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(10-Ethyl-10*H*-phenothiazine-3,7-diyl)bis(*p*-tolyl-methanone)

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The title compound, $C_{30}H_{25}NO_2S$, crystallizes with two independent molecules (*A* and *B*) having similar conformations in the asymmetric unit. Both phenothiazine units have a butterfly structure; the dihedral angles between the planes of the benzene rings are 17.95 (13) and 12.65 (14)° for molecules *A* and *B*, respectively. In the crystal, the *B* molecules are linked by pairs of C– $H \cdots O$ hydrogen bonds, forming inversion dimers with an $R_2^2(10)$ ring motif. The *A* molecules are linked by C– $H \cdots \pi$ interactions. Layers of *A* molecules and layers of *B* molecules are linked by a second C– $H \cdots \pi$ interaction, forming *A*–*B*–*A* slabs, which stack back-to-back and lie parallel to the *bc* plane.



Structure description

Phenothiazine is a well known heterocycle that occurs in many synthetic dyes, electroluminescent materials (Miller *et al.*, 1999) and drugs, especially various antipsychotic drugs, *e.g.* chlorpromazine, antihistaminic drugs and promethazine (Wermuth, 2003). Recently, new applications for phenothiazine derivatives in medicine have been developed, such as antitubercular (Wang *et al.*, 2008) and antitumor (Lam *et al.*, 2001). As part of our program devoted to new applications of phenothiazine derivatives in medicine, we report herein on the synthesis and crystal structure of the title compound.

The title compound, Fig. 1, crystallizes with two independent molecules (A and B) in the asymmetric unit. The molecular structures of A and B are similar (Fig. 2). The phenothiazine moieties have a butterfly structure, where the dihedral angles between the two benzene rings (C9–C14 and C17–C22 in A, and C9'–C14' and C17'-C22' in B) are 17.95 (13) and 12.65 (14)°, respectively. The thiazine rings in both molecules have a shallow boat-like conformation. The phenyl rings (C2–C7 and C24–C29) are inclined to





Figure 1

The molecular structure of the title compound, showing the atom labelling and 30% probability displacement ellipsoids.

the phenothiazine ring mean plane by 52.24 (10) and 61.61 (11)°, respectively, for molecule A and by 51.3 (1) and 59.07 (10)°, respectively, for the corresponding dihedral angles in molecule B. The two phenyl rings are inclined to one another by 71.65 (14)° in molecule A and by 76.67 (13)° in molecule B. The oxygen atoms, O1 and O2, in molecule A deviate from the mean plane of the phenothiazine ring by 0.109 (3) and -1.044 (2) Å, respectively. In molecule B, oxygen atoms, O1' and O2', deviate by -0.236 (2) and 0.783 (3) Å, respectively, from the phenothiazine ring mean plane.

In the crystal, the *B* molecules are linked by pairs of C– H···O hydrogen bonds, forming inversion dimers with an $R_2^2(10)$ ring motif (Fig. 3 and Table 1). The *A* molecules are linked by C–H··· π interactions (Fig. 3 and Table 1). Layers of *A* molecules and layers of *B* molecules are linked by a second C–H··· π interaction, forming *A*–*B*–*B*–*A* slabs, stacking back-to-back, and lying parallel to the *bc* plane (Fig. 3 and Table 1).

Synthesis and crystallization

To 10-ethyl-10*H*-phenothiazine (1 g, 4.4 mmol) in DCM (75 ml) was added AlCl₃ (1.76 g, 13.2 mmol) in a three-necked flask under a nitrogen atmosphere. *p*-Tolouyl chloride (1.2 ml, 9.25 mmol) was added dropwise to the reaction mixture, which was then refluxed gently. Thereafter, it was stirred at room temperature for another 8 h. The reaction mixture was taken up in DCM (200 ml), brine (100 ml) and dried with Na₂SO₄. The organic layer was concentrated under vacuum and the residue was purified by column chromatography on silica gel



Figure 2 AutoMolFit (*PLATON*; Spek, 2009) of molecule *B* (red) inverted on molecule *A* (black).

Table 1Hydrogen-bond geometry (Å, $^{\circ}$).

Cg2 and Cg3 are the centroids of rings C2–C7 (molecule A) and C2'–C7' (molecule B), respectively.

$D - H \cdot \cdot \cdot A$	D-H	$H \cdot \cdot \cdot A$	$D \cdot \cdot \cdot A$	$D - \mathbf{H} \cdot \cdot \cdot A$
$C4'-H4'\cdots O1'^i$	0.93	2.55	3.325 (3)	141
$C30-H30F\cdots Cg2^{ii}$	0.96	2.98	3.716 (3)	134
$C1-H1A\cdots Cg3$	0.96	2.91	3.667 (4)	137

Symmetry codes: (i) -x, -y, -z + 1; (ii) $x, -y + \frac{3}{2}, z - \frac{1}{2}$.

Table 2

Expe	imental	details.	

Crystal data	
Chemical formula	$C_{30}H_{25}NO_2S$
M _r	463.57
Crystal system, space group	Monoclinic, $P2_1/c$
Temperature (K)	293
a, b, c (Å)	19.6758 (8), 12.9382 (5),
ρ (0)	21.1300(9)
p(1)	117.313 (1)
V (A')	4770.8 (3)
	8
Radiation type	Μο Κα
$\mu (\text{mm}^{-1})$	0.16
Crystal size (mm)	$0.30 \times 0.25 \times 0.20$
Data collection	
Diffractometer	Bruker SMART APEXII CCD
Absorption correction	Multi-scan (<i>SADABS</i> ; Bruker, 2008)
T_{\min}, T_{\max}	0.949, 0.966
No. of measured, independent and observed $[I > 2\sigma(I)]$ reflections	57343, 8414, 5992
R _{int}	0.039
$(\sin \theta / \lambda)_{\rm max} ({\rm \AA}^{-1})$	0.595
Refinement	
$R[F^2 > 2\sigma(F^2)], wR(F^2), S$	0.046, 0.141, 1.03
No. of reflections	8414
No. of parameters	613
H-atom treatment	H-atom parameters constrained
$\Delta \rho_{\rm max}, \Delta \rho_{\rm min} \ ({\rm e} \ {\rm \AA}^{-3})$	0.80, -0.59

Computer programs: *APEX2* and *SAINT* (Bruker, 2008), *SHELXS97* and *SHELXL97* (Sheldrick, 2008), *ORTEP-3 for Windows* (Farrugia, 2012) and *PLATON* (Spek, 2009).



Figure 3

The crystal structure of the title compound, viewed along the *b* axis. Hydrogen bonds are illustrated by dashed lines and $C-H\cdots\pi$ interactions by blue arrows (see Table 1; colour code: molecule *A* black and molecule *B* red). For clarity, only the H atoms involved in these interactions have been included.

using chloroform–hexane (1:1 v/v) to give the title compound as orange–red block-like crystals.

