

Probing the spatial coherence of wide X-ray beams with Fresnel mirrors at BL25SU of SPring-8

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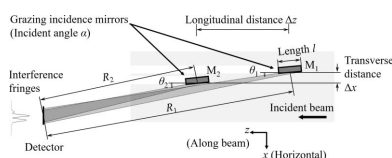
Probing the spatial coherence of X-rays has become increasingly important when designing advanced optical systems for beamlines at synchrotron radiation sources and free-electron lasers. Double-slit experiments at various slit widths are a typical method of quantitatively measuring the spatial coherence over a wide wavelength range including the X-ray region. However, this method cannot be used for the analysis of spatial coherence when the two evaluation points are separated by a large distance of the order of millimetres owing to the extremely narrow spacing between the interference fringes. A Fresnel-mirror-based optical system can produce interference patterns by crossing two beams from two small mirrors separated in the transverse direction to the X-ray beam. The fringe spacing can be controlled via the incidence angles on the mirrors. In this study, a Fresnel-mirror-based optical system was constructed at the soft X-ray beamline (BL25SU) of SPring-8. The relationship between the coherence and size of the virtual source was quantitatively measured at 300 eV in both the vertical and horizontal directions using the beam. The results obtained indicate that this is a valuable method for the optimization of optical systems along beamlines.

1. Introduction

Brilliant and highly coherent X-ray beams have become available with the appearance of third-generation synchrotron radiation sources and X-ray free-electron lasers (XFELs). This has prompted the development of various X-ray imaging methods using coherent X-rays, such as phase-contrast imaging, coherent X-ray diffraction imaging and in-line holography (Snigirev *et al.*, 1995; Miao *et al.*, 1999; Spanne *et al.*, 1999). An X-ray nanofocusing system with diffraction-limited performance has also been constructed (Mimura *et al.*, 2010).

The design and construction of optical systems for carrying out such techniques requires specific beam characteristics in terms of not only brightness but also coherence, which is classified into spatial coherence and temporal coherence. A synchrotron radiation source can provide highly monochromatic X-rays by using a high-performance monochromator. The temporal coherence of an X-ray beam can be controlled to be sufficiently high so as to have no effect on imaging applications and focusing performances. However, the spatial coherence at the apparatus for these applications depends on the selected energy of the X-rays and the parameters of the optical system, such as the geometrical arrangement and slit width.

One purpose of the coherence measurement in this study is to aid in the design of a new soft X-ray nanofocusing system that uses an ellipsoidal mirror at the soft X-ray beamline



(BL25SU) of SPring-8 (Motoyama *et al.*, 2016; Mimura *et al.*, 2018). The coherence property of the incident beam has an influence on the intensity, size and coherence width of the focusing beam. At BL25SU of SPring-8, the beam sizes of the soft X-ray beams are of the order of millimetres.

Spatial coherence has been probed using various methods in X-ray domains (Ishikawa, 1988; Trebes *et al.*, 1992; Marconi *et al.*, 1997; Kohn *et al.*, 2000; Lin *et al.*, 2003; Suzuki, 2004; Pfeiffer *et al.*, 2005; Snigirev *et al.*, 2009) and has been recently investigated by analysis of the single-shot diffraction patterns generated by inserting defined objects such as double pinholes and gold colloidal particles into the focusing beams (Vartanyants *et al.*, 2011; Gutt *et al.*, 2012; Inoue *et al.*, 2015; Kobayashi *et al.*, 2018). However, it becomes difficult to apply these methods to the determination of transverse coherence when the two evaluation points are separated by a large distance of the order of millimetres due to the narrower spacing of the interference fringe as described below.

The degree of coherence between two incoming beams has been measured on the basis of the visibility of the interference profile (Takayama *et al.*, 1998; Paterson *et al.*, 2001). For such analysis, the interference pattern should be sufficiently wide to be analysed with an imaging detector. For example, when the wavelength (λ) of the X-rays is 1 nm, the separation (d) of the two slits is 100 μm and the distance (L) between the slits and the detector is 10 m, the peak-to-peak separation (Λ) in the fringes is calculated to be as small as 100 μm from the following equation,

$$\Lambda = (L/d)\lambda. \quad (1)$$

Although the interval increases with increasing distance between the double slits and the detector, the intensity of the image decreases significantly.

