$

2.3. Refinement

T.I.I. 4

$R[F^2 > 2\sigma(F^2)] = 0.079$	7 restraints
$vR(F^2) = 0.229$?
S = 1.01	$\Delta \rho_{\rm max} = 0.36 \ {\rm e} \ {\rm \AA}^{-3}$
1946 reflections	$\Delta \rho_{\rm min} = -0.36 \text{ e } \text{\AA}^{-3}$
199 parameters	

lable l			
Hydrogen-bond	geometry	(Å,	°).

$D - H \cdot \cdot \cdot A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdots A$
O4−H4···O2′	0.88 (2)	1.84 (3)	2.683 (3)	162 (3)
$O4' - H4' \cdots O2^i$	0.84 (3)	1.85 (3)	2.673 (2)	165 (3)
O5−H5···O1	0.83 (3)	1.80 (3)	2.616 (3)	168 (3)
$O5' - H5' \cdots O2'$	0.85 (4)	1.96 (4)	2.797 (3)	171 (4)
$C10-H10A\cdots O5'^{ii}$	0.97	2.60	3.380 (3)	138
$C14-H14B\cdots O1'^{ii}$	0.97	2.43	3.347 (3)	158
$C14' - H14D \cdots O2^{iii}$	0.97	2.36	3.241 (3)	151
$C17' - H17' \cdots O3'$	0.93	2.49	3.326 (3)	149
Symmetry codes: (i)	$x - \frac{1}{2}, -y + \frac{1}{2},$	$z - \frac{1}{2};$ (ii)	-x + 1, -y + 1, -x + 1, -x + 1, -y +	-z + 1; (iii)

 $-x + \frac{1}{2}, y - \frac{1}{2}, -z + \frac{3}{2}.$

 $V = 3554.7 (2) \text{ Å}^{3}$ Z = 8Mo K\alpha radiation $\mu = 0.10 \text{ mm}^{-1}$ T = 293 K $0.26 \times 0.22 \times 0.12 \text{ mm}$

33119 measured reflections 11946 independent reflections 6442 reflections with $I > 2\sigma(I)$ $R_{int} = 0.044$ Data collection: *CrysAlis PRO* (Agilent, 2014); cell refinement: *CrysAlis PRO*; data reduction: *CrysAlis PRO*; program(s) used to solve structure: *SHELXS2014* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL2014* (Sheldrick, 2015); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 2012); software used to prepare material for publication: *PLATON* (Spek, 2009).

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Supporting information for this paper is available from the IUCr electronic archives (Reference: HB7542).

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Crystal structure of 2-[9-(2-hydroxyphenyl)-1,8-dioxo-1,2,3,4,5,6,7,8,9,10-decahydroacridin-10-yl]acetic acid

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S1. Comment

Acridines and acridinium salts are highly fluorescent (Szymanska *et al.*, 2000), and as electron acceptors in photochemical processes (Fox & Chanon, 1988). In addition, acridine derivatives have found application as antimalarial, and antitumour agents (Groundwater & Munawar, 1997; Cane *et al.*, 1991). In this context, we report herein the synthesis and crystal structure of the title compound.

Fig. 1 shows two molecules (A and B) of the title compound in the asymmetric unit. In the molecules (A and B), the central 1,4-dihydropyridine rings (N1/C5–C9 and N1'/C5'–C9') of the 1,2,3,4,5,6,7,8,9,10-decahydroacridine ring systems (N1/C1–C13 and N1'/C1'–C13') adopt nearly a chair conformation [the puckering parameters are $Q_T = 0.261$ (2) Å, $\theta = 110.0$ (4) °, $\varphi = 360.0$ (5) ° and $Q_T = 0.337$ (2) Å, $\theta = 108.1$ (3) °, $\varphi = 4.8$ (4) °, repsectively], which the cyclohexene rings (C1–C6, C8–C13 and C1'–C6', C8'–C13') of the 1,2,3,4,5,6,7,8,9,10-decahydroacridine ring systems have a twisted-boat conformation [for molecule A, the puckering parameters are $Q_T = 0.470$ (4) Å, $\theta = 120.0$ (4) °, $\varphi = 286.9$ (4) ° and $Q_T = 0.460$ (3) Å, $\theta = 60.2$ (4) °, $\varphi = 196.0$ (4) °, repsectively, and for molecule B, $Q_T = 0.465$ (3) Å, $\theta = 120.0$ (4) °, $\varphi = 288.3$ (4) ° and $Q_T = 0.474$ (3) Å, $\theta = 61.3$ (4) °, $\varphi = 194.8$ (4) °, respectively].

In the crystal structure, adjacent molecules are connected by O—H···O, C—H···O and C—H··· π interactions, forming a three-dimensional network (Table 1, Fig. 2).

S2. Experimental

A mixture of ethyl 2-[9-(2-hydroxyphenyl)-1,8-dioxo-2,3,4,5,6,7,8,9-octahydroacridin- 10(1*H*)-yl) acetate (2.0 g, 0.005 mol) and a solution of NaOH (0.4 g, 0.01 mol) in (40 ml) ethanol was heated under reflux for 5 h. The reaction mixture was poured onto cold water and acidified with conc. HCl. The separated solid was filtered off, dried and crystallized from ethanol to afford dark red prisms. Yield: 93.5%, mp. 511–513 K. IR (λ_{max} , cm⁻¹): 3356 (OH_{acid}), 3119 (OH_{arom}), 3081 (CH_{arom}) 2969–2852 (CH_{aliph}), 1726 (C=O_{acid}), 1625 (C=O_{cyclic ketone}). ¹*H*-NMR (DMSO-d₆), δ p.p.m.: 13.39 (s, 1H, OH acid, disappeared by D₂O), 9.6 (s, 1H, OH_{arom}, disappeared by D₂O), 6.96–6.67 (m, 4H, CH_{arom}), 4.99 (s, 1H, CH), 4.72 (s, 2H, CH₂COOH), 2.91 (t, 2H, CH₂C=O), 2.45 (t, 2H, CH₂CO), 2.29 (t, 4H, 2CH₂-C=C), 1.96 (m, 2H, CH₂—CH₂—CH₂), 1.81 (m, 2H, CH₂—CH₂—CH₂). ¹³C-NMR (DMSO-d₆), δ p.p.m.: 197.62, 171.23, 156.26, 153.83, 132.81, 128.46, 127.77, 120.23, 117.26, 114.83, 47.93, 36.06, 25.99, 25.67.