Refinement

Crystal data, data collection and structure refinement details are summarized in Table 2.

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full crystallographic data

IUCrData (2016). **1**, x161838 [https://doi.org/10.1107/S2414314616018381]

(10-Ethyl-10*H*-phenothiazine-3,7-diyl)bis(*p*-tolylmethanone)

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(10-Ethyl-10H-phenothiazine-3,7-diyl)bis(p-tolylmethanone)

Crystal data

C₃₀H₂₅NO₂S $M_r = 463.57$ Monoclinic, P2₁/c Hall symbol: -P 2ybc a = 19.6758 (8) Å b = 12.9382 (5) Å c = 21.1306 (9) Å $\beta = 117.513$ (1)° V = 4770.8 (3) Å³ Z = 8

Data collection

Bruker SMART APEXII CCD diffractometer Radiation source: fine-focus sealed tube Graphite monochromator ω and φ scans Absorption correction: multi-scan (*SADABS*; Bruker, 2008) $T_{\min} = 0.949, T_{\max} = 0.966$

Refinement

Refinement on F^2 Least-squares matrix: full $R[F^2 > 2\sigma(F^2)] = 0.046$ $wR(F^2) = 0.141$ S = 1.038414 reflections 613 parameters 0 restraints Primary atom site location: structure-invariant direct methods Secondary atom site location: difference Fourier map F(000) = 1952 $D_x = 1.291 \text{ Mg m}^{-3}$ Mo K\alpha radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 5992 reflections $\theta = 1.2-25.0^{\circ}$ $\mu = 0.16 \text{ mm}^{-1}$ T = 293 KBlock, orange–red $0.30 \times 0.25 \times 0.20 \text{ mm}$

57343 measured reflections 8414 independent reflections 5992 reflections with $I > 2\sigma(I)$ $R_{int} = 0.039$ $\theta_{max} = 25.0^{\circ}, \theta_{min} = 1.2^{\circ}$ $h = -23 \rightarrow 23$ $k = -15 \rightarrow 15$ $l = -25 \rightarrow 24$

Hydrogen site location: inferred from neighbouring sites H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.0639P)^2 + 2.3313P]$ where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{max} < 0.001$ $\Delta\rho_{max} = 0.80 \text{ e} \text{ Å}^{-3}$ $\Delta\rho_{min} = -0.59 \text{ e} \text{ Å}^{-3}$ Extinction correction: SHELXL97 (Sheldrick, 2008), Fc*=kFc[1+0.001xFc²\lambda^3/sin(2\theta)]^{-1/4} Extinction coefficient: 0.0023 (4)

Special details

Geometry. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F, with F set to zero for negative F^2 . The threshold expression of $F^2 > 2$ sigma(F^2) is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R- factors based on ALL data will be even larger.

 $U_{\rm iso} * / U_{\rm eq}$ х Ζ v C1′ 0.0668 (8) 0.21978 (17) -0.0743(2)0.78932 (16) 0.100* H1′1 0.2682 -0.04660.8235 0.100* H1'2 0.2266 -0.14430.7783 H1'3 0.1844 -0.07290.8089 0.100* -0.0687(2)0.0669 (8) C1 0.27952 (18) 0.59268 (17) 0.100* H1A 0.2293 -0.04450.5824 H1B -0.06190.100* 0.3132 0.6429 H1C 0.2767 -0.14000.5791 0.100* C2 0.30984(14)-0.00555(18)0.55147 (14) 0.0471 (6) C2' 0.18861 (13) -0.01010(18)0.72228(13)0.0441 (6) C3′ 0.11942 (14) -0.03427(18)0.66442 (14) 0.0449 (6) H3' 0.0928 -0.09270.6662 0.054* C3 0.0494 (6) 0.38131 (15) -0.02495(19)0.55703 (14) 0.059* H3 0.4094 -0.08080.5843 C4′ 0.0444(6)0.08915 (14) 0.02664 (17) 0.60415 (13) H4'0.053* 0.0429 0.0083 0.5656 C4 0.0487 (6) 0.41231 (15) 0.03576 (18) 0.52354 (14) 0.058* H4 0.4605 0.0203 0.5281 C5 0.37177(14)0.12036 (18) 0.48281 (13) 0.0458 (6) C5′ 0.12708 (13) 0.11525 (17) 0.60039(12)0.0400(5)C6′ 0.13937 (18) 0.0459 (6) 0.19735(13)0.65853 (13) 0.055* H6' 0.1981 0.2239 0.6571 C6 0.29903 (14) 0.1388(2)0.47541 (14) 0.0523 (6) H6 0.1940 0.063* 0.2706 0.4477 0.50845 (15) C7 0.26833 (15) 0.0765(2)0.0540(7)0.065* H7 0.2190 0.0895 0.5019 C7′ 0.0499 (6) 0.22756 (14) 0.07683 (19) 0.71786 (14) H7'0.2750 0.0931 0.7557 0.060* C8 0.40814 (15) 0.1840(2)0.44764 (14) 0.0524(6)C8′ 0.09327 (14) 0.17748 (18) 0.53355 (13) 0.0448(6)C9 0.39953 (14) 0.29850 (18) 0.44435(13)0.0455(6)C9' 0.29161 (17) 0.10108 (13) 0.53681 (12) 0.0414(5)C10′ 0.08842(14)0.47499 (13) 0.0439 (6) 0.34462 (18) H10' 0.0818 0.3071 0.4350 0.053* 0.39779 (12) C10 0.41756 (14) 0.35455 (18) 0.0448(6)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

