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Dibenzo[2,3:6,7]thiepino[4,5-*d*][1,2,3]selenadiazole

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Four tetracyclic molecules of the title compound, $C_{14}H_8N_2SSe$, are present in the asymmetric unit. Their molecular structures are very similar, adopting the shape of a saddle. The selenadiazole moiety of one of the molecules is disordered over two set of sites [occupancy ratio 0.618 (6):0.382 (6)]. In the crystal, layers of molecules with hydrogen surfaces extend parallel to the *ab* plane and are stacked along the *c* axis. The crystal studied was refined as an inversion twin.



Structure description

1,2,3-Selenadiazoles are useful precursors for strained cycloalkynes (Bissinger *et al.*, 1988; Detert & Meier, 1997) and heterocycles (Detert *et al.* 1992), and are precursors for photochemically induced (Jedináková *et al.*, 2016) as well as for strain-accelerated click-reactions (Jewett & Bertozzi, 2010).

Sixteen molecules, *i.e.* four sets of four independent molecules, of the title compound fill the unit cell (Z' = 4). The forms of all four molecules are nearly identical (Fig. 1). Molecule A is nearly identical to molecule B, and molecule D is nearly identical to molecule C. However, molecules A and D are pseudo-mirror images. The selenadiazole moiety of molecule D is disordered over two sets of sites, with the ratio D (major component):E (minor component) being 0.618 (6):0.382 (6). The molecular shape of these tetracycles is that of a saddle, with the sulfur atom being the pommel, the selenadiazole moiety the cantle and the benzene rings the flaps. Representative for the nearly identical parts in molecules A-E, only details for A are given. The mean planes of the benzene rings are inclined by an angle of 63.7 (7)°. Although the five-membered diphenyl-1,2,3-selenadiazole unit is not symmetrical, the dihedral angles between the mean planes of neighbouring rings are virtually the same: (C1–C6)–selenadiazole: 40.7 (7)° and selenadiazole–(C8–C13): 39.3 (7)°. The C–S–C bond angle at the sulfur atom [99.5 (7)°] is significantly larger than the N–Se–C bond angle of 87.2 (6)°. The





Figure 1

The structures of the four molecules present in the asymmetric unit of the title compound. Displacement ellipsoids are drawn at the 50% probability level. The minor disorder component is shown with dashed lines.

latter is close to the corresponding angle in a 3-methyl-1,2,3-selenadiazolium salt [89.1 (4) $^{\circ}$; Schollmeyer & Detert, 2016].

In the crystal structure (Fig. 2), the molecules are packed according to their molecular shape, forming layers parallel to the ab plane. These layers have hydrogen surfaces and are stacked along the c axis.

Crystal data	
Chemical formula	$C_{14}H_8N_2SSe$
M _r	315.24
Crystal system, space group	Orthorhombic, Pna21
Temperature (K)	193
a, b, c (Å)	20.8533 (8), 9.9698 (3), 23.4151 (8)
$V(Å^3)$	4868.1 (3)
Ζ	16
Radiation type	Μο Κα
$\mu (\text{mm}^{-1})$	3.24
Crystal size (mm)	$0.34 \times 0.26 \times 0.05$
Data collection	
Diffractometer	Stoe IPDS 2T
Absorption correction	Integration (X-RED32; Stoe & Cie 2006)
T_{\min}, T_{\max}	0.406, 0.689
No. of measured, independent and observed $[I > 2\sigma(I)]$ reflections	28240, 12118, 8561
R _{int}	0.058
$(\sin \theta / \lambda)_{\max} (\text{\AA}^{-1})$	0.674
Refinement	
$R[F^2 > 2\sigma(F^2)], wR(F^2), S$	0.080, 0.189, 1.16
No. of reflections	12118
No. of parameters	666
No. of restraints	33
H-atom treatment	H-atom parameters constrained
$\Delta \rho_{\rm max}, \Delta \rho_{\rm min} ({\rm e} {\rm \AA}^{-3})$	0.71, -0.90
Absolute structure	Refined as an inversion twin
Absolute structure parameter	0.41 (2)

Computer programs: X-AREA (Stoe & Cie, 2006), X-RED32 (Stoe & Cie, 2006), SHELXT2014 (Sheldrick, 2015a), SHELXL2017 (Sheldrick, 2015b), PLATON (Spek, 2009), publCIF (Westrip, 2010).



Table 1

Experimental details.

Figure 2

The crystal packing in the title compound in a view along the *a* axis. The four independent molecules are shown in different colours.