S3. Refinement

The hydroxyl hydrogen atoms were found from a difference Fourier map and the O—H distances were restrained to 0.82 (2) Å, using the *DFIX* option and included in the structure-factor calculations with $U_{iso}(H) = 1.5U_{eq}(O)$. The remaining H atoms were placed in calculated positions with C—H = 0.93 - 0.98 Å, and refined as riding with $U_{iso}(H) = 1.5U_{eq}(O)$.





Figure 1

View of two molecules in the asymmetric unit of the title compound with displacement ellipsoids drawn at the 30% probability level.



Figure 2

View of the hydrogen bonding and packing of the title compounds down the [010] axis. H atoms not involved in hydrogen bonding have been omitted for clarity.

2-[9-(2-Hydroxyphenyl)-1,8-dioxo-1,2,3,4,5,6,7,8,9,10-decahydroacridin-10-yl]acetic acid

Crystal data

 $C_{21}H_{21}NO_5$ F(000) = 1552 $M_r = 367.39$ $D_{\rm x} = 1.373 {\rm Mg} {\rm m}^{-3}$ Monoclinic, $P2_1/n$ Mo *K* α radiation, $\lambda = 0.71073$ Å Hall symbol: -P 2yn Cell parameters from 4652 reflections $\theta = 3.8 - 27.1^{\circ}$ *a* = 19.4735 (7) Å $\mu = 0.10 \text{ mm}^{-1}$ b = 8.9773 (4) Å c = 20.3414 (8) Å T = 293 K $\beta = 91.619(3)^{\circ}$ Prism, dark red V = 3554.7 (2) Å³ $0.26 \times 0.22 \times 0.12 \text{ mm}$ Z = 8Data collection Agilent Xcalibur (Eos, Gemini) Absorption correction: multi-scan (CrysAlis PRO; Agilent, 2014) diffractometer $T_{\rm min} = 0.901, T_{\rm max} = 1.000$ Radiation source: Enhance (Mo) X-ray Source 33119 measured reflections Graphite monochromator Detector resolution: 16.0416 pixels mm⁻¹ 11946 independent reflections 6442 reflections with $I > 2\sigma(I)$ ω scans $R_{\rm int} = 0.044$

→ 13
•30
ts
n site location: mixed
$(F_o^2) + (0.092P)^2 + 1.4407P$
$P = (F_{\rm o}^2 + 2F_{\rm c}^2)/3$
< 0.001
.36 e Å ⁻³
0.36 e Å ⁻³

Special details

Geometry. Bond distances, angles *etc*. have been calculated using the rounded fractional coordinates. All su's are estimated from the variances of the (full) variance-covariance matrix. The cell e.s.d.'s are taken into account in the estimation of distances, angles and torsion angles

Refinement. Refinement on F^2 for ALL reflections except those flagged by the user for potential systematic errors. Weighted *R*-factors *wR* and all goodnesses of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The observed criterion of $F^2 > \sigma(F^2)$ is used only for calculating *-R*-factor-obs *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*-factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$
01	0.54951 (10)	1.0494 (2)	0.80712 (11)	0.0622 (7)
O2	0.46153 (8)	0.56884 (17)	0.87478 (8)	0.0433 (5)
03	0.36550 (14)	0.6857 (4)	0.58385 (13)	0.1172 (15)
O4	0.41939 (12)	0.6805 (4)	0.49001 (11)	0.0891 (9)
O5	0.44030 (11)	1.0230 (2)	0.87818 (9)	0.0565 (6)
N1	0.48876 (10)	0.6798 (2)	0.65174 (9)	0.0445 (6)
C1	0.54926 (12)	1.0057 (3)	0.75006 (15)	0.0496 (8)
O1′	0.39287 (9)	0.2869 (3)	0.52414 (10)	0.0675 (8)
C2	0.59167 (17)	1.0827 (4)	0.69950 (18)	0.0732 (13)
O2′	0.29880 (9)	0.7291 (2)	0.42658 (10)	0.0601 (7)
C3	0.5597 (2)	1.0692 (4)	0.63282 (18)	0.0815 (15)
O3′	0.10134 (9)	0.1149 (2)	0.42055 (10)	0.0653 (7)
C4	0.54754 (17)	0.9082 (3)	0.61352 (15)	0.0661 (10)
O4′	-0.00242 (8)	0.1429 (2)	0.46142 (8)	0.0472 (5)
C5	0.51323 (12)	0.8215 (3)	0.66776 (12)	0.0446 (7)
O5′	0.37299 (12)	0.5356 (3)	0.34753 (12)	0.0773 (9)
C6	0.50975 (11)	0.8746 (2)	0.72947 (11)	0.0401 (7)
C7	0.46943 (10)	0.7948 (2)	0.78090 (10)	0.0336 (6)
C8	0.46571 (10)	0.6316 (2)	0.76357 (10)	0.0341 (6)
С9	0.47006 (11)	0.5828 (2)	0.70101 (10)	0.0366 (6)
C10	0.45820 (13)	0.4225 (3)	0.68218 (12)	0.0473 (8)
C11	0.42648 (14)	0.3332 (3)	0.73625 (13)	0.0524 (8)
C12	0.46099 (16)	0.3626 (3)	0.80162 (13)	0.0533 (8)
C13	0.46154 (10)	0.5261 (2)	0.81698 (11)	0.0360 (6)
C14	0.48528 (14)	0.6324 (3)	0.58306 (12)	0.0538 (9)
C15	0.41689 (17)	0.6716 (4)	0.55438 (14)	0.0623 (10)