H10	0.4285	0.3189	0.3654	0.054*
C11	0.41968 (13)	0.46085 (18)	0.39826 (12)	0.0407 (5)
C11′	0.08532 (13)	0.45108 (17)	0.47120 (12)	0.0411 (5)
C12′	0.09787 (13)	0.51072 (17)	0.53132 (12)	0.0393 (5)
C12	0.40114 (13)	0.51805 (18)	0.44485 (12)	0.0397 (5)
C13′	0.11327 (14)	0.45661 (18)	0.59384 (13)	0.0460 (6)
H13′	0.1237	0.4934	0.6351	0.055*
C13	0.38083 (15)	0.46127 (19)	0.48976 (13)	0.0495 (6)
H13	0.3664	0.4964	0.5201	0.059*
C14	0.38146 (15)	0.35449 (19)	0.49045 (13)	0.0496 (6)
H14	0.3695	0.3195	0.5225	0.059*
C14′	0.11335 (14)	0.35002 (18)	0.59575 (13)	0.0457 (6)
H14′	0.1219	0.3167	0.6378	0.055*
C15	0.38786 (14)	0.67828 (19)	0.50153 (13)	0.0459 (6)
H15A	0.4125	0.7455	0.5122	0.055*
H15B	0.4105	0.6377	0.5450	0.055*
C15′	0.10342 (14)	0.67352 (18)	0.59412 (12)	0.0416 (5)
H15C	0.0797	0.6333	0.6174	0.050*
H15D	0.0774	0.7397	0.5809	0.050*
C16′	0.18679 (15)	0.6915 (2)	0.64643 (13)	0.0530(6)
H16A	0.1902	0.7266	0.6878	0.079*
H16B	0.2103	0.7331	0.6243	0.079*
H16C	0.2128	0.6263	0.6604	0.079*
C16	0.30322 (15)	0.6925 (2)	0.47868 (15)	0.0594 (7)
H16D	0.2969	0.7261	0.5161	0.089*
H16E	0.2786	0.6262	0.4691	0.089*
H16F	0.2806	0.7341	0.4363	0.089*
C17′	0.09416 (13)	0.67828 (17)	0.47387 (12)	0.0397 (5)
C17	0.40185 (13)	0.68766 (18)	0.39154 (12)	0.0395 (5)
C18	0.41822 (13)	0.64591 (17)	0.33849 (12)	0.0398 (5)
C18′	0.08166 (14)	0.63426 (17)	0.40819 (12)	0.0425 (6)
C19′	0.08529 (14)	0.69365 (19)	0.35596 (13)	0.0473 (6)
H19′	0.0783	0.6621	0.3138	0.057*
C19	0.41100 (13)	0.70532 (18)	0.28176 (12)	0.0429 (6)
H19	0.4192	0.6747	0.2460	0.051*
C20′	0.09912 (15)	0.79945 (18)	0.36410(13)	0.0483 (6)
C20	0.39191 (13)	0.80970 (18)	0.27601 (13)	0.0438 (6)
C21	0.37872 (15)	0.85238 (19)	0.32956 (14)	0.0496 (6)
H21	0.3673	0.9224	0.3281	0.060*
C21′	0.10987 (15)	0.84357 (19)	0.42761 (14)	0.0520 (6)
H21′	0.1189	0.9142	0.4345	0.062*
C22′	0.10749 (15)	0.78442 (18)	0.48115 (13)	0.0495 (6)
H22′	0.1150	0.8165	0.5233	0.059*
C22	0.38233 (15)	0.79241 (18)	0.38507 (13)	0.0487 (6)
H22	0.3714	0.8227	0.4193	0.058*
C23	0.38333 (14)	0.8663 (2)	0.21178 (13)	0.0482 (6)
C23′	0.10651 (17)	0.8552 (2)	0.30615 (15)	0.0579 (7)
C24	0.38274 (14)	0.98162 (19)	0.20998 (13)	0.0458 (6)

C24′	0.11282 (16)	0.97004 (19)	0.30765 (13)	0.0500 (6)
C25′	0.16577 (17)	1.0166 (2)	0.29121 (14)	0.0581 (7)
H25′	0.1993	0.9760	0.2821	0.070*
C25	0.33361 (15)	1.0323 (2)	0.14739 (14)	0.0512 (6)
H25	0.2982	0.9946	0.1088	0.061*
C26	0.33712 (15)	1.1381 (2)	0.14219 (14)	0.0537 (7)
H26	0.3027	1.1710	0.1005	0.064*
C26′	0.16950 (19)	1.1227 (2)	0.28817 (15)	0.0662 (8)
H26′	0.2063	1.1528	0.2780	0.079*
C27	0.39059 (15)	1.19654 (19)	0.19755 (15)	0.0508 (6)
C27′	0.1195 (2)	1.1851 (2)	0.29996 (15)	0.0656 (8)
C28	0.43847 (15)	1.14547 (19)	0.26014 (14)	0.0508 (6)
H28	0.4744	1.1832	0.2985	0.061*
C28′	0.06678 (18)	1.1383 (2)	0.31601 (15)	0.0617 (7)
H28′	0.0324	1.1790	0.3239	0.074*
C29′	0.06352 (16)	1.03236 (19)	0.32074 (14)	0.0534 (7)
H29′	0.0280	1.0026	0.3328	0.064*
C29	0.43398 (15)	1.04008 (19)	0.26688 (13)	0.0492 (6)
H29	0.4656	1.0080	0.3100	0.059*
C30′	0.1229 (3)	1.3012 (2)	0.2955 (2)	0.1176 (16)
H30A	0.1635	1.3199	0.2845	0.176*
H30B	0.1324	1.3311	0.3404	0.176*
H30C	0.0751	1.3264	0.2587	0.176*
C30	0.39930 (18)	1.3108 (2)	0.19008 (18)	0.0691 (8)
H30D	0.4393	1.3374	0.2339	0.104*
H30E	0.3520	1.3451	0.1795	0.104*
H30F	0.4122	1.3228	0.1521	0.104*
N1	0.40368 (11)	0.62686 (15)	0.44721 (10)	0.0417 (5)
N1′	0.09290 (11)	0.61911 (14)	0.52887 (10)	0.0409 (5)
O1′	0.05830 (12)	0.13384 (13)	0.47603 (9)	0.0621 (5)
01	0.44698 (13)	0.14253 (15)	0.42364 (12)	0.0751 (6)
O2′	0.10905 (17)	0.80727 (16)	0.25741 (13)	0.0923 (8)
O2	0.37729 (13)	0.81890 (14)	0.15934 (10)	0.0689 (6)
S1	0.45355 (4)	0.51999 (5)	0.34352 (4)	0.05027 (19)
S1'	0.05463 (5)	0.50526 (5)	0.38606 (4)	0.0605 (2)

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
C1′	0.0627 (18)	0.0652 (18)	0.0595 (18)	0.0032 (14)	0.0172 (15)	0.0202 (15)
C1	0.078 (2)	0.0512 (16)	0.086 (2)	-0.0083 (15)	0.0501 (18)	0.0002 (15)
C2	0.0550 (15)	0.0374 (13)	0.0516 (15)	-0.0070 (11)	0.0269 (13)	-0.0092 (11)
C2′	0.0435 (13)	0.0421 (13)	0.0461 (14)	0.0054 (11)	0.0202 (12)	0.0038 (11)
C3′	0.0458 (14)	0.0354 (12)	0.0551 (16)	-0.0027 (10)	0.0245 (12)	0.0031 (11)
C3	0.0598 (16)	0.0388 (13)	0.0492 (15)	0.0062 (12)	0.0248 (13)	0.0026 (11)
C4′	0.0427 (13)	0.0396 (13)	0.0451 (14)	-0.0033 (10)	0.0154 (11)	-0.0021 (11)
C4	0.0523 (15)	0.0434 (14)	0.0548 (16)	0.0086 (11)	0.0285 (13)	0.0031 (12)
C5	0.0541 (15)	0.0412 (13)	0.0444 (14)	0.0035 (11)	0.0246 (12)	0.0007 (11)