In this study, a Fresnel-mirror-based optical system was constructed to measure the degree of spatial coherence for millimetre-size soft X-ray beams at BL25SU of SPring-8. In a Fresnel-mirror-based optical system, two grazing incidence mirrors are arranged so that the two beams reflecting at each mirror generate interference patterns, as shown in Fig. 1. This optical setup is suitable for the coherence evaluation of the wide X-ray beam, because one can increase the spacing of the interference fringe by controlling the difference between the deflection angles at the two mirrors. This method was previously utilized to measure the spatial coherence of a hard X-ray beam at a synchrotron radiation facility and to measure

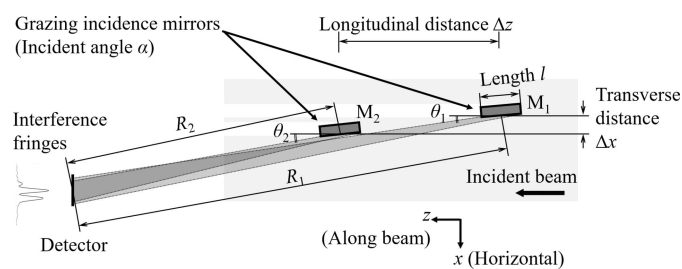


Figure 1
Schematic of the Fresnel-mirror-based optical system for the evaluation of the spatial coherence of X-ray beams.

that of an extreme ultraviolet beam in a high-order harmonic generation system (Fezzaa *et al.*, 1997; Le Déroff *et al.*, 2000). Although an interferometer system that uses four mirrors to measure the coherence property of wide X-ray beams has been proposed, the optical system is rather complicated (Cash *et al.*, 2000).

We will describe the evaluation of the degree of spatial coherence of the soft X-ray beam at 300 eV with a transverse distance of more than 1 mm. The width of the slit placed 18 m upstream of the double mirrors was varied to change the spatial coherence at the mirrors. There is a marked difference in the spatial coherence properties between the horizontal and vertical directions owing to the characteristics of the source under SPring-8 specifications. This difference can be observed by comparing the results obtained before and after rotating the entire Fresnel-mirror-based optical system by 90°.

2. Theoretical model and analytical procedure

In interferometry with Fresnel mirrors, two parts of an incident X-ray beam are reflected at two small mirrors under grazing incidences. An interference fringe pattern is produced because of the overlapping of these reflected beams. The acceptances of the two mirrors are sufficiently small relative to the size of the incident X-ray beam. When the detector is placed in the far field of these mirrors, the degree of coherence analysed from the visibility of the interference fringe can be regarded as the degree of coherence between two X-rays reflecting at the central points of the two mirrors.

The aperture width w of each mirror is equal to $l\sin\alpha$, where l is the longitudinal length of the mirror and α is the incidence angle. Flat or cylindrical shapes of the wavefront at the detector are preferable from the viewpoint of the analysis. In the Fraunhofer diffraction equation, the wavefront inside the central band of a propagating beam is assumed to be cylindrical, although $w^2/8R \ll \lambda$ must be satisfied, where λ is the wavelength and R is the distance between the mirror and the detector. The beam reflected at the mirror travels while expanding in the horizontal direction as a result of the diffraction effect, as shown in Fig. 1.

Here, we develop an expression for the intensity and phase profiles of the beam from the upstream mirror (M_1) in Fig. 2. The (x, y, z) reference frame is defined by the beam propa-

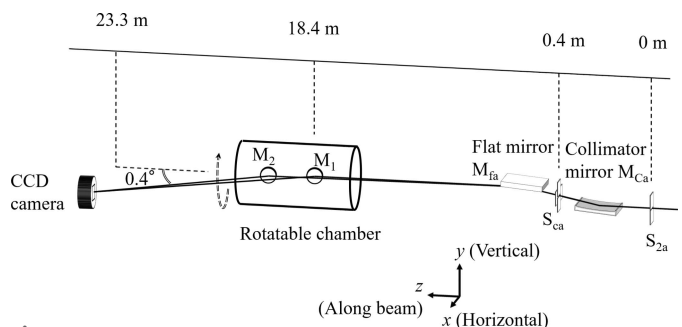


Figure 2
Layout of the Fresnel-mirror-based optical system at the soft X-ray beamline of SPring-8.