C16	0.39868 (11)	0.8636 (2)	0.78994 (10)	0.0355 (6)
C17	0.34257 (12)	0.8207 (3)	0.75127 (12)	0.0479 (8)
C18	0.27772 (14)	0.8762 (4)	0.76125 (15)	0.0654 (10)
C19	0.26799 (16)	0.9772 (4)	0.81090 (16)	0.0682 (11)
C20	0.32242 (17)	1.0251 (3)	0.84917 (14)	0.0609 (10)
C21	0.38832 (13)	0.9711 (3)	0.83864 (11)	0.0438 (7)
N1′	0.15357 (8)	0.3463 (2)	0.49752 (8)	0.0362(5)
C1′	0.33538(12)	0.2426(3)	0.53659(12)	0.0468(8)
C2'	0 32463 (16)	0.1296(4)	0 58950 (16)	0.0689(11)
C3′	0.26161 (16)	0.1290(1) 0.0409(4)	0 57678 (18)	0.0716 (11)
C4'	0.19809 (13)	0.0409(4) 0.1389(3)	0.57070(10)	0.0491 (8)
C5′	0.19007(13) 0.21077(11)	0.1505(3)	0.50772(12) 0.52069(10)	0.0491(6)
C5 C6'	0.21077(11) 0.27448(10)	0.2031(2) 0.3044(2)	0.52009(10) 0.50276(10)	0.0360(0)
C0	0.27448(10) 0.28481(10)	0.3044(2) 0.4107(2)	0.30270(10) 0.45054(10)	0.0301(0)
$C^{\prime\prime}$	0.26461(10) 0.22602(10)	0.4197(2)	0.45034(10) 0.45228(10)	0.0303(0)
	0.22693 (10)	0.5304(2)	0.45558(10) 0.4(078(10))	0.0352(6)
C9 C10/	0.16270 (10)	0.4855(2)	0.46978 (10)	0.0330(0)
	0.10140 (11)	0.5844 (3)	0.460/5 (11)	0.0442(7)
CII'	0.11568 (13)	0.7190 (3)	0.41893 (14)	0.0550 (9)
C12'	0.18185 (14)	0.7926 (3)	0.43997 (15)	0.0580 (9)
C13'	0.24005 (12)	0.6846 (3)	0.43923 (11)	0.0428 (7)
C14′	0.08462 (11)	0.2878 (3)	0.50771 (11)	0.0412 (7)
C15′	0.06362 (11)	0.1735 (2)	0.45782 (11)	0.0382 (6)
C16′	0.28966 (11)	0.3533 (3)	0.38153 (11)	0.0422 (7)
C17′	0.24941 (14)	0.2339 (4)	0.36209 (13)	0.0594 (9)
C18′	0.25191 (18)	0.1744 (5)	0.29965 (15)	0.0773 (13)
C19′	0.29600 (19)	0.2327 (5)	0.25536 (15)	0.0817 (13)
C20′	0.33619 (17)	0.3501 (4)	0.27253 (14)	0.0710 (13)
C21′	0.33296 (13)	0.4147 (3)	0.33476 (13)	0.0538 (9)
H2A	0.59640	1.18720	0.71090	0.0880*
H2B	0.63720	1.03910	0.69970	0.0880*
H3A	0.58940	1.11560	0.60120	0.0980*
H3B	0.51620	1.12200	0.63150	0.0980*
H4	0.3763 (10)	0.686 (4)	0.4766 (17)	0.0850*
H4A	0.59110	0.86180	0.60400	0.0790*
H4B	0.51870	0.90450	0.57390	0.0790*
Н5	0.4779 (12)	1.025 (4)	0.8603 (16)	0.0850*
H7	0.49510	0.80370	0.82280	0.0400*
H10A	0.50170	0.37770	0.67120	0.0570*
H10B	0.42820	0.41860	0.64330	0.0570*
HIIA	0.37810	0.35810	0.73850	0.0630*
H11B	0.42990	0.22800	0.72610	0.0630*
H12A	0.50780	0.32580	0.80130	0.0640*
H12B	0.43700	0.30960	0.83560	0.0640*
H14A	0 49240	0.52570	0.58030	0.0640*
H14R	0.52100	0.68150	0 55880	0.0640*
H17	0 34880	0.75250	0.71760	0.0570*
H18	0.24080	0.84560	0 73460	0.0780*
нто H10	0.24000	1 01210	0.75400	0.0700
1117	0.22410	1.01310	0.01000	0.0620

H20	0.31550	1.09410	0.88240	0.0730*
H2′1	0.36400	0.06330	0.59220	0.0830*
H2′2	0.32130	0.18000	0.63150	0.0830*
H3′1	0.25500	-0.02650	0.61330	0.0860*
H4′	-0.013 (2)	0.088 (4)	0.4291 (15)	0.1160*
H3′2	0.26720	-0.01870	0.53750	0.0860*
H5′	0.353 (2)	0.590 (4)	0.3751 (18)	0.1160*
H4′1	0.16000	0.07900	0.55100	0.0590*
H4′2	0.18560	0.17920	0.61000	0.0590*
H7′	0.32790	0.47230	0.46090	0.0440*
H10C	0.08660	0.61730	0.50350	0.0530*
H10D	0.06410	0.52780	0.44040	0.0530*
H11C	0.11810	0.68890	0.37330	0.0660*
H11D	0.07830	0.78970	0.42240	0.0660*
H12C	0.19110	0.87480	0.41060	0.0700*
H12D	0.17770	0.83260	0.48400	0.0700*
H14C	0.05200	0.36940	0.50590	0.0490*
H14D	0.08310	0.24390	0.55120	0.0490*
H17′	0.21970	0.19230	0.39200	0.0710*
H18′	0.22370	0.09470	0.28780	0.0930*
H19′	0.29840	0.19180	0.21350	0.0980*
H20′	0.36650	0.38840	0.24230	0.0850*