C5′	0.0416 (13)	0.0339 (12)	0.0443 (14)	0.0007 (10)	0.0198 (11)	-0.0011 (10)
C6′	0.0409 (13)	0.0405 (13)	0.0540 (16)	-0.0050 (10)	0.0200 (12)	0.0015 (12)
C6	0.0485 (15)	0.0469 (14)	0.0538 (16)	0.0074 (12)	0.0170 (13)	0.0044 (12)
C7	0.0424 (14)	0.0518 (15)	0.0659 (18)	-0.0019 (12)	0.0235 (13)	-0.0048 (13)
C7′	0.0376 (13)	0.0517 (15)	0.0510 (16)	-0.0011 (11)	0.0125 (12)	0.0020 (12)
C8	0.0639 (17)	0.0504 (15)	0.0497 (16)	0.0113 (13)	0.0320 (14)	0.0066 (12)
C8′	0.0458 (14)	0.0427 (13)	0.0457 (15)	-0.0030 (11)	0.0209 (12)	-0.0011 (11)
C9	0.0497 (14)	0.0463 (14)	0.0446 (14)	0.0070 (11)	0.0253 (12)	0.0061 (11)
C9′	0.0445 (13)	0.0379 (13)	0.0411 (13)	-0.0005(10)	0.0191 (11)	0.0011 (10)
C10′	0.0529 (14)	0.0431 (13)	0.0385 (13)	-0.0030(11)	0.0235 (11)	-0.0042(11)
C10	0.0519 (14)	0.0483 (14)	0.0376 (13)	0.0085 (11)	0.0234 (11)	0.0025 (11)
C11	0.0423 (13)	0.0449 (13)	0.0349 (13)	0.0060 (10)	0.0179 (11)	0.0049 (10)
C11′	0.0481 (14)	0.0406 (13)	0.0377(13)	-0.0029(10)	0.0225 (11)	0.0001 (10)
C12′	0.0436 (13)	0.0377(12)	0.0390(13)	-0.0018(10)	0.0210(11)	-0.0008(10)
C12	0.0410(13)	0.0448(13)	0.0324(12)	0.0030(10)	0.0162(10)	0,0002 (10)
C13′	0.0609(16)	0.0415(13)	0.0324(12) 0.0354(13)	-0.0020(11)	0.0102(10) 0.0221(12)	-0.0013(10)
C13	0.0603(16)	0.0520(15)	0.0351(15) 0.0456(15)	0.0020(11) 0.0048(12)	0.0221(12) 0.0345(13)	0.0003(12)
C14	0.0622(10)	0.0320(15) 0.0494(15)	0.0474(15)	0.0010(12) 0.0041(12)	0.0339(13)	0.0002(12)
C14′	0.0020(10)	0.0445(14)	0.0360(13)	0.0011(12) 0.0004(11)	0.0337(13) 0.0207(12)	0.0002(12) 0.0047(11)
C15	0.0580(15) 0.0584(15)	0.0487(14)	0.0355(13)	0.0001(11)	0.0258(12)	-0.0036(11)
C15'	0.0538(14)	0.0385(12)	0.0350(13) 0.0380(13)	-0.0012(11)	0.0250(12) 0.0259(11)	-0.0037(10)
C16′	0.0606 (16)	0.0537(12)	0.0300(15) 0.0434(15)	-0.0075(13)	0.0239(11) 0.0230(13)	-0.0055(12)
C16	0.0600(10) 0.0640(17)	0.0696 (18)	0.0151(13) 0.0552(17)	0.0075 (15)	0.0250(15) 0.0367(14)	-0.0009(12)
C17'	0.0010(17) 0.0456(13)	0.0399(13)	0.0352(17)	0.0017(10)	0.0205(11)	0.00000000000000000000000000000000000
C17	0.0396(12)	0.0333(13) 0.0455(13)	0.0333(12)	-0.0037(10)	0.0203(11) 0.0167(10)	-0.0020(10)
C18	0.0330(12) 0.0412(13)	0.0437(13)	0.0364(13)	-0.0032(10)	0.0107(10)	-0.0016(10)
C18′	0.0525(14)	0.0392(13)	0.0398(13)	0.00052(11)	0.0192(11) 0.0247(12)	0.0012(10)
C19′	0.0600 (16)	0.0372(13) 0.0475(14)	0.0390(13) 0.0420(14)	0.0022(11) 0.0072(12)	0.0299(12)	0.0012(10) 0.0033(11)
C19	0.0459(13)	0.0476(14)	0.0392(13)	-0.0038(11)	0.0232(11)	-0.0045(11)
C20′	0.0616 (16)	0.0439(14)	0.0475(15)	0.0042(12)	0.0321(13)	0.0085(12)
C20	0.0468 (14)	0.0467 (14)	0.0409(14)	-0.0042(11)	0.0229(11)	0.0002(11)
C21	0.0617 (16)	0.0410(13)	0.0529 (16)	0.0004(12)	0.0322(13)	0.0004(12)
C21'	0.0699(17)	0.0403(13)	0.0469(15)	-0.0032(12)	0.0222(13)	0.0034(12)
C22'	0.0670(17)	0.0431(14)	0.0395(14)	-0.0042(12)	0.0254(13)	-0.0023(11)
C22	0.0652 (17)	0.0435 (14)	0.0465 (15)	0.0009 (12)	0.0337 (13)	-0.0037(11)
C23	0.0518(15)	0.0529 (15)	0.0426 (15)	-0.0041(12)	0.0240(12)	0.0011 (12)
C23′	0.083 (2)	0.0518 (16)	0.0539 (17)	0.0097 (14)	0.0444 (16)	0.0102 (13)
C24	0.0516(14)	0.0518 (14)	0.0412 (14)	-0.0001(12)	0.0277(12)	0.0052(11)
C24′	0.0702 (17)	0.0468 (14)	0.0389 (14)	0.0049 (12)	0.0302 (13)	0.0082(11)
C25′	0.0715 (18)	0.0642 (18)	0.0509 (16)	0.0060 (14)	0.0388 (15)	0.0097 (13)
C25	0.0492 (15)	0.0634 (17)	0.0417 (14)	-0.0003(12)	0.0216 (12)	0.0038 (12)
C26	0.0560 (16)	0.0609 (17)	0.0502 (16)	0.0134 (13)	0.0295 (14)	0.0183 (13)
C26′	0.086 (2)	0.0677 (19)	0.0566 (18)	-0.0169 (16)	0.0428 (17)	0.0033 (15)
C27	0.0564 (16)	0.0488 (15)	0.0601 (17)	0.0075 (12)	0.0379 (14)	0.0069 (13)
C27′	0.108 (2)	0.0478 (16)	0.0523 (17)	-0.0060 (16)	0.0468 (18)	0.0013 (13)
C28	0.0565 (16)	0.0512 (15)	0.0492 (15)	-0.0026 (12)	0.0282 (13)	-0.0003 (12)
C28′	0.087 (2)	0.0513 (16)	0.0550 (17)	0.0092 (15)	0.0401 (16)	0.0055 (13)
C29′	0.0697 (18)	0.0497 (15)	0.0509 (16)	0.0023 (13)	0.0364 (14)	0.0071 (12)
	× /	× /	· /	· /	× /	× /