gation direction (z), the vertical direction (y) and the horizontal direction (x), with $+x$ pointing towards the storage ring. On an arbitrary horizontal line at the detector represented by $y = y_0$, the observed intensity distribution $I_1(x, y_0)$ is given by the approximate formula

$$I_1(x, y_0) = I_1(0, y_0) \left| \text{sinc} \frac{kwx \cos \theta_1}{2R_1} \right|^2, \quad (2)$$

where $I_1(0, y_0)$ is the maximum intensity on the arbitrary horizontal line, k is the wavenumber, R_1 is the distance between M_1 and the detector, and θ_1 is the angle between the reflected beam and the z axis. As the diffraction pattern is given by a rectangular aperture, the intensity profile in x is expressed by the square of a sinc function, whereas the width of the central band is $2\lambda R_1/(w \cos \theta_1)$. Inside this region, the phase profile is linear with x and is given by

$$\phi_1(x, y_0) = \phi_1(0, y_0) + kx \sin \theta_1, \quad (3)$$

where $\phi_1(0, y_0)$ is the phase of the propagating beam at the central point on the arbitrary horizontal line.

In this experiment, the positions and inclinations of the two mirrors are adjusted so that the central bands of the intensity profiles of the two beams overlap at the detector. If the relationship between the two beams is perfectly coherent, then an interference fringe pattern can be clearly observed.

The intensity profile of an interference fringe pattern is calculated by summing the complex wavefields and squaring the absolute amplitude of the total wavefield. Here, I_3 is the intensity profile observed at the detector when the two beams overlap. I_1 and I_2 are the intensity profiles of the single beams from the upstream mirror M_1 and the downstream mirror M_2 , respectively. The subscripts of θ_1 , θ_2 , ϕ_1 and ϕ_2 indicate the mirror number. On the basis of the above definitions, I_3 is given by

$$I_3(x, y_0) = I_1(x, y_0) + I_2(x, y_0) + 2\sqrt{I_1 I_2} \cos \left[\phi_{y_0} + \left(\frac{2\pi}{\Lambda} \right) x \right],$$

$$\phi_{y_0} \equiv \phi_2(0, y_0) - \phi_1(0, y_0), \quad (4)$$

$$\Lambda \equiv \lambda / |\sin \theta_2 - \sin \theta_1|,$$

where ϕ_{y_0} is a constant and Λ is the interval of the fringe. If the relationship between the two beams is characterized by partial coherence, then their complex degree of coherence is defined quantitatively by the mutual coherence function. The intensity profile I_3 is updated to

$$I_3 = I_1 + I_2 + 2\sqrt{I_1 I_2} \text{Re}[\gamma_{12}]$$

$$= I_1 + I_2 + 2\sqrt{I_1 I_2} |\gamma_{12}| \cos \left(\phi_{y_0} + \frac{2\pi}{\Lambda} x \right), \quad (5)$$

where γ_{12} is the complex degree of coherence. The absolute value of γ_{12} is defined as the degree of coherence, which takes values between 0 and 1. The degree of coherence can be analysed from the normalization of the interference intensity profile. The normalized profile is represented by

$$\text{Re}[\gamma_{12}] = \frac{I_3 - (I_1 + I_2)}{2\sqrt{I_1 I_2}} = |\gamma_{12}| \cos \left(\phi_{y_0} + \frac{2\pi}{\Lambda} x \right). \quad (6)$$

For precise analysis, $|\gamma_{12}|$ is determined by the amplitude of the sine curve fit to $\text{Re}[\gamma_{12}]$.

3. Optical system setup of Fresnel mirrors

A Fresnel-mirror-based optical system was constructed at the soft X-ray beamline (BL25SU) of SPring-8, where a twin helical undulator has been installed. Measurement experiments of the transverse coherence were conducted at the BL25SU-a beamline. Soft X-rays are monochromated with an optical system that consists of three mirrors and a varied-line-spacing plane grating (Senba *et al.*, 2016). Soft X-rays are focused on a transversal plane in the vertical direction, on which the S_{2a} slit is placed and dispersed so that each wavelength satisfies the diffraction grating equation. The mean energy and energy bandwidth of the X-rays are determined by the slit position and opening width, respectively. The soft X-ray beam after the S_{2a} slit propagates with a vertical divergence angle of at least the order of $100 \mu\text{rad}$, and horizontally diverges with an angle of the order of $10 \mu\text{rad}$. To suppress the large beam divergence in the vertical direction, a collimator mirror (M_{Ca}) was set 270 mm downstream of S_{2a} . The S_{Ca} slit, which is composed of four blades, was installed 0.4 m downstream from S_{2a} as the virtual source for this study. The beam energy and energy bandwidth were set to 300 eV and $E/\Delta E = 10\,000$, respectively. The sizes of the beam are 1.27 mm and 0.45 mm in the horizontal and vertical directions, respectively, when the X-ray beam impinges on the S_{Ca} slit.