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
01	0.0625 (12)	0.0388 (10)	0.0849 (14)	-0.0124 (9)	-0.0024 (10)	-0.0031 (10)
O2	0.0532 (9)	0.0330 (8)	0.0441 (8)	0.0069 (7)	0.0067 (7)	0.0040 (7)
03	0.0716 (16)	0.201 (4)	0.0788 (16)	0.0340 (19)	-0.0036 (13)	-0.010 (2)
04	0.0745 (15)	0.130 (2)	0.0619 (13)	-0.0260 (16)	-0.0121 (11)	0.0250 (14)
05	0.0814 (13)	0.0385 (9)	0.0495 (10)	-0.0029 (10)	0.0027 (9)	-0.0070 (8)
N1	0.0530 (11)	0.0409 (11)	0.0402 (10)	0.0023 (9)	0.0120 (8)	0.0023 (8)
C1	0.0378 (12)	0.0308 (12)	0.0806 (18)	0.0008 (10)	0.0074 (11)	0.0099 (12)
01′	0.0364 (9)	0.0949 (17)	0.0712 (12)	0.0032 (10)	0.0009 (8)	0.0210 (11)
C2	0.0665 (19)	0.0437 (16)	0.111 (3)	-0.0115 (14)	0.0289 (18)	0.0119 (16)
O2′	0.0464 (10)	0.0474 (11)	0.0862 (13)	-0.0130 (8)	-0.0034 (9)	0.0174 (10)
C3	0.102 (3)	0.0479 (17)	0.097 (3)	-0.0075 (17)	0.048 (2)	0.0218 (17)
O3′	0.0486 (10)	0.0677 (13)	0.0806 (13)	-0.0091 (9)	0.0210 (9)	-0.0326 (11)
C4	0.0743 (19)	0.0516 (17)	0.0743 (18)	0.0038 (15)	0.0354 (15)	0.0169 (14)
O4′	0.0376 (8)	0.0464 (10)	0.0579 (10)	-0.0082 (7)	0.0069 (7)	-0.0111 (8)
C5	0.0420 (12)	0.0351 (12)	0.0575 (14)	0.0033 (10)	0.0141 (10)	0.0122 (10)
O5′	0.0692 (13)	0.0725 (16)	0.0921 (16)	-0.0095 (12)	0.0374 (11)	0.0162 (12)
C6	0.0364 (11)	0.0285 (10)	0.0558 (13)	0.0020 (9)	0.0093 (9)	0.0064 (9)
C7	0.0352 (10)	0.0258 (10)	0.0398 (10)	-0.0001 (8)	0.0031 (8)	0.0020 (8)
C8	0.0320 (10)	0.0264 (10)	0.0441 (11)	0.0012 (8)	0.0062 (8)	0.0020 (8)
C9	0.0349 (10)	0.0320 (11)	0.0430 (11)	0.0026 (9)	0.0055 (8)	0.0022 (9)
C10	0.0545 (14)	0.0370 (12)	0.0507 (13)	0.0011 (11)	0.0063 (10)	-0.0064 (10)
C11	0.0601 (15)	0.0346 (13)	0.0624 (15)	-0.0088 (11)	0.0025 (12)	-0.0014 (11)