Synthesis and crystallization

The title compound was prepared in seven steps from *o*-phenylthiobenzoic acid according to Jílek *et al.* (1965) and Lorch & Meier (1981). ¹H NMR (CDCl₃, 400 MHz): 8.17 (*dd*, 1 H), 7.71 (m, 2 H), 7.53-7.43 (*m*, 4 H), 7.33 (*ddd*, 1 H); ⁷⁷Se NMR (CDCl₃, 76.3 MHz, δ SeO₂/D₂O) = 0 p.p.m.): δ = 257.3 p.p.m. The title compound was recrystallized from chloroform/ 2-propanol (1:1, *v*:*v*) to give light-yellow crystals; m.p. = 413 K.

Refinement

Crystal data, data collection and structure refinement details are summarized in Table 1. The two N atoms and the Se atoms of the five membered seleneadiazole ring of molecule D are disordered over two sets of sites with a refined occupancy ratio of 0.618 (6)/0.382 (6). The C–N and N–N bond lengths inside the ring were restrained to be equal. RIGU and EADP instructions were used for the corresponding ring atoms. Refinement as a inversion twin with a BASF value of 0.41 (2) improved the final reliability factor by 0.35%. References

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full crystallographic data

IUCrData (2018). 3, x180070 [https://doi.org/10.1107/S2414314618000706]

Dibenzo[2,3:6,7]thiepino[4,5-d][1,2,3]selenadiazole

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Dibenzo[2,3:6,7]thiepino[4,5-d][1,2,3]selenadiazole

Crystal data C14H8N2SSe $M_r = 315.24$ Orthorhombic, $Pna2_1$ a = 20.8533 (8) Å *b* = 9.9698 (3) Å c = 23.4151 (8) Å V = 4868.1 (3) Å³ Z = 16F(000) = 2496

Data collection

Stoe IPDS 2T diffractometer Radiation source: sealed X-ray tube, 12 x 0.4 mm long-fine focus Detector resolution: 6.67 pixels mm⁻¹ rotation method scans Absorption correction: integration (X-RED32; Stoe & Cie, 2006) $T_{\rm min} = 0.406, \ T_{\rm max} = 0.689$

Refinement

Refinement on F^2 Hydrogen site location: inferred from Least-squares matrix: full neighbouring sites $R[F^2 > 2\sigma(F^2)] = 0.080$ H-atom parameters constrained $wR(F^2) = 0.189$ $w = 1/[\sigma^2(F_0^2) + (0.0335P)^2 + 36.2917P]$ where $P = (F_0^2 + 2F_c^2)/3$ *S* = 1.16 12118 reflections $(\Delta/\sigma)_{\rm max} < 0.001$ $\Delta \rho_{\rm max} = 0.71 \ {\rm e} \ {\rm \AA}^{-3}$ 666 parameters $\Delta \rho_{\rm min} = -0.90 \ {\rm e} \ {\rm \AA}^{-3}$ 33 restraints

Special details

Geometry. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Refinement. Refined as a 2-component inversion twin

 $D_{\rm x} = 1.721 {\rm Mg m^{-3}}$ Melting point: 413 K Mo *K* α radiation, $\lambda = 0.71073$ Å Cell parameters from 38903 reflections $\theta = 2.0 - 28.3^{\circ}$ $\mu = 3.24 \text{ mm}^{-1}$ T = 193 KPlate, light yellow $0.34\times0.26\times0.05~mm$

28240 measured reflections 12118 independent reflections 8561 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.058$ $\theta_{\rm max} = 28.6^{\circ}, \ \theta_{\rm min} = 2.0^{\circ}$ $h = -27 \rightarrow 26$ $k = -11 \rightarrow 13$ $l = -31 \rightarrow 31$

Absolute structure: Refined as an inversion twin Absolute structure parameter: 0.41 (2)