The Fresnel-mirror-based optical system shown in Fig. 2 was constructed 18 m downstream of S_{Ca} . The diameter of the two plane mirrors was 25.4 mm and the incidence angle was approximately 0.2° . A CCD detector (PIXIS-XO:2048B, Princeton Instruments) with a pixel size of $13.5 \mu\text{m}$ was located 4.9 m downstream of the Fresnel mirrors. The detector can move horizontally and vertically to track the beam positions during the alignment of the two mirrors.

Fig. 3 shows the two mirrors held on a five-axis stage to adjust their inclinations and positions. The incident angles corresponding to the pitching angles determine the intervals

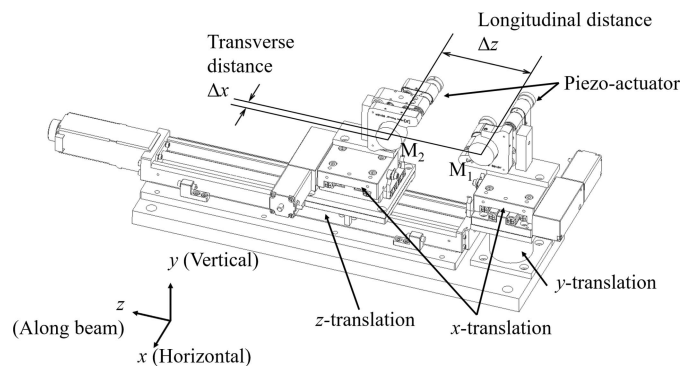


Figure 3 Installed alignment system for two small mirrors in the Fresnel-mirror-based optical system.

Table 1

Experimental conditions for measuring the degree of spatial coherence using a Fresnel-mirror-based optical system.

Direction	Transverse distance Δx or Δy (μm)	Longitudinal distance Δz (mm)	Interval between interference fringes Λ (μm)	Difference between deflection angles (μrad)
Horizontal	171	51	142	29.1
Horizontal	1232	199	170	24.3
Vertical	224	51	180	23.0
Vertical	1273	199	136	30.4

between the interference fringes. The rolling angles are tuned so that the fringes are parallel to the y direction and the effect of the vertical coherence property on the horizontal measurement is eliminated. The distance between the central points of two mirrors in the z direction can be changed by moving the downstream mirror with a one-axis motor stage. The distance Δx in Fig. 3 is the transverse distance between the two mirrors, which is adjusted by the x stages of the mirrors. The whole system shown in Fig. 3 can be rotated by 90° around the optical axis. Owing to geometric constraints, the settable range of Δx is expressed as

$$D\alpha_0 \leq \Delta x \leq 2(\Delta z_{\text{max}} - D)\alpha_0, \quad (7)$$

where D and α_0 are the mirror length and incident angle, respectively, and Δz_{max} is the maximum distance between the two mirrors in the z direction. For example, for the settings $\alpha_0 = 0.2^\circ$ and $\Delta z_{\text{max}} = 211$ mm, the measurable values of Δx range from $88 \mu\text{m}$ to $1296 \mu\text{m}$.

Table 1 shows the geometric parameters of the two mirrors. The slit size of S_{Ca} is varied under these geometrical conditions. The relationships between the slit width and the degree of coherence for the two beams reflected at the two mirrors were investigated in the horizontal and vertical directions. Δx and Δy were also varied.

Low temporal coherence deteriorates the visibility of an interference fringe pattern when there is a difference in the optical path length between the two beams. A difference of the order of $10 \mu\text{m}$ has a significant impact on the visibility at a wavelength of 4.13 nm with $E/\Delta E = 10000$. Under the geometrical conditions shown in Table 1, the maximum difference in the optical path is $4 \mu\text{m}$; thus, the effect of temporal coherence is negligible.