C12	0.0791 (18)	0.0262 (11)	0.0546 (14)	-0.0015 (12)	0.0040 (12)	0.0034 (10)
C13	0.0316 (10)	0.0284 (10)	0.0482 (12)	0.0025 (8)	0.0054 (8)	0.0035 (9)
C14	0.0625 (16)	0.0557 (16)	0.0435 (13)	0.0037 (13)	0.0095 (11)	0.0027 (11)
C15	0.0685 (19)	0.070 (2)	0.0484 (15)	-0.0049 (16)	0.0012 (13)	0.0032 (13)
C16	0.0408 (11)	0.0287 (10)	0.0375 (10)	0.0056 (9)	0.0088 (8)	0.0046 (8)
C17	0.0428 (12)	0.0545 (15)	0.0466 (12)	0.0086 (11)	0.0054 (10)	-0.0047 (11)
C18	0.0434 (14)	0.086 (2)	0.0669 (17)	0.0169 (15)	0.0031 (12)	0.0012 (16)
C19	0.0555 (17)	0.072 (2)	0.078 (2)	0.0292 (16)	0.0182 (15)	0.0098 (16)
C20	0.082 (2)	0.0421 (14)	0.0599 (16)	0.0219 (14)	0.0268 (14)	0.0026 (12)
C21	0.0616 (14)	0.0294 (11)	0.0409 (11)	0.0049 (10)	0.0095 (10)	0.0052 (9)
N1′	0.0292 (8)	0.0374 (10)	0.0422 (9)	-0.0049 (7)	0.0069 (7)	-0.0046 (7)
C1′	0.0410 (12)	0.0535 (15)	0.0459 (12)	0.0038 (11)	0.0018 (9)	0.0020 (11)
C2′	0.0591 (17)	0.075 (2)	0.0720 (19)	0.0043 (16)	-0.0084 (14)	0.0261 (16)
C3′	0.0713 (19)	0.0569 (18)	0.086 (2)	-0.0039 (15)	-0.0069 (16)	0.0285 (16)
C4′	0.0536 (14)	0.0469 (14)	0.0470 (13)	-0.0098 (12)	0.0071 (10)	0.0056 (11)
C5′	0.0376 (11)	0.0336 (11)	0.0369 (10)	-0.0030 (9)	0.0050 (8)	-0.0028 (8)
C6′	0.0345 (10)	0.0365 (11)	0.0375 (10)	0.0010 (9)	0.0046 (8)	-0.0014 (8)
C7′	0.0286 (9)	0.0361 (11)	0.0449 (11)	-0.0009 (9)	0.0040 (8)	0.0021 (9)
C8′	0.0315 (10)	0.0346 (11)	0.0395 (10)	-0.0018 (8)	0.0023 (8)	-0.0017 (8)
C9′	0.0326 (10)	0.0350 (11)	0.0334 (10)	-0.0015 (8)	0.0025 (7)	-0.0066 (8)
C10′	0.0339 (11)	0.0530 (14)	0.0458 (12)	0.0058 (10)	0.0029 (9)	-0.0017 (10)
C11′	0.0497 (14)	0.0535 (16)	0.0618 (15)	0.0157 (12)	0.0008 (11)	0.0033 (12)
C12′	0.0601 (16)	0.0362 (13)	0.0775 (18)	0.0065 (12)	-0.0011 (13)	-0.0008 (12)
C13′	0.0394 (12)	0.0369 (12)	0.0519 (13)	-0.0039 (10)	-0.0029 (9)	0.0011 (10)
C14′	0.0305 (10)	0.0420 (12)	0.0517 (12)	-0.0055 (9)	0.0109 (9)	-0.0070 (10)
C15′	0.0343 (10)	0.0329 (11)	0.0478 (12)	-0.0022 (9)	0.0065 (9)	-0.0018 (9)
C16′	0.0328 (10)	0.0492 (14)	0.0452 (12)	0.0106 (10)	0.0112 (9)	0.0049 (10)
C17′	0.0534 (15)	0.0712 (19)	0.0543 (15)	-0.0054 (14)	0.0167 (12)	-0.0141 (13)
C18′	0.074 (2)	0.098 (3)	0.0604 (17)	-0.0054 (19)	0.0126 (15)	-0.0292 (17)
C19′	0.087 (2)	0.108 (3)	0.0509 (17)	0.018 (2)	0.0158 (16)	-0.0081 (18)
C20′	0.0696 (19)	0.093 (3)	0.0521 (16)	0.0293 (19)	0.0298 (14)	0.0192 (16)
C21′	0.0456 (13)	0.0590 (17)	0.0575 (15)	0.0118 (12)	0.0157 (11)	0.0162 (12)

Geometric parameters (Å, °)

01—C1	1.225 (4)	C11—H11A	0.9700
O2—C13	1.237 (3)	C11—H11B	0.9700
O3—C15	1.188 (4)	C12—H12A	0.9700
O4—C15	1.314 (4)	C12—H12B	0.9700
O5—C21	1.357 (3)	C14—H14A	0.9700
N1—C5	1.394 (3)	C14—H14B	0.9700
N1—C9	1.384 (3)	C17—H17	0.9300
N1-C14	1.460 (3)	C18—H18	0.9300
O4—H4	0.88 (2)	C19—H19	0.9300
O5—H5	0.83 (3)	C20—H20	0.9300
C1—C6	1.461 (3)	C1′—C6′	1.463 (3)
C1—C2	1.505 (4)	C1′—C2′	1.498 (4)
01′—C1′	1.221 (3)	C2'—C3'	1.480 (5)

C2—C3	1.481 (5)	C3′—C4′	1.525 (4)
O2'—C13'	1.246 (3)	C4'—C5'	1.508 (3)
C3—C4	1.515 (5)	C5'—C6'	1.350 (3)
O3'—C15'	1.193 (3)	C6'—C7'	1.501 (3)
C4—C5	1.520 (4)	C7'—C16'	1.531 (3)
O4'—C15'	1.319 (3)	C7'—C8'	1.505 (3)
C5—C6	1.346 (3)	C8'—C13'	1.438 (3)
O5'—C21'	1.357 (4)	C8′—C9′	1.365 (3)
C6—C7	1.507 (3)	C9'—C10'	1.496 (3)
C7—C16	1.526 (3)	C10′—C11′	1.508 (4)
C7—C8	1.508 (3)	C11′—C12′	1.500 (4)
C8—C9	1.351 (3)	C12'—C13'	1.492 (4)
C8-C13	1 445 (3)	C14′—C15′	1 492 (3)
C9—C10	1 505 (3)	C16'-C21'	1.192(3)
C10—C11	1 507 (4)	C16' - C17'	1 379 (4)
C11-C12	1 496 (4)	C17'-C18'	1.379(1) 1 380(4)
C12 - C13	1.501 (3)	C18'-C19'	1.366(5)
$C_{12} = C_{13}$	1.301(3) 1 481(4)	$C_{10} = C_{10}$	1.300(5) 1.353(5)
$C_{14} = C_{15}$	1.401(4) 1.282(2)	$C_{19} = C_{20}$	1.335(3) 1.305(4)
C16 C21	1.303(3)	$C_{20} = C_{21}$	0.0700
C10 - C21	1.402(3)	$C_2 - \pi_2 T$	0.9700
C17 - C18	1.378(4)	$C_2 - \Pi_2 Z$	0.9700
C18—C19	1.3/4(3)		0.9700
C19—C20	1.367 (4)	C3'—H3'2	0.9700
C20—C21	1.394 (4)	C4'—H4'1	0.9700
NI'	1.402 (3)	C4'—H4'2	0.9700
N1′—C9′	1.383 (3)	С7'—Н7'	0.9800
N1'—C14'	1.462 (3)	C10′—H10C	0.9700
C2—H2A	0.9700	C10'—H10D	0.9700
C2—H2B	0.9700	C11′—H11C	0.9700
С3—НЗА	0.9700	C11′—H11D	0.9700
С3—Н3В	0.9700	C12′—H12C	0.9700
C4—H4A	0.9700	C12'—H12D	0.9700
C4—H4B	0.9700	C14′—H14C	0.9700
O4'—H4'	0.84 (3)	C14'—H14D	0.9700
O5'—H5'	0.85 (4)	C17'—H17'	0.9300
С7—Н7	0.9800	C18'—H18'	0.9300
C10—H10B	0.9700	С19'—Н19'	0.9300
C10—H10A	0.9700	С20'—Н20'	0.9300
C5—N1—C9	120.01 (18)	C17—C18—H18	120.00
C5—N1—C14	119.74 (19)	С20—С19—Н19	120.00
C9—N1—C14	120.22 (18)	С18—С19—Н19	120.00
C15—O4—H4	105 (2)	С19—С20—Н20	120.00
С21—О5—Н5	114 (2)	C21—C20—H20	120.00
C2—C1—C6	118.0 (3)	C2'—C1'—C6'	117.8 (2)
O1—C1—C2	120.9 (3)	O1'—C1'—C2'	121.1 (2)
O1—C1—C6	121.2 (2)	O1'—C1'—C6'	121.0 (2)
C1—C2—C3	111.3 (3)	C1'—C2'—C3'	111.8 (3)