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
Se1A	0.05143 (8)	0.45875 (16)	0.54238 (7)	0.0493 (4)	
C1A	0.0215 (7)	0.5129 (13)	0.4230 (7)	0.039 (3)	
C2A	-0.0007 (7)	0.6410 (15)	0.4345 (8)	0.047 (4)	
H2A	-0.012930	0.664452	0.472250	0.056*	
C3A	-0.0051 (7)	0.7355 (16)	0.3911 (8)	0.050 (4)	
H3A	-0.020032	0.823479	0.399162	0.061*	
C4A	0.0123 (8)	0.7008 (18)	0.3357 (8)	0.051 (4)	
H4A	0.008540	0.764993	0.305914	0.061*	
C5A	0.0347 (8)	0.5754 (16)	0.3237 (8)	0.050 (4)	
H5A	0.047064	0.553217	0.285857	0.060*	
C6A	0.0394 (7)	0.4790 (14)	0.3672 (7)	0.041 (3)	
S7A	0.07130 (19)	0.3183 (4)	0.3501 (2)	0.0475 (9)	
C8A	0.0029 (7)	0.2171 (14)	0.3656 (7)	0.042 (3)	
C9A	-0.0228 (7)	0.1421 (14)	0.3223 (7)	0.043 (3)	
H9A	-0.006455	0.150252	0.284574	0.051*	
C10A	-0.0736 (7)	0.0529 (15)	0.3338 (7)	0.044 (4)	
H10A	-0.092918	0.003662	0.303604	0.052*	
C11A	-0.0945 (7)	0.0377 (15)	0.3879 (7)	0.042 (3)	
H11A	-0.126862	-0.026769	0.395763	0.051*	
C12A	-0.0701 (7)	0.1132 (15)	0.4320 (7)	0.042 (3)	
H12A	-0.087109	0.104390	0.469415	0.050*	
C13A	-0.0195 (7)	0.2044 (14)	0.4210 (6)	0.037 (3)	
C14A	0.0083 (6)	0.2796 (14)	0.4697 (6)	0.037 (3)	
C15A	0.0260 (6)	0.4132 (13)	0.4687 (7)	0.039 (3)	
N16A	0.0135 (6)	0.2135 (13)	0.5210 (6)	0.044 (3)	
N17A	0.0339 (7)	0.2808 (13)	0.5628 (6)	0.047 (3)	
Se1B	0.17948 (8)	0.44736 (17)	-0.03038 (8)	0.0527 (4)	
C1B	0.1465 (7)	0.5053 (15)	0.0877 (8)	0.045 (4)	
C2B	0.1273 (7)	0.6349 (16)	0.0762 (8)	0.049 (4)	
H2B	0.116688	0.658540	0.038027	0.058*	
C3B	0.1230 (8)	0.7319 (16)	0.1185 (9)	0.053 (4)	
H3B	0.110984	0.820843	0.108665	0.064*	
C4B	0.1360 (8)	0.7010 (18)	0.1742 (10)	0.057 (5)	
H4B	0.132583	0.767475	0.203078	0.068*	
C5B	0.1544 (8)	0.5700 (16)	0.1880 (7)	0.047 (4)	
H5B	0.162552	0.546371	0.226639	0.056*	
C6B	0.1607 (7)	0.4747 (14)	0.1451 (8)	0.043 (3)	
S7B	0.19277 (19)	0.3150 (4)	0.1643 (2)	0.0484 (10)	
C8B	0.1270 (6)	0.2093 (13)	0.1468 (7)	0.040 (3)	
C9B	0.1004 (7)	0.1329 (16)	0.1929 (8)	0.045 (4)	
H9B	0.114887	0.143828	0.231084	0.054*	
C10B	0.0516 (7)	0.0406 (15)	0.1788 (7)	0.044 (3)	
H10B	0.033834	-0.014707	0.207743	0.053*	
C11B	0.0290 (7)	0.0293 (14)	0.1226 (7)	0.041 (3)	
H11B	-0.004845	-0.030958	0.113904	0.050*	

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\hat{A}^2)