4. Measurements of coherence properties

Fig. 4 shows representative intensity distributions and their cross-sectional profiles recorded by the CCD camera during the measurement of the degree of coherence in the horizontal direction, where the width of the S_{Ca} slit is $10 \mu\text{m}$ and the transverse distance between the two mirrors is $171 \mu\text{m}$. The line with circles in Fig. 4(d) shows the intensity profile measured when only the upstream mirror M_1 reflected a beam, which is the square of the sinc function profile corresponding to the Fraunhofer diffraction pattern of X-rays propagating from a small rectangular aperture. Interference fringes

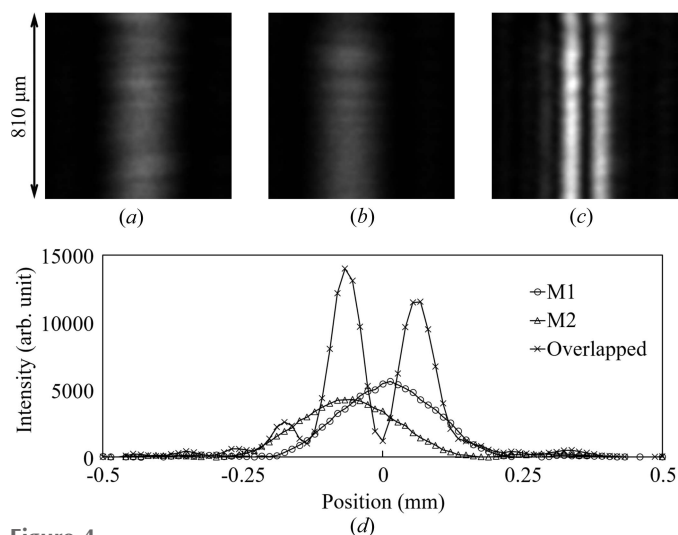


Figure 4 Intensity images and cross-sectional profiles of a measured interference fringe pattern. The X-ray energy is 300 eV . Intensity images of (a) the beam from M_1 , (b) the beam from M_2 and (c) the overlapped beams. (d) Cross-sectional profiles in the horizontal direction.

appeared on the superposition of the two beams from the two mirrors. The spacing of the interference fringe was optimized by tuning the deflection angle of M_2 for the observation using the CCD camera. The cross-sectional profiles were normalized using equation (6) and were fitted by a sine curve profile as shown in Fig. 5. This fitting calculation was performed within two periods of the interference fringe pattern within the central bands. The degree of spatial coherence was determined by the amplitude of the fitted sine curve. To increase the accuracy, five fitted curves obtained at different lines were used and their amplitudes were averaged. Fig. 6 shows the interference images when Δx is $171 \mu\text{m}$ and the width of the S_{Ca} slit is changed from $10 \mu\text{m}$ to the full opening of $20000 \mu\text{m}$, which indicates that the fringe visibility decreases with increasing slit width.

In this study, the width of the S_{Ca} slit and Δx or Δy were varied as parameters to clarify the spatial coherence properties of wide soft X-ray beams. Fig. 7(a) shows a graph of the relationship between the horizontal slit width and the degree of spatial coherence when Δx is $171 \mu\text{m}$ and $1232 \mu\text{m}$. The degree of coherence monotonically increases with decreasing slit width for both values of Δx . It was thus confirmed that the degree of spatial coherence is improved by closing the S_{Ca} slit.

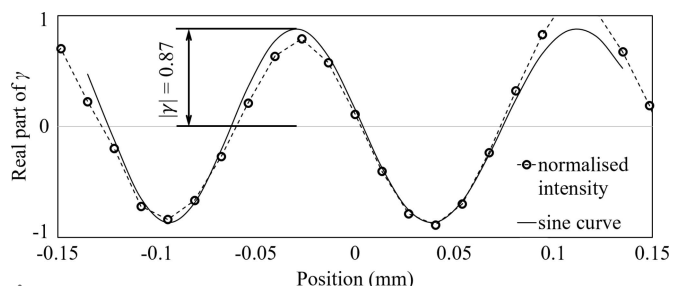


Figure 5 Determination of the degree of coherence. A sine curve is used to fit the normalized intensity profile of the interference fringe shown in Fig. 4.

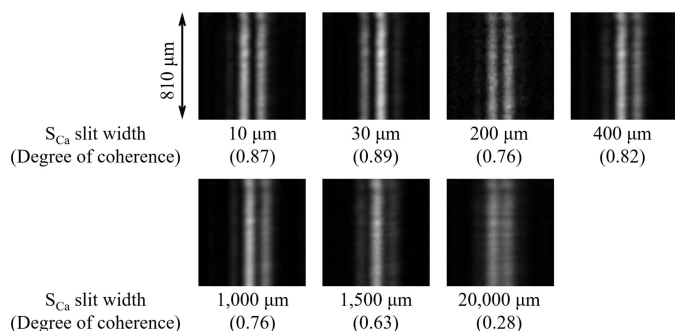


Figure 6 Comparison between the degrees of coherence for different S_{Ca} slit widths as a virtual source and measured intensity images of the interference fringe of the X-ray beams.