C2—C3—C4	112.0 (3)	C2'—C3'—C4'	112.1 (3)
C3—C4—C5	111.7 (3)	C3'—C4'—C5'	111.3 (2)
N1—C5—C4	116.9 (2)	N1′—C5′—C4′	117.47 (19)
N1—C5—C6	121.0 (2)	N1′—C5′—C6′	120.06 (17)
C4—C5—C6	122.0 (2)	C4′—C5′—C6′	122.42 (19)
C1—C6—C5	120.8 (2)	C1'—C6'—C5'	120.84 (19)
C5—C6—C7	121.33 (19)	C5'—C6'—C7'	120.94 (18)
C1—C6—C7	117.7 (2)	C1'—C6'—C7'	118.12 (18)
C8—C7—C16	112.57 (16)	C8'—C7'—C16'	110.98 (17)
C6-C7-C16	112 41 (16)	C6'-C7'-C16'	113 18 (17)
C6-C7-C8	108 79 (16)	C6' - C7' - C8'	108.23(16)
C7 - C8 - C9	122 10 (17)	C7' - C8' - C9'	120.39 (16)
C7 - C8 - C13	122.10(17) 117.66(17)	C7' - C8' - C13'	119 37 (18)
$C_{1}^{0} = C_{1}^{0} = C_{1}^{0}$	117.00(17) 120.13(17)	C' = C' = C'' = C''	119.37(18) 120.24(18)
N1 C9 C8	120.13(17) 120.19(17)	N1' - C0' - C1'	110 77 (17)
$C_{8} = C_{9} = C_{8}$	120.19(17) 122.45(18)	N1 - C3 - C8	119.77(17) 121.81(18)
$C_{0} = C_{0} = C_{10}$	122.43(18)	$C_{0} = C_{0} = C_{10}$	121.01(18) 119.29(19)
NI = C9 = C10	117.31(10) 112.7(2)	NI = C9 = C10	110.38 (18)
	112.7(2)		112.74 (18)
	111.8 (2)	$C10^{}$ $C12^{}$ $C12^{}$ $C12^{}$	111.3 (2)
	111.0(2)	$C11^{2}$ $C12^{2}$ $C13^{2}$	111.0 (2)
02-013-012	120.08 (19)	$02^{2}-013^{2}-012^{2}$	119.7 (2)
02	120.85 (17)	02'-013'-08'	121.3 (2)
C8—C13—C12	118.99 (19)	C8'-C13'-C12'	119.0 (2)
N1—C14—C15	108.9 (2)	N1'—C14'—C15'	112.69 (18)
O3—C15—C14	126.0 (3)	O3'—C15'—C14'	125.0 (2)
O4—C15—C14	110.4 (3)	O4'—C15'—C14'	110.75 (18)
O3—C15—O4	123.5 (3)	O3'—C15'—O4'	124.2 (2)
C17—C16—C21	117.8 (2)	C17'—C16'—C21'	117.3 (2)
C7—C16—C17	121.36 (18)	C7'—C16'—C17'	121.1 (2)
C7—C16—C21	120.82 (19)	C7'—C16'—C21'	121.6 (2)
C16—C17—C18	121.9 (2)	C16'—C17'—C18'	122.0 (3)
C17—C18—C19	119.5 (3)	C17'—C18'—C19'	119.9 (4)
C18—C19—C20	120.4 (3)	C18′—C19′—C20′	119.9 (3)
C19—C20—C21	120.4 (3)	C19′—C20′—C21′	121.2 (3)
C16—C21—C20	120.0 (2)	C16'—C21'—C20'	119.7 (3)
O5-C21-C16	122.4 (2)	O5'—C21'—C16'	122.5 (2)
O5—C21—C20	117.6 (2)	O5'—C21'—C20'	117.8 (3)
C5'—N1'—C9'	119.76 (16)	C1′—C2′—H2′1	109.00
C5'—N1'—C14'	119.33 (18)	C1′—C2′—H2′2	109.00
C9'—N1'—C14'	120.74 (17)	C3'—C2'—H2'1	109.00
C3—C2—H2B	109.00	C3'—C2'—H2'2	109.00
H2A—C2—H2B	108.00	H2'1—C2'—H2'2	108.00
C1—C2—H2A	109.00	C2'—C3'—H3'1	109.00
C1—C2—H2B	109.00	C2'—C3'—H3'2	109.00
C3—C2—H2A	109.00	C4′—C3′—H3′1	109.00
C2—C3—H3A	109.00	C4′—C3′—H3′2	109.00
C2—C3—H3B	109.00	H3'1—C3'—H3'2	108.00
C4—C3—H3A	109.00	C3'—C4'—H4'1	109.00