C12B	0.0560 (7)	0.1054 (15)	0.0804 (7)	0.042 (3)	
H12B	0.040790	0.096279	0.042379	0.050*	
C13B	0.1053 (6)	0.1963 (14)	0.0918 (7)	0.038 (3)	
C14B	0.1346 (6)	0.2741 (13)	0.0429 (7)	0.037(3)	
C15B	0.1516(7)	0.4067 (14)	0.0420 (7)	0.044 (3)	
N16B	0 1405 (6)	0 2060 (13)	-0.0067(6)	0.043(3)	
N17B	0 1618 (7)	0.2679(14)	-0.0504(7)	0.054(3)	
Se1C	0 33561 (7)	0 52544 (15)	0 14539 (8)	0.0476(4)	
CIC	0 2971 (6)	0 7737 (14)	0.0899(6)	0.037(3)	
C2C	0.2971(0)	0.7166 (16)	0.0362(8)	0.037(3)	
H2C	0.316441	0.633824	0.029887	0.059*	
C3C	0.2626 (9)	0.055024	-0.0090(8)	0.057(5)	
H3C	0.260555	0.734853	-0.045433	0.069*	
C4C	0.2329 (8)	0.9006 (19)	0.043433	0.002(4)	
H4C	0.211807	0.9000 (19)	-0.020326	0.052 (4)	
C5C	0.211097 0.2333(7)	0.945020	0.029320	0.003	
U5C	0.2333 (7)	0.9395 (17)	0.050947	0.052 (4)	
	0.211990	1.042020	0.039847	0.002	
C0C	0.2039(0)	0.0932(14)	0.0997(7) 0.16780(10)	0.038(3)	
S/C	0.20304(17)	1.0082(14)	0.10780(19) 0.1720(7)	0.0401(3)	
	0.3409(7)	1.0082(14) 1.1445(16)	0.1729(7) 0.1751(7)	0.042(3)	
	0.3030 (8)	1.1445 (10)	0.1751(7)	0.049 (4)	
CIOC	0.333483	1.2123/3	0.1/0022	0.058	
	0.4289 (9)	1.1790 (18)	0.1838 (8)	0.058 (5)	
HIOC	0.440448	1.2/1401	0.187192	0.069*	
	0.4759 (8)	1.081/(18)	0.18/4 (/)	0.052 (4)	
HIIC	0.519689	1.105663	0.191688	0.063*	
C12C	0.4575 (8)	0.9463 (16)	0.1848 (7)	0.046 (4)	
HI2C	0.489243	0.8/8414	0.188238	0.055*	
C13C	0.3940 (7)	0.9097 (16)	0.1772 (6)	0.039 (3)	
C14C	0.3768 (6)	0.7672 (14)	0.1725 (7)	0.035 (3)	
C15C	0.3342 (6)	0.7100 (14)	0.1355 (7)	0.040 (3)	
N16C	0.4114 (6)	0.6782 (13)	0.2063 (6)	0.046 (3)	
N17C	0.3994 (6)	0.5515 (12)	0.2006 (6)	0.047 (3)	
Se1D	0.20970 (16)	0.5125 (3)	0.35682 (17)	0.0487 (10)	0.618 (6)
Se1E	0.2824 (5)	0.6295 (9)	0.2903 (4)	0.051 (2)	0.382 (6)
C1D	0.1705 (7)	0.7708 (14)	0.4123 (7)	0.040 (3)	
C2D	0.1656 (8)	0.7163 (15)	0.4674 (7)	0.048 (4)	
H2D	0.185103	0.632270	0.475315	0.057*	
C3D	0.1331 (9)	0.782 (2)	0.5103 (8)	0.057 (5)	
H3D	0.130491	0.743195	0.547290	0.069*	
C4D	0.1045 (8)	0.9034 (18)	0.4994 (8)	0.054 (4)	
H4D	0.081816	0.948653	0.528863	0.065*	
C5D	0.1085 (7)	0.9587 (17)	0.4466 (8)	0.052 (4)	
H5D	0.088427	1.042690	0.439787	0.062*	
C6D	0.1414 (7)	0.8961 (16)	0.4020 (7)	0.046 (4)	
S7D	0.14250 (18)	0.9657 (4)	0.33250 (19)	0.0480 (9)	
C8D	0.2262 (7)	1.0023 (15)	0.3266 (7)	0.041 (3)	
C9D	0.2462 (8)	1.1366 (18)	0.3245 (8)	0.051 (4)	

				0.0.011	
H9D	0.215960	1.207576	0.326746	0.061*	
C10D	0.3109 (9)	1.1633 (19)	0.3193 (8)	0.061 (5)	
H10D	0.325387	1.253317	0.316121	0.073*	
C11D	0.3537 (8)	1.0609 (18)	0.3185 (8)	0.058 (5)	
H11D	0.398042	1.082280	0.316193	0.070*	
C12D	0.3366 (7)	0.9281 (18)	0.3210 (7)	0.048 (4)	
H12D	0.368128	0.859450	0.318923	0.057*	
C13D	0.2701 (7)	0.8959 (15)	0.3268 (7)	0.042 (3)	
C14D	0.2510 (8)	0.7555 (15)	0.3305 (6)	0.040 (3)	
C15D	0.2079 (7)	0.7001 (13)	0.3679 (7)	0.040 (3)	
N16D	0.288 (2)	0.657 (4)	0.299 (2)	0.038 (5)	0.618 (6)
N17D	0.2742 (13)	0.532 (3)	0.2986 (12)	0.059 (5)	0.618 (6)
N16E	0.204 (2)	0.558 (3)	0.365 (2)	0.038 (5)	0.382 (6)
N17E	0.239 (2)	0.508 (4)	0.325 (2)	0.059 (5)	0.382 (6)