C29	0.0551 (15)	0.0517 (15)	0.0387 (14)	-0.0014 (12)	0.0198 (12)	0.0047 (12)
C30′	0.217 (5)	0.0494 (19)	0.135 (4)	-0.016 (2)	0.122 (4)	0.001 (2)
C30	0.079 (2)	0.0518 (16)	0.086 (2)	0.0113 (15)	0.0465 (18)	0.0132 (16)
N1	0.0509 (12)	0.0458 (11)	0.0340 (10)	0.0022 (9)	0.0245 (9)	-0.0029 (9)
N1′	0.0550 (12)	0.0367 (10)	0.0346 (10)	-0.0029 (9)	0.0237 (9)	-0.0027 (8)
01′	0.0857 (14)	0.0470 (10)	0.0426 (11)	-0.0146 (9)	0.0203 (10)	-0.0037 (8)
01	0.1114 (17)	0.0571 (12)	0.0918 (16)	0.0258 (11)	0.0768 (14)	0.0178 (11)
O2′	0.176 (3)	0.0556 (12)	0.0946 (17)	0.0102 (14)	0.1040 (19)	0.0063 (12)
O2	0.1067 (16)	0.0586 (12)	0.0480 (11)	-0.0054 (11)	0.0413 (11)	-0.0031 (9)
S1	0.0664 (4)	0.0486 (4)	0.0524 (4)	0.0089 (3)	0.0415 (3)	0.0042 (3)
S1′	0.1021 (6)	0.0439 (4)	0.0387 (4)	-0.0068 (4)	0.0353 (4)	-0.0031 (3)

Geometric parameters (Å, °)

<u> </u>	1.507 (3)	C15'—H15D	0.9700
C1'—H1'1	0.9600	C16'—H16A	0.9600
C1′—H1′2	0.9600	C16'—H16B	0.9600
C1'—H1'3	0.9600	C16'—H16C	0.9600
C1—C2	1.504 (4)	C16—H16D	0.9600
C1—H1A	0.9600	C16—H16E	0.9600
C1—H1B	0.9600	C16—H16F	0.9600
C1—H1C	0.9600	C17′—C22′	1.393 (3)
C2—C3	1.379 (4)	C17'—N1'	1.401 (3)
C2—C7	1.391 (4)	C17′—C18′	1.413 (3)
C2′—C3′	1.381 (3)	C17—C22	1.398 (3)
C2'—C7'	1.388 (3)	C17—N1	1.402 (3)
C3'—C4'	1.377 (3)	C17—C18	1.409 (3)
С3′—Н3′	0.9300	C18—C19	1.375 (3)
C3—C4	1.374 (3)	C18—S1	1.755 (2)
С3—Н3	0.9300	C18′—C19′	1.373 (3)
C4′—C5′	1.390 (3)	C18′—S1′	1.749 (2)
C4'—H4'	0.9300	C19'—C20'	1.391 (3)
C4—C5	1.393 (3)	С19'—Н19'	0.9300
C4—H4	0.9300	C19—C20	1.392 (3)
С5—С6	1.387 (3)	C19—H19	0.9300
C5—C8	1.495 (3)	C20'—C21'	1.382 (3)
C5'—C6'	1.396 (3)	C20'—C23'	1.485 (3)
C5'—C8'	1.489 (3)	C20—C21	1.387 (3)
C6'—C7'	1.375 (3)	C20—C23	1.482 (3)
Сб'—Нб'	0.9300	C21—C22	1.380 (3)
С6—С7	1.375 (4)	C21—H21	0.9300
С6—Н6	0.9300	C21′—C22′	1.384 (3)
С7—Н7	0.9300	C21'—H21'	0.9300
С7'—Н7'	0.9300	C22'—H22'	0.9300
C8—O1	1.220 (3)	С22—Н22	0.9300
C8—C9	1.489 (3)	C23—O2	1.224 (3)
C8'—O1'	1.223 (3)	C23—C24	1.492 (3)
C8′—C9′	1.483 (3)	C23'—O2'	1.223 (3)

C9—C14	1.386 (3)	C23'—C24'	1.490 (4)
C9—C10	1.394 (3)	C24—C29	1.383 (3)
C9'—C14'	1.379 (3)	C24—C25	1.390 (3)
C9′—C10′	1.392 (3)	C24′—C25′	1.380 (4)
C10'—C11'	1.379 (3)	C24′—C29′	1.384 (4)
C10'—H10'	0.9300	C25′—C26′	1.378 (4)
C10-C11	1.376 (3)	C25'—H25'	0.9300
С10—Н10	0.9300	C25—C26	1.377 (4)
C11—C12	1.408 (3)	C25—H25	0.9300
C11—S1	1.755 (2)	C26—C27	1.382 (4)
C11'—C12'	1.407 (3)	C26—H26	0.9300
C11'—S1'	1.758 (2)	C26'—C27'	1.382 (4)
C12'—C13'	1.399 (3)	C26'—H26'	0.9300
C12'—N1'	1.405 (3)	C27—C28	1.386 (4)
C12—C13	1.397 (3)	C27 - C30	1.505 (3)
C12—N1	1.397(3) 1 409(3)	C27'-C28'	1.302(3) 1.372(4)
C13'-C14'	1380(3)	C27'-C30'	1.572(1)
C13'—H13'	0.9300	C_{28} C_{29}	1.300(1) 1.378(3)
C13—C14	1 382 (3)	C28—H28	0.9300
C13_H13	0.9300	C28' - C29'	1.378(4)
C14—H14	0.9300	$C_{28} = C_{29}$ $C_{28} = H_{28}$	0.9300
C14'H14'	0.9300	C20'_H20'	0.9300
C15—N1	1,479(3)	$C_{29} = H_{29}$	0.9300
C15-C16	1.775(3)	C_{20} H_{20}	0.9600
C15H15A	0.9700	C30'H30B	0.9600
C15H15B	0.9700	C30'—H30C	0.9600
C15'_N1'	1.475(3)	C30_H30D	0.9600
C15' - C16'	1.475(3) 1 514(3)	C30—H30E	0.9600
C15'_H15C	0.9700	C30_H30E	0.9600
	0.9700	050-11501	0.9000
C2'—C1'—H1'1	109.5	H16A—C16′—H16C	109.5
C2'—C1'—H1'2	109.5	H16B—C16′—H16C	109.5
H1'1—C1'—H1'2	109.5	C15—C16—H16D	109.5
C2'—C1'—H1'3	109.5	C15—C16—H16E	109.5
H1'1—C1'—H1'3	109.5	H16D—C16—H16E	109.5
H1′2—C1′—H1′3	109.5	C15—C16—H16F	109.5
C2-C1-H1A	109.5	H16D—C16—H16F	109.5
C2—C1—H1B	109.5	H16E—C16—H16F	109.5
H1A—C1—H1B	109.5	C22'—C17'—N1'	121.4 (2)
C2-C1-H1C	109.5	C22′—C17′—C18′	116.4 (2)
H1A—C1—H1C	109.5	N1′—C17′—C18′	122.2 (2)
H1B—C1—H1C	109.5	C22—C17—N1	121.7 (2)
C3—C2—C7	117.5 (2)	C22—C17—C18	116.6 (2)
C3—C2—C1	120.9 (2)	N1—C17—C18	121.7 (2)
C7—C2—C1	121.5 (2)	C19—C18—C17	120.6 (2)
C3'—C2'—C7'	118.2 (2)	C19—C18—S1	116.76 (18)
C3'—C2'—C1'	120.9 (2)	C17—C18—S1	122.50 (18)
C7'—C2'—C1'	120.8 (2)	C19′—C18′—C17′	120.9 (2)
	· /		· /