С4—С3—Н3В	109.00	C3'—C4'—H4'2	109.00
НЗА—СЗ—НЗВ	108.00	C5'—C4'—H4'1	109.00
C3—C4—H4B	109.00	C5'—C4'—H4'2	109.00
H4A—C4—H4B	108.00	H4'1—C4'—H4'2	108.00
С5—С4—Н4А	109.00	C6'—C7'—H7'	108.00
C5—C4—H4B	109.00	C8′—C7′—H7′	108.00
C3—C4—H4A	109.00	C16'—C7'—H7'	108.00
C15'—O4'—H4'	107 (3)	C9′—C10′—H10C	109.00
C21'	108 (3)	C9'—C10'—H10D	109.00
С8—С7—Н7	108.00	C11′—C10′—H10C	109.00
С16—С7—Н7	108.00	C11' - C10' - H10D	109.00
С6—С7—Н7	108.00	H10C—C10′—H10D	108.00
C9-C10-H10B	109.00	C10'-C11'-H11C	109.00
C9-C10-H10A	109.00	C10' - C11' - H11D	109.00
H_{10A} C_{10} H_{10B}	108.00	C12'-C11'-H11C	109.00
$C_{11} - C_{10} - H_{10A}$	108.00	C12' - C11' - H11D	109.00
C_{11} C_{10} H_{10R}	109.00		109.00
	109.00		100.00
	109.00	C11 - C12 - H12C	109.00
	108.00	C11 - C12 - H12D	109.00
CI2—CII—HIIB	109.00	$C13^{-}$ $C12^{-}$ $H12C$	110.00
CIQ_CII_HIIB	109.00	$C13^{}C12^{}H12D$	109.00
CI2—CII—HIIA	109.00	HI2C—CI2'—HI2D	108.00
C13—C12—H12A	109.00	NI'—C14'—H14C	109.00
C11—C12—H12B	109.00	N1′—C14′—H14D	109.00
C11—C12—H12A	109.00	C15'—C14'—H14C	109.00
C13—C12—H12B	109.00	C15'—C14'—H14D	109.00
H12A—C12—H12B	108.00	H14C—C14′—H14D	108.00
C15—C14—H14A	110.00	C16'—C17'—H17'	119.00
C15—C14—H14B	110.00	C18'—C17'—H17'	119.00
N1—C14—H14B	110.00	C17'—C18'—H18'	120.00
N1-C14-H14A	110.00	C19'—C18'—H18'	120.00
H14A—C14—H14B	108.00	C18'—C19'—H19'	120.00
С16—С17—Н17	119.00	C20'—C19'—H19'	120.00
C18—C17—H17	119.00	C19'—C20'—H20'	119.00
C19—C18—H18	120.00	C21'—C20'—H20'	119.00
C5—N1—C9—C8	9.8 (3)	C5'—N1'—C9'—C8'	12.7 (3)
C14—N1—C9—C8	-172.4 (2)	C14'—N1'—C9'—C8'	-172.10 (19)
C5—N1—C14—C15	-90.8 (3)	C5'—N1'—C14'—C15'	-81.6 (2)
C9—N1—C14—C15	91.4 (3)	C9'—N1'—C14'—C15'	103.3 (2)
C14—N1—C5—C4	-11.2 (3)	C14'—N1'—C5'—C4'	-13.1 (3)
C9—N1—C5—C6	-9.8 (3)	C9'—N1'—C5'—C6'	-15.4(3)
C14—N1—C5—C6	172.4 (2)	C14'—N1'—C5'—C6'	169.37 (19)
C9—N1—C5—C4	166.6 (2)	C9'—N1'—C5'—C4'	162.15 (19)
C5—N1—C9—C10	-167.6(2)	C5'—N1'—C9'—C10'	-165.21 (18)
C14—N1—C9—C10	10.2 (3)	C14'—N1'—C9'—C10'	10.0 (3)
C6-C1-C2-C3	31.3 (4)	C6'-C1'-C2'-C3'	30.4 (4)
01 - C1 - C2 - C3	-1507(3)	01'-01'-02'-03'	-152.9(3)
		······································	