The coherence properties were also investigated in the vertical direction under almost the same experimental conditions as those for the horizontal direction. The optical system was rotated by 90° and aligned to observe the interference pattern using the CCD camera. Fig. 7(b) shows the coherence properties obtained by varying the vertical width of the S_{Ca} slit, which clearly indicates that the coherence properties in the vertical direction are superior to those in the horizontal direction.

The degree of coherence was calculated on the basis of van Cittert–Zernike’s theorem, as shown in Fig. 7(c), in which the soft X-ray beam was assumed to be incoherent light at the S_{Ca} slit. The measured degree of coherence is higher than the calculated values in both the horizontal and vertical directions, which indicates that the soft X-rays at the S_{Ca} slit have a partial coherence property.

5. Discussion and summary

The degree of spatial coherence of the soft X-ray beam at BL25SU-a of SPring-8 was measured using a Fresnel-mirror-based optical system. The effect of the upstream optics on the spatial coherence on the downstream side, where the soft X-ray beam has diverged, could be quantitatively evaluated. The degree of spatial coherence in both the horizontal and vertical directions tends to decrease upon increasing width of

the slit placed far upstream of the Fresnel mirrors. The degree of spatial coherence was higher in the vertical direction than in the horizontal direction for the X-ray source properties of the synchrotron radiation source.

According to the experimental results, when the slit widths are approximately $10\ \mu\text{m}$ and $20\ \mu\text{m}$ in the horizontal and vertical directions, respectively, the soft X-ray beam is fully coherent in a square area of the beam of $1.2\ \text{mm}^2$ at the Fresnel mirrors. Thus, the diffraction-limited soft X-ray focusing is theoretically possible under these conditions.

The results indicate that the Fresnel-mirror-based system can be used to measure the spatial coherence properties of wide X-ray beams under highly monochromatic conditions. This optical system can also be used to determine the degree of coherence of X-ray pulses for XFELs owing to the possibility of single-shot measurements. Precise quantitative information on coherence will lead to further improvements of soft X-ray beamlines and various methods applying coherence at synchrotron radiation and XFEL facilities.

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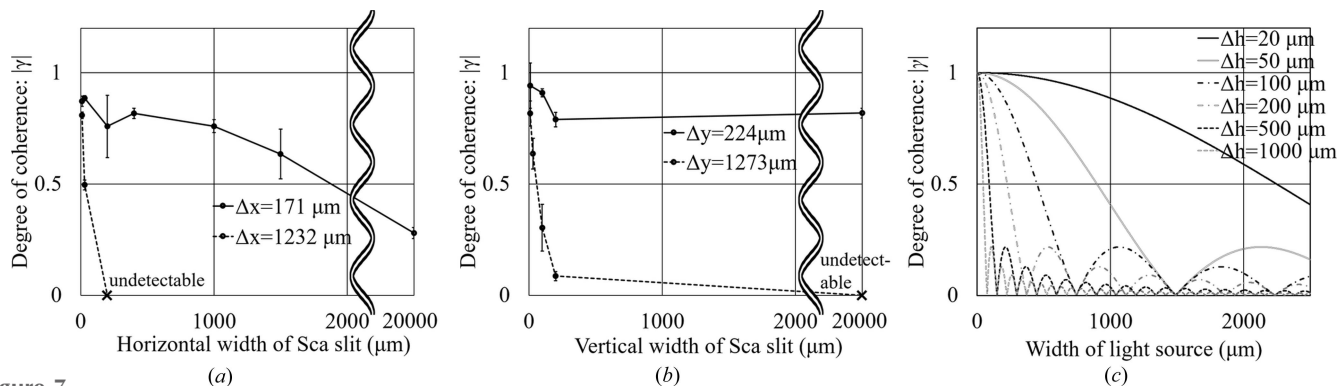


Figure 7 Relationship between the degree of coherence and the S_{Ca} slit width in the (a) horizontal and (b) vertical directions. Δx is the horizontal distance between the central points of the two mirrors and Δy is the vertical distance. These results were measured at an X-ray energy of 300 eV. (c) Degree of coherence calculated on the basis of the van Cittert–Zernike’s theorem; Δh is the transverse distance between the central points of the mirrors.

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