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	<i>U</i> ¹³	<i>U</i> ²³
SelA	0.0528 (9)	0.0437 (8)	0.0515 (9)	-0.0091 (7)	-0.0088 (8)	-0.0013 (8)
C1A	0.036 (7)	0.025 (6)	0.057 (9)	0.010 (5)	-0.005 (6)	0.002 (6)
C2A	0.034 (7)	0.035 (8)	0.072 (12)	0.005 (6)	-0.013 (7)	-0.002 (7)
C3A	0.037 (8)	0.033 (8)	0.082 (13)	-0.001 (6)	-0.009 (8)	0.007 (8)
C4A	0.046 (9)	0.052 (9)	0.055 (11)	0.000(7)	-0.012 (8)	0.020 (8)
C5A	0.034 (8)	0.045 (9)	0.071 (12)	-0.011 (7)	-0.001 (8)	0.000 (8)
C6A	0.035 (7)	0.036 (7)	0.050 (9)	-0.002 (6)	-0.001 (6)	0.001 (7)
S7A	0.040 (2)	0.042 (2)	0.061 (3)	0.0016 (16)	0.0106 (19)	-0.0024 (19)
C8A	0.044 (8)	0.037 (7)	0.046 (8)	0.007 (6)	0.002 (7)	0.000 (7)
C9A	0.044 (8)	0.032 (7)	0.051 (9)	0.006 (6)	-0.008 (7)	0.001 (6)
C10A	0.037 (7)	0.040 (8)	0.054 (9)	0.004 (6)	-0.014 (7)	-0.011 (7)
C11A	0.031 (7)	0.038 (7)	0.058 (9)	0.001 (6)	0.001 (6)	-0.011 (7)
C12A	0.039 (8)	0.037 (8)	0.049 (9)	-0.001 (6)	0.007 (7)	-0.001 (7)
C13A	0.034 (7)	0.030 (7)	0.048 (9)	0.004 (5)	0.002 (6)	-0.003 (6)
C14A	0.034 (7)	0.038 (7)	0.040 (7)	-0.003 (5)	0.000 (6)	0.005 (7)
C15A	0.036 (7)	0.036 (7)	0.045 (8)	0.002 (5)	0.006 (6)	0.004 (7)
N16A	0.040 (7)	0.048 (7)	0.045 (7)	0.002 (6)	-0.003 (6)	-0.001 (6)
N17A	0.043 (7)	0.047 (7)	0.051 (8)	-0.004 (6)	-0.005 (6)	0.001 (6)
Se1B	0.0546 (9)	0.0460 (8)	0.0576 (10)	-0.0042 (7)	0.0079 (8)	0.0039 (8)
C1B	0.032 (7)	0.040 (8)	0.062 (10)	-0.007 (6)	0.001 (7)	0.000 (7)
C2B	0.047 (9)	0.041 (8)	0.058 (11)	0.005 (7)	-0.001 (8)	-0.002 (7)
C3B	0.042 (9)	0.030 (7)	0.088 (13)	0.006 (6)	0.007 (9)	-0.015 (8)
C4B	0.043 (9)	0.042 (9)	0.086 (14)	-0.007 (7)	0.005 (9)	-0.013 (9)
C5B	0.049 (9)	0.044 (8)	0.048 (9)	-0.006 (7)	0.003 (7)	-0.011 (7)
C6B	0.031 (6)	0.041 (7)	0.057 (9)	-0.008 (6)	-0.002 (7)	-0.002 (8)
S7B	0.0357 (18)	0.041 (2)	0.068 (3)	-0.0033 (15)	-0.0106 (18)	0.0054 (18)
C8B	0.028 (6)	0.032 (6)	0.061 (9)	0.009 (5)	-0.009(7)	-0.005 (7)
C9B	0.032 (7)	0.049 (9)	0.054 (10)	0.000 (6)	0.001 (7)	0.003 (7)
C10B	0.037 (8)	0.039 (8)	0.056 (10)	-0.003 (6)	0.008 (7)	0.007 (7)
C11B	0.030 (7)	0.030 (7)	0.064 (10)	-0.004 (5)	0.008 (7)	-0.003 (7)