C^{2} C^{1} C^{6} C^{5}	22(2)	C2' $C1'$ $C6'$ $C5'$	27(2)
$C_2 = C_1 = C_0 = C_3$	2.3(3)	$C_2 = C_1 = C_0 = C_3$	2.7(3)
$C_2 = C_1 = C_0 = C_7$	-175.7(2)	$C_2 = C_1 = C_0 = C_7$	-174.0(2)
01 - C1 - C6 - C3	-1/3.7(2)	01 - C1 - C0 - C3	-1/4.0(2)
01 - 01 - 00 - 07	-0.1(3)	01 - 01 - 00 - 07	2.2(3)
C1 - C2 - C3 - C4	-30.1(4)	C1 - C2 - C3 - C4	-33.3(4)
$C_2 = C_3 = C_4 = C_5$	4/.8 (4)	$C_2 = C_3 = C_4 = C_5$	47.8 (3)
$C_3 - C_4 - C_5 - N_1$	169.3 (2)	C3 - C4 - C5 - NT	167.6(2)
C3-C4-C5-C6	-14.3(4)	C3' - C4' - C5' - C6'	-14.9 (3)
NIC5C6C1	165.4 (2)	NI′—C5′—C6′—C1′	167.06 (19)
C4—C5—C6—C1	-10.9 (4)	C4'—C5'—C6'—C1'	-10.4 (3)
N1—C5—C6—C7	-10.0 (3)	N1′—C5′—C6′—C7′	-9.1 (3)
C4—C5—C6—C7	173.7 (2)	C4′—C5′—C6′—C7′	173.51 (19)
C5—C6—C7—C16	-99.3 (2)	C5'—C6'—C7'—C16'	-91.8 (2)
C5—C6—C7—C8	26.1 (3)	C5'—C6'—C7'—C8'	31.6 (2)
C1—C6—C7—C8	-149.37 (19)	C1'—C6'—C7'—C8'	-144.58 (19)
C1—C6—C7—C16	85.3 (2)	C1'—C6'—C7'—C16'	92.0 (2)
C6—C7—C8—C9	-26.3 (3)	C6'—C7'—C8'—C9'	-34.2 (3)
C8—C7—C16—C17	-36.3 (3)	C8′—C7′—C16′—C17′	-84.2(3)
C8—C7—C16—C21	142.7 (2)	C8'—C7'—C16'—C21'	93.2 (2)
C6—C7—C8—C13	149.89 (18)	C6'—C7'—C8'—C13'	145.26 (19)
C16—C7—C8—C9	99.0 (2)	C16'—C7'—C8'—C9'	90.6 (2)
C6-C7-C16-C21	-941(2)	C6' - C7' - C16' - C21'	-144.9(2)
C6-C7-C16-C17	870(2)	C6' - C7' - C16' - C17'	377(3)
$C_{16} - C_{7} - C_{8} - C_{13}$	-848(2)	$C_{16}^{\prime} - C_{7}^{\prime} - C_{8}^{\prime} - C_{13}^{\prime}$	-900(2)
C7 C8 C9 N1	10.0(3)	$C_{10} - C_{1} - C_{10} - C_{10} - C_{10}$	14.1(3)
C^{0} C^{8} C^{13} O^{2}	10.0(3) 175 8 (2)	$C' = C^{3} = C^{3} = C^{3} = C^{3}$	1773(2)
$C_{7} = C_{8} = C_{13} = C_{2}$	173.0(2)	$C_{7} = C_{8} = C_{13} = 0_{2}$	177.3(2)
$C_1 = C_2 = C_1 = C_1 = C_1 = C_2$	-1/7.3(2)	$C_{1} = C_{0} = C_{13} = C_{12}$	1/8.0(2)
C13 - C3 - C9 - N1	-100.08(19)	C13 - C8 - C9 - N1	-103.37(19)
C_{9} C_{8} C_{13} C_{12}	-1.0(3)	$C9^{}C8^{}C13^{}C12^{}$	-2.6(3)
C/C8C9C10	-1/2.69 (19)		-168.08 (19)
C/C8C13O2	-0.5 (3)	C//C8/C13'O2'	-2.2 (3)
C13—C8—C9—C10	11.2 (3)	C13'—C8'—C9'—C10'	12.5 (3)
C8—C9—C10—C11	12.6 (3)	C8'—C9'—C10'—C11'	12.9 (3)
N1—C9—C10—C11	-170.1(2)	N1′—C9′—C10′—C11′	-169.3(2)
C9—C10—C11—C12	-45.5 (3)	C9'—C10'—C11'—C12'	-46.7 (3)
C10-C11-C12-C13	54.6 (3)	C10'—C11'—C12'—C13'	55.5 (3)
C11—C12—C13—C8	-32.0 (3)	C11'—C12'—C13'—C8'	-31.6 (3)
C11—C12—C13—O2	151.2 (2)	C11'—C12'—C13'—O2'	148.6 (2)
N1—C14—C15—O3	-26.1 (5)	N1'—C14'—C15'—O3'	12.6 (3)
N1-C14-C15-O4	157.7 (3)	N1'-C14'-C15'-O4'	-168.95 (18)
C7—C16—C17—C18	176.5 (2)	C7'—C16'—C17'—C18'	178.6 (3)
C21—C16—C17—C18	-2.5 (4)	C21'—C16'—C17'—C18'	1.1 (4)
C7—C16—C21—O5	2.4 (3)	C7'—C16'—C21'—O5'	0.1 (4)
C7—C16—C21—C20	-175.6 (2)	C7'—C16'—C21'—C20'	179.6 (2)
C17—C16—C21—O5	-178.6(2)	C17'—C16'—C21'—O5'	177.6 (3)
C_{17} C_{16} C_{21} C_{20}	3.5 (3)	C17'-C16'-C21'-C20'	-2.9(4)
C_{16} C_{17} C_{18} C_{19}	0.0 (5)	$C_{16}' - C_{17}' - C_{18}' - C_{19}'$	10(5)
C17-C18-C19-C20	15(5)	C17'-C18'-C19'-C20'	-11(6)
	···· (~)		(0)

C18—C19—C20—C21	-0.6 (5)	C18'—C19'—C20'—C21'	-0.8 (6)
C19—C20—C21—O5	179.9 (3)	C19'—C20'—C21'—O5'	-177.6 (3)
C19—C20—C21—C16	-2.0 (4)	C19'—C20'—C21'—C16'	2.9 (5)

Hydrogen-bond geometry (Å, °)

<i>D</i> —H··· <i>A</i>	D—H	H···A	D····A	D—H···A
04—H4…O2′	0.88 (2)	1.84 (3)	2.683 (3)	162 (3)
$O4'$ — $H4'$ ··· $O2^{i}$	0.84 (3)	1.85 (3)	2.673 (2)	165 (3)
O5—H5…O1	0.83 (3)	1.80 (3)	2.616 (3)	168 (3)
O5'—H5'····O2'	0.85 (4)	1.96 (4)	2.797 (3)	171 (4)
C10—H10A····O5′ ⁱⁱ	0.97	2.60	3.380 (3)	138
C14—H14 <i>B</i> ····O1′ ⁱⁱ	0.97	2.43	3.347 (3)	158
C14′—H14D…O2 ⁱⁱⁱ	0.97	2.36	3.241 (3)	151
С17′—Н17′…О3′	0.93	2.49	3.326 (3)	149

Symmetry codes: (i) x-1/2, -y+1/2, z-1/2; (ii) -x+1, -y+1, -z+1; (iii) -x+1/2, y-1/2, -z+3/2.