C4'—C3'—C2'	121.2 (2)	C19'—C18'—S1'	116.20 (18)
C4'—C3'—H3'	119.4	C17'-C18'-S1'	122.74 (18)
C2'-C3'-H3'	119.4	C18'-C19'-C20'	122.1(2)
C4-C3-C2	122.0(2)	C18'-C19'-H19'	119.0
C4—C3—H3	119.0	C20'-C19'-H19'	119.0
C2_C3_H3	119.0	C_{18} C_{19} C_{20}	1222(2)
$C_{2}^{2} = C_{3}^{2} = C_{4}^{2} = C_{5}^{2}$	120.7(2)	C18 - C19 - H19	112.2 (2)
$C_3' = C_4' = C_3'$	110.7	C_{10} C_{10} H_{10}	118.0
$C_{2} = C_{4} = H_{4}$	110.7	$C_{20} = C_{10} = III_{20}$	117.4(2)
$C_3 = C_4 = 114$	119.7	$C_{21} = C_{20} = C_{13}$	117.4(2) 124.8(2)
$C_3 = C_4 = C_3$	120.2 (2)	$C_{21} = C_{20} = C_{23}$	124.0(2)
C_{5} C_{4} H_{4}	119.9	C19 - C20 - C23	117.7(2)
C3-C4-H4	119.9	$C_{21} = C_{20} = C_{19}$	117.4 (2)
$C_{6} - C_{5} - C_{4}$	118.1 (2)	$C_{21} = C_{20} = C_{23}$	124.4 (2)
C6—C5—C8	123.8 (2)	C19—C20—C23	118.1 (2)
C4—C5—C8	118.1 (2)	C22—C21—C20	120.9 (2)
C4′—C5′—C6′	118.3 (2)	C22—C21—H21	119.5
C4'—C5'—C8'	118.9 (2)	C20—C21—H21	119.5
C6'—C5'—C8'	122.7 (2)	C20'—C21'—C22'	121.2 (2)
C7'—C6'—C5'	120.4 (2)	C20'—C21'—H21'	119.4
С7'—С6'—Н6'	119.8	C22'—C21'—H21'	119.4
С5'—С6'—Н6'	119.8	C21'—C22'—C17'	122.0 (2)
C7—C6—C5	121.0 (2)	C21'—C22'—H22'	119.0
С7—С6—Н6	119.5	C17'—C22'—H22'	119.0
С5—С6—Н6	119.5	C21—C22—C17	122.1 (2)
C6—C7—C2	121.1 (2)	C21—C22—H22	118.9
С6—С7—Н7	119.5	С17—С22—Н22	118.9
С2—С7—Н7	119.5	O2—C23—C20	120.2 (2)
C6'—C7'—C2'	121.2 (2)	O2—C23—C24	118.8 (2)
C6'—C7'—H7'	119.4	C20—C23—C24	120.9 (2)
C2' - C7' - H7'	119.4	02'-023'-020'	120.3(2)
01 - C8 - C9	1199(2)	02' - C23' - C24'	1192(2)
01 - 08 - 05	1200(2)	$C_{20}' - C_{23}' - C_{24}'$	119.2(2) 1204(2)
C9-C8-C5	120.0(2) 120.1(2)	$C_{20} = C_{23} = C_{24}$	120.4(2) 1184(2)
01' $01'$ $01'$	120.1(2) 120.3(2)	$C_{29} C_{24} C_{23}$	110.4(2) 122.0(2)
01' - 00' - 00'	120.5(2) 110 5 (2)	$C_{25} = C_{24} = C_{23}$	122.0(2) 1103(2)
$C_{0}^{0} = C_{0}^{0} = C_{0}^{0}$	119.3(2) 120.2(2)	$C_{25} = C_{24} = C_{25}$	119.5(2)
$C_{9} = C_{8} = C_{5}$	120.2(2)	$C_{23} = C_{24} = C_{29}$	110.3(2)
C14 - C9 - C10	117.1(2)	$C_{23} = C_{24} = C_{23}$	119.7(2)
C14 - C9 - C8	123.2 (2)	$C_{29} = C_{24} = C_{23}$	121.7(2)
C10-C9-C8	119.3 (2)	$C_{26} = C_{25} = C_{24}$	120.6 (3)
C14'-C9'-C10'	117.3 (2)	C26'-C25'-H25'	119.7
C14'-C9'-C8'	124.0 (2)	C24'—C25'—H25'	119.7
C10'—C9'—C8'	118.5 (2)	C26—C25—C24	120.4 (3)
C11'-C10'-C9'	122.0 (2)	C26—C25—H25	119.8
C11'—C10'—H10'	119.0	C24—C25—H25	119.8
C9'—C10'—H10'	119.0	C25—C26—C27	121.5 (2)
C11—C10—C9	122.1 (2)	C25—C26—H26	119.2
C11—C10—H10	118.9	C27—C26—H26	119.2
C9-C10-H10	118.9	C25'—C26'—C27'	121.1 (3)