C12B	0.029 (7)	0.045 (8)	0.052 (9)	0.002 (6)	-0.001 (6)	-0.005 (7)
C13B	0.030 (7)	0.030(7)	0.055 (9)	0.003 (5)	0.003 (6)	0.000 (6)
C14B	0.028 (6)	0.034 (7)	0.048 (8)	0.000 (5)	0.004 (6)	0.001 (7)
C15B	0.041 (8)	0.032 (7)	0.058 (9)	0.011 (6)	-0.007 (7)	0.008 (7)
N16B	0.030 (6)	0.047 (7)	0.053 (8)	0.003 (5)	0.001 (6)	-0.001 (6)
N17B	0.045 (7)	0.049 (8)	0.068 (9)	0.005 (6)	-0.002 (7)	-0.004 (7)
Se1C	0.0406 (8)	0.0325 (6)	0.0695 (10)	0.0016 (6)	-0.0008 (8)	0.0042 (8)
C1C	0.023 (6)	0.036 (7)	0.052 (9)	-0.004 (5)	-0.004 (6)	0.009 (6)
C2C	0.040 (8)	0.043 (8)	0.064 (11)	0.006 (6)	-0.009 (7)	-0.006 (8)
C3C	0.066 (12)	0.054 (10)	0.052 (10)	-0.011 (9)	-0.009 (9)	0.000 (8)
C4C	0.036 (8)	0.066 (11)	0.055 (10)	-0.003 (7)	-0.012 (7)	0.011 (9)
C5C	0.025 (7)	0.054 (10)	0.078 (13)	-0.006 (6)	-0.009 (7)	0.001 (9)
C6C	0.025 (7)	0.037 (7)	0.051 (9)	-0.006 (5)	-0.005 (6)	0.006 (6)
S7C	0.0301 (17)	0.042 (2)	0.066 (3)	0.0062 (14)	0.0034 (16)	-0.0021 (18)
C8C	0.039 (7)	0.030(7)	0.059 (9)	0.002 (6)	0.000(7)	0.005 (6)
C9C	0.045 (9)	0.044 (9)	0.057 (10)	-0.006 (7)	-0.002 (7)	-0.001 (7)
C10C	0.055 (10)	0.047 (9)	0.071 (12)	-0.015 (8)	-0.008 (9)	0.004 (9)
C11C	0.046 (9)	0.055 (10)	0.057 (10)	-0.011 (7)	-0.001 (8)	0.003 (8)
C12C	0.041 (8)	0.048 (9)	0.049 (9)	-0.002 (7)	-0.002 (7)	-0.002 (7)
C13C	0.034 (7)	0.048 (8)	0.037 (8)	-0.008 (6)	0.002 (6)	-0.003 (7)
C14C	0.022 (6)	0.036 (7)	0.047 (8)	0.005 (5)	0.001 (6)	0.004 (6)
C15C	0.026 (6)	0.042 (7)	0.051 (9)	-0.004 (5)	-0.001 (6)	-0.004 (7)
N16C	0.043 (7)	0.046 (7)	0.050 (8)	0.007 (6)	0.005 (6)	0.009 (6)
N17C	0.033 (6)	0.038 (7)	0.070 (9)	0.009 (5)	0.003 (6)	0.009 (6)
Se1D	0.0419 (17)	0.0320 (14)	0.072 (2)	0.0013 (13)	-0.0030 (14)	-0.0002 (15)
Se1E	0.038 (3)	0.060 (6)	0.054 (4)	0.008 (3)	0.001 (3)	-0.015 (3)
C1D	0.034 (7)	0.032 (7)	0.055 (9)	0.003 (5)	-0.002 (7)	-0.002 (6)
C2D	0.056 (10)	0.040 (8)	0.047 (9)	-0.007 (7)	0.000 (8)	0.001 (7)
C3D	0.053 (11)	0.070 (12)	0.049 (10)	-0.013 (9)	0.002 (8)	0.010 (9)
C4D	0.034 (8)	0.060 (11)	0.067 (12)	-0.014 (7)	0.008 (8)	-0.013 (9)
C5D	0.039 (8)	0.044 (9)	0.072 (11)	0.009 (7)	-0.003 (8)	-0.020 (8)
C6D	0.030 (7)	0.042 (8)	0.065 (11)	-0.002 (6)	-0.005 (7)	-0.007 (7)
S7D	0.0354 (19)	0.046 (2)	0.063 (3)	0.0019 (16)	-0.0041 (17)	0.0098 (19)
C8D	0.043 (8)	0.041 (8)	0.040 (8)	-0.016 (6)	0.000 (6)	0.000 (6)
C9D	0.049 (9)	0.046 (9)	0.059 (10)	0.001 (7)	0.002 (8)	0.001 (8)
C10D	0.057 (11)	0.056 (11)	0.070 (12)	-0.024 (9)	0.010 (9)	0.004 (9)
C11D	0.040 (9)	0.059 (11)	0.076 (12)	-0.014 (8)	0.004 (8)	-0.001 (9)
C12D	0.030 (7)	0.063 (10)	0.050 (9)	-0.004 (7)	0.000 (7)	0.001 (8)
C13D	0.035 (7)	0.039 (8)	0.052 (9)	-0.003 (6)	-0.002 (7)	0.004 (7)
C14D	0.043 (8)	0.035 (7)	0.041 (8)	0.000 (6)	-0.002 (6)	0.004 (6)
C15D	0.036 (7)	0.029 (6)	0.054 (9)	0.000 (5)	-0.008 (6)	0.002 (6)
N16D	0.029 (10)	0.034 (8)	0.050 (13)	0.000 (7)	-0.013 (8)	-0.005 (9)
N17D	0.059 (13)	0.039 (8)	0.078 (14)	0.002 (8)	0.006 (8)	-0.009 (8)
N16E	0.029 (10)	0.034 (8)	0.050 (13)	0.000 (7)	-0.013 (8)	-0.005 (9)
N17E	0.059 (13)	0.039 (8)	0.078 (14)	0.002 (8)	0.006 (8)	-0.009 (8)

Geometric parameters (Å, °)

Se1A—C15A	1.862 (16)	C1C—C2C	1.38 (2)	
Se1A—N17A	1.874 (13)	C1C—C6C	1.39 (2)	
C1A—C2A	1.384 (19)	C1C—C15C	1.462 (19)	
C1A—C6A	1.40 (2)	C2C—C3C	1.39 (2)	
C1A—C15A	1.46 (2)	C2C—H2C	0.9500	
C2A—C3A	1.39 (2)	C3C—C4C	1.41 (2)	
C2A—H2A	0.9500	C3C—H3C	0.9500	
C3A—C4A	1.39 (2)	C4C—C5C	1.36 (3)	
СЗА—НЗА	0.9500	C4C—H4C	0.9500	
C4A—C5A	1.36 (2)	C5C—C6C	1.42 (2)	
C4A—H4A	0.9500	C5C—H5C	0.9500	
C5A—C6A	1.40 (2)	C6C—S7C	1.760 (16)	
С5А—Н5А	0.9500	S7C—C8C	1.753 (15)	
C6A—S7A	1.779 (15)	C8C—C13C	1.39 (2)	
S7A—C8A	1.785 (16)	C8C—C9C	1.41 (2)	
C8A—C9A	1.37 (2)	C9C—C10C	1.39 (2)	
C8A—C13A	1.38 (2)	С9С—Н9С	0.9500	
C9A—C10A	1.41 (2)	C10C—C11C	1.38 (2)	
С9А—Н9А	0.9500	C10C—H10C	0.9500	
C10A—C11A	1.35 (2)	C11C—C12C	1.40 (2)	
C10A—H10A	0.9500	C11C—H11C	0.9500	
C11A—C12A	1.37 (2)	C12C—C13C	1.39 (2)	
C11A—H11A	0.9500	C12C—H12C	0.9500	
C12A—C13A	1.42 (2)	C13C—C14C	1.47 (2)	
C12A—H12A	0.9500	C14C—C15C	1.366 (19)	
C13A—C14A	1.48 (2)	C14C—N16C	1.390 (18)	
C14A—N16A	1.373 (18)	N16C—N17C	1.294 (17)	
C14A—C15A	1.383 (18)	Se1D—C15D	1.889 (14)	
N16A—N17A	1.262 (18)	Se1D—N17D	1.93 (3)	
Se1B—C15B	1.836 (17)	Se1E—C14D	1.700 (17)	
Se1B—N17B	1.885 (14)	Se1E—N17E	1.72 (5)	
C1B—C2B	1.38 (2)	C1D—C2D	1.40 (2)	
C1B—C6B	1.41 (2)	C1D—C6D	1.41 (2)	
C1B—C15B	1.46 (2)	C1D—C15D	1.48 (2)	
C2B—C3B	1.39 (2)	C2D—C3D	1.37 (2)	
C2B—H2B	0.9500	C2D—H2D	0.9500	
C3B—C4B	1.37 (3)	C3D—C4D	1.38 (3)	
C3B—H3B	0.9500	C3D—H3D	0.9500	
C4B—C5B	1.40 (2)	C4D—C5D	1.36 (2)	
C4B—H4B	0.9500	C4D—H4D	0.9500	
C5B—C6B	1.39 (2)	C5D—C6D	1.40 (2)	
C5B—H5B	0.9500	C5D—H5D	0.9500	
C6B—S7B	1.783 (16)	C6D—S7D	1.770 (17)	
S7B—C8B	1.777 (14)	S7D—C8D	1.787 (15)	
C8B—C13B	1.37 (2)	C8D—C13D	1.40 (2)	
C8B—C9B	1.43 (2)	C8D—C9D	1.40 (2)	