C10-C11-C12	120.9 (2)	C25'—C26'—H26'	119.5
C10-C11-S1	116.79 (18)	C27'—C26'—H26'	119.5
C12—C11—S1	122.12 (18)	C26—C27—C28	117.6 (2)
C10'—C11'—C12'	120.7 (2)	C26—C27—C30	121.9 (3)
C10′—C11′—S1′	116.28 (18)	C28—C27—C30	120.5 (3)
C12'-C11'-S1'	122.64 (18)	$C_{28'} - C_{27'} - C_{26'}$	1180(3)
C13'-C12'-N1'	121.0(2)	$C_{28}' - C_{27}' - C_{30}'$	1211(3)
C13' - C12' - C11'	1167(2)	$C_{26} = C_{27} = C_{30}$	1209(3)
N1' - C12' - C11'	1223(2)	C_{29} C_{28} C_{27}	120.5(3)
C_{12} C_{12} C_{11}	122.5(2) 116 5 (2)	$C_{29} C_{28} H_{28}$	110.3
C_{13} C_{12} C_{11} C_{12} C_{11}	110.3(2) 121.2(2)	$C_{27} = C_{28} = H_{28}$	110.3
$C_{11} = C_{12} = N_1$	121.2(2) 122.2(2)	$C_{27} = C_{28} = 1128$	119.5 121.5(2)
C14' - C12' - C12'	122.2(2) 121.6(2)	$C_{27} = C_{28} = C_{29}$	121.3(3)
C14 - C13 - C12	121.0 (2)	$C_{27} - C_{28} - H_{28}$	119.2
C14	119.2	$C_{29} = C_{28} = H_{28}$	119.2
$C12^{2}$ — $C13^{2}$ —H13^{2}	119.2	$C_{28} = C_{29} = C_{24}$	120.3 (3)
C14—C13—C12	121.9 (2)	C28'—C29'—H29'	119.8
C14—C13—H13	119.0	C24'—C29'—H29'	119.8
C12—C13—H13	119.0	C28—C29—C24	120.5 (2)
C13—C14—C9	121.3 (2)	С28—С29—Н29	119.8
C13—C14—H14	119.4	С24—С29—Н29	119.8
C9—C14—H14	119.4	C27'—C30'—H30A	109.5
C9'—C14'—C13'	121.6 (2)	С27'—С30'—Н30В	109.5
C9'—C14'—H14'	119.2	H30A—C30′—H30B	109.5
C13'—C14'—H14'	119.2	С27'—С30'—Н30С	109.5
N1—C15—C16	113.7 (2)	H30A—C30′—H30C	109.5
N1—C15—H15A	108.8	H30B—C30′—H30C	109.5
C16—C15—H15A	108.8	C27—C30—H30D	109.5
N1—C15—H15B	108.8	С27—С30—Н30Е	109.5
C16—C15—H15B	108.8	H30D-C30-H30E	109.5
H15A—C15—H15B	107.7	C27—C30—H30F	109.5
N1'-C15'-C16'	113.1 (2)	H30D-C30-H30F	109.5
N1′—C15′—H15C	109.0	H30E—C30—H30E	109.5
C16'-C15'-H15C	109.0	C17 - N1 - C12	122.98 (18)
N1'-C15'-H15D	109.0	C17 - N1 - C15	122.90(10) 117.77(19)
C16'-C15'-H15D	109.0	C12 - N1 - C15	117.40(19)
H_{15} C_{15} H_{15}	107.8	C17' N1' $C12'$	117.40(19) 123.24(10)
$C_{15'} = C_{15'} = H_{16A}$	109.5	C17' = N1' = C12'	123.24(19) 117.77(18)
$C_{15} = C_{16} = H_{16}$	109.5	C12' = N1' = C15'	117.77(10)
$H_{16} = C_{16} = H_{16} B$	109.5	$C_{12} = N_1 = C_{13}$	117.00(10)
$\begin{array}{c} HIOA-CIO & -HIOB \\ CISI & CIOI & HIOC \\ \end{array}$	109.5	CII - SI - CI8	100.02(11)
C15'-C16'-H16C	109.5	$C18^{2}-S1^{2}-C11^{2}$	100.88 (11)
	0.0 (4)		10(4)
$C_{1}^{2} - C_{2}^{2} - C_{3}^{2} - C_{4}^{2}$	-0.8(4)	C18 - C19 - C20 - C21	-1.2 (4)
C1'-C2'-C3'-C4'	1//.3 (2)	C18 - C19 - C20 - C23	-178.3(2)
C/C2C3C4	2.1 (4)	C19—C20—C21—C22	-1.8 (4)
C1—C2—C3—C4	-175.8 (2)	C23—C20—C21—C22	175.0 (2)
C2'—C3'—C4'—C5'	-1.0 (4)	C19'—C20'—C21'—C22'	0.5 (4)
C2—C3—C4—C5	0.4 (4)	C23'—C20'—C21'—C22'	-175.1 (3)
C3—C4—C5—C6	-2.1 (4)	C20′—C21′—C22′—C17′	-0.1(4)

$C_{3} - C_{4} - C_{5} - C_{8}$	179 8 (2)	N1′—C17′—C22′—C21′	1791(2)
$C_{3'} - C_{4'} - C_{5'} - C_{6'}$	1,5,6(2)	$C_{18'} = C_{17'} = C_{27'} = C_{21'}$	-12(4)
$C_{3'} - C_{4'} - C_{5'} - C_{8'}$	1.3(1) 178 5 (2)	C_{20} C_{21} C_{22} C_{21} C_{20} C_{21} C_{22} C_{17}	23(4)
$C_{4'} = C_{5'} = C_{6'} = C_{7'}$	-0.3(4)	N1 - C17 - C22 - C21	-1785(2)
$C^{*} - C^{*} - C^{*} - C^{*} - C^{*}$	-1772(2)	$C_{18} = C_{17} = C_{22} = C_{21}$	170.3(2)
$C_{1}^{4} = C_{2}^{5} = C_{1}^{6} = C_{1}^{7}$	177.2(2)	$C_{10} = C_{17} = C_{22} = C_{21}$	-161.0(3)
$C_{1}^{*} = C_{2}^{*} = C_{2}^{*} = C_{2}^{*}$	1.5(4) 170 2 (2)	$C_{21} - C_{20} - C_{23} - O_{2}$	150(4)
$C_{0} = C_{0} = C_{0} = C_{1}$	179.2(2) 1 3 (4)	$C_{19} = C_{20} = C_{23} = C_{24}$	13.0(4)
$C_{3} = C_{2} = C_{7} = C_{2}$	-2.9(4)	$C_{21} = C_{20} = C_{23} = C_{24}$	-1644(2)
$C_{3} = C_{2} = C_{7} = C_{0}$	2.9(4)	C19 - C20 - C23 - C24	104.4(2)
$C_1 = C_2 = C_1 = C_0$	1/4.9(3)	$C_{21} - C_{20} - C_{23} - O_{2}$	107.4(3)
$C_{3} = C_{6} = C_{7} = C_{2}$	-1.4(4)	C19 - C20 - C23 - O2	-8.2(4)
$C_3 - C_2 - C_7 - C_6$	2.0(4)	$C_{21} - C_{20} - C_{23} - C_{24}$	-11.1 (4)
$C1^{\prime} - C2^{\prime} - C6^{\prime}$	-1/6.1(3)	C19' - C20' - C23' - C24'	1/3.3(2)
C6-C5-C8-01	-141.5(3)	02-023-024-029	-135.8 (3)
C4—C5—C8—O1	36.5 (4)	C20—C23—C24—C29	43.5 (4)
C6—C5—C8—C9	40.9 (4)	O2—C23—C24—C25	38.8 (4)
C4—C5—C8—C9	-141.2 (2)	C20—C23—C24—C25	-141.8(2)
C4'—C5'—C8'—O1'	-33.8 (3)	O2'—C23'—C24'—C25'	-42.2 (4)
C6'—C5'—C8'—O1'	143.0 (3)	C20'—C23'—C24'—C25'	136.3 (3)
C4'—C5'—C8'—C9'	145.3 (2)	O2'—C23'—C24'—C29'	133.6 (3)
C6'—C5'—C8'—C9'	-37.8 (3)	C20'—C23'—C24'—C29'	-47.9 (4)
O1—C8—C9—C14	-156.1 (3)	C29'—C24'—C25'—C26'	0.2 (4)
C5—C8—C9—C14	21.6 (4)	C23'—C24'—C25'—C26'	176.2 (3)
O1—C8—C9—C10	17.4 (4)	C29—C24—C25—C26	1.1 (4)
C5—C8—C9—C10	-165.0 (2)	C23—C24—C25—C26	-173.8 (2)
O1′—C8′—C9′—C14′	155.5 (2)	C24—C25—C26—C27	2.1 (4)
C5'—C8'—C9'—C14'	-23.7 (4)	C24'—C25'—C26'—C27'	-1.4(5)
O1′—C8′—C9′—C10′	-18.4 (4)	C25—C26—C27—C28	-3.0 (4)
C5'—C8'—C9'—C10'	162.5 (2)	C25—C26—C27—C30	174.7 (2)
C14′—C9′—C10′—C11′	-2.3 (4)	C25'—C26'—C27'—C28'	1.1 (5)
C8′—C9′—C10′—C11′	171.9 (2)	C25'—C26'—C27'—C30'	-179.0 (3)
C14—C9—C10—C11	1.8 (4)	C26—C27—C28—C29	1.0 (4)
C8—C9—C10—C11	-172.1 (2)	C30—C27—C28—C29	-176.8 (2)
C9—C10—C11—C12	-2.0 (4)	C26'—C27'—C28'—C29'	0.3 (5)
C9—C10—C11—S1	173.12 (19)	C30'—C27'—C28'—C29'	-179.5 (3)
C9′—C10′—C11′—C12′	2.4 (4)	C27'—C28'—C29'—C24'	-1.5 (4)
C9′—C10′—C11′—S1′	-170.67 (19)	C25'—C24'—C29'—C28'	1.2 (4)
C10′—C11′—C12′—C13′	-0.1(3)	C23'—C24'—C29'—C28'	-174.7(3)
S1'-C11'-C12'-C13'	172.56 (18)	C_{27} C_{28} C_{29} C_{24}	2.1 (4)
C10'-C11'-C12'-N1'	-1780(2)	$C_{25} - C_{24} - C_{29} - C_{28}$	-31(4)
S1'-C11'-C12'-N1'	-54(3)	C_{23} C_{24} C_{29} C_{28}	1716(2)
C10-C11-C12-C13	0.0(3)	$C_{22} = C_{12} = C$	1612(2)
S1-C11-C12-C13	-174.90(18)	$C_{18} - C_{17} - N_{1} - C_{12}$	-17.6(3)
C10-C11-C12-N1	179.2 (2)	C_{22} C_{17} N_{1} C_{12}	-29(3)
S1-C11-C12-N1	43(3)	C_{18} C_{17} N_{1} C_{15}	1783(2)
N1'-C12'-C13'-C14'	175 7 (2)	C_{13} C_{12} N_{1} C_{13}	-1611(2)
C11'-C12'-C13'-C14'	-23(4)	C11 - C12 - N1 - C17	107.1(2)
$C_{11} = C_{12} = C_{13} = C_{14}$	2.3(T)	$C_{12} - C_{12} - N_1 - C_{17}$	30(3)
011 - 012 - 013 - 017	2·· J (T)	013 - 012 - 101 - 013	5.0 (5)

N1-C12-C13-C14 $C12-C13-C14-C9$ $C10-C9-C14-C13$ $C8-C9-C14-C13$ $C10'-C9'-C14'-C13'$ $C12'-C13'-C14'-C13'$ $C12'-C13'-C14'-C9'$ $C22-C17-C18-C19$ $N1-C17-C18-S1$ $N1-C17-C18-S1$ $C22'-C17'-C18'-C19'$ $N1'-C17'-C18'-C19'$ $N1'-C17'-C18'-C19'$	-177.0 (2) -2.5 (4) 0.5 (4) 174.1 (2) -0.1 (4) -174.0 (2) 2.5 (4) -3.3 (3) 175.6 (2) 173.00 (18) -8.1 (3) 2.1 (3) -178.2 (2)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	-176.1 (2) 81.4 (3) -83.6 (3) -164.4 (2) 15.9 (3) 2.2 (3) -177.5 (2) 165.8 (2) -16.3 (3) -0.8 (3) 177.1 (2) -83.7 (3) 83.7 (3)
N1-C17-C18-S1 C22'-C17'-C18'-C19' N1'-C17'-C18'-C19' C22'-C17'-C18'-S1' N1'-C17'-C18'-S1' C17'-C18'-C19'-C20' S1'-C18'-C19'-C20' S1-C18-C19-C20 S1-C18-C19-C20 C18'-C19'-C20'-C21' C18'-C19'-C20'-C23'	$\begin{array}{c} -8.1 (3) \\ 2.1 (3) \\ -178.2 (2) \\ -173.43 (19) \\ 6.2 (3) \\ -1.9 (4) \\ 174.0 (2) \\ 3.9 (4) \\ -172.67 (18) \\ 0.5 (4) \\ 176.4 (2) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$177.1 (2) \\ -83.7 (3) \\ 83.7 (3) \\ 162.02 (19) \\ -22.9 (2) \\ -158.69 (18) \\ 24.9 (2) \\ 162.75 (19) \\ -21.5 (2) \\ -165.95 (19) \\ 21.1 (2)$

Hydrogen-bond geometry (Å, °)

Cg2 and Cg3 are the centroids of rings C2–C7 (molecule *A*) and C2'–C7' (molecule *B*), respectively.

D—H···A	D—H	H···A	D····A	D—H··· A
C4′—H4′…O1′ ⁱ	0.93	2.55	3.325 (3)	141
C30—H30 <i>F</i> … <i>C</i> g2 ⁱⁱ	0.96	2.98	3.716 (3)	134
C1—H1 <i>A</i> ··· <i>Cg</i> 3	0.96	2.91	3.667 (4)	137

Symmetry codes: (i) -x, -y, -z+1; (ii) x, -y+3/2, z-1/2.