COB C10B	1 41 (2)		1.38(2)
	0.0500		0.0500
	1.40.(2)		1.26(2)
	1.40(2)		1.50 (5)
CIUB—HIUB	0.9500		0.9500
CIIB—CI2B	1.37 (2)	CIID—CI2D	1.37(2)
CIIB—HIIB	0.9500	CIID—HIID	0.9500
C12B—C13B	1.40 (2)	C12D—C13D	1.43 (2)
C12B—H12B	0.9500	C12D—H12D	0.9500
C13B—C14B	1.51 (2)	C13D—C14D	1.46 (2)
C14B—N16B	1.35 (2)	C14D—C15D	1.37 (2)
C14B—C15B	1.369 (19)	C14D—N16D	1.45 (4)
N16B—N17B	1.273 (19)	C15D—N16E	1.42 (3)
Se1C—C15C	1.855 (15)	N16D—N17D	1.28 (4)
Se1C—N17C	1.874 (14)	N16E—N17E	1.28 (4)
C15A—Se1A—N17A	87.2 (6)	C1C—C2C—C3C	122.1 (15)
C2A—C1A—C6A	119.5 (14)	C1C—C2C—H2C	118.9
C_2A — C_1A — C_15A	120 5 (15)	C3C—C2C—H2C	118.9
C6A - C1A - C15A	120.0(12)	$C_{2}C_{-}C_{3}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{4}C_{-}C_{-}C_{-}C_{4}C_{-}C_{-}C_{-}C_{4}C_{-}C_{-}C_{-}C_{4}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-$	117.5(17)
C1A - C2A - C3A	120.0(12) 120.4(17)	$C_2C_2C_3C_4$	121.2
C1A - C2A - H2A	119.8	C4C-C3C-H3C	121.2
$C_{1}^{3}A = C_{2}^{3}A = H_{2}^{3}A$	110.8	$C_{1}^{2}C_{2}^{2}C$	121.2 122.1(17)
$C_{2A} = C_{2A} = C_{4A}$	119.0	$C_{5C} = C_{4C} = U_{4C}$	122.1 (17)
$C_{2A} = C_{3A} = U_{2A}$	119.0 (10)	$C_{3}C_{-}C_{4}C_{-}H_{4}C_{-}C_{2}C_{-}C_{4}C_{-}H_{4}C_{-}C_{-}C_{2}C_{-}C_{4}C_{-}H_{4}C_{-}C_{-}C_{2}C_{-}C_{4}C_{-}H_{4}C_{-}C_{-}C_{2}C_{-}C_{-}C_{4}C_{-}H_{4}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-$	110.9
C_{2A} — C_{3A} — H_{3A}	120.1	$C_3C - C_4C - H_4C$	118.9
C4A—C3A—H3A	120.1	C4C—C5C—C6C	119.3 (16)
C5A—C4A—C3A	120.6 (16)	С4С—С5С—Н5С	120.3
C5A—C4A—H4A	119.7	C6C—C5C—H5C	120.3
C3A—C4A—H4A	119.7	C1C—C6C—C5C	119.4 (15)
C4A—C5A—C6A	120.2 (17)	C1C—C6C—S7C	121.5 (11)
C4A—C5A—H5A	119.9	C5C—C6C—S7C	119.1 (12)
C6A—C5A—H5A	119.9	C8C—S7C—C6C	98.3 (7)
C1A—C6A—C5A	119.5 (14)	C13C—C8C—C9C	119.2 (14)
C1A—C6A—S7A	121.7 (11)	C13C—C8C—S7C	122.6 (11)
C5A—C6A—S7A	118.8 (13)	C9C—C8C—S7C	118.1 (11)
C6A—S7A—C8A	99.5 (7)	C10C—C9C—C8C	120.2 (16)
C9A—C8A—C13A	120.9 (15)	С10С—С9С—Н9С	119.9
C9A—C8A—S7A	118.1 (12)	С8С—С9С—Н9С	119.9
C13A—C8A—S7A	120.8 (12)	C11C—C10C—C9C	120.5 (16)
C8A—C9A—C10A	119.8 (15)	C11C—C10C—H10C	119.7
С8А—С9А—Н9А	120.1	C9C-C10C-H10C	119 7
C10A - C9A - H9A	120.1	C10C - C11C - C12C	118.8 (15)
$C_{11}A - C_{10}A - C_{9}A$	119.6 (14)	C10C - C11C - H11C	120.6
C_{11A} C_{10A} H_{10A}	120.2		120.0
C_{0A} C_{10A} H_{10A}	120.2	$C_{12}C_{-}C_{11}C_{-}C_{-}C_{11}C_{-}C_{-$	120.0 121.3(16)
$C_{10A} = C_{10A} = m_{0A}$	120.2 121 6 (14)	$C_{13}C_{-}C_{12}C_{-}H_{12}C_{-}$	110 /
C10A = C11A = U11A	121.0 (14)	$C_{11}C = C_{12}C = H_{12}C$	117. 4 110 /
$C_{12A} = C_{11A} = H_{11A}$	117.2	$C_{12}C_{-}C_{12}C_{-}C_{12}C_{-}C_{-}C_{2}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-$	112. 4 110.0 (14)
$C_{12A} = C_{12A} = C_{12A}$	119.2	$C_{12}C_{-}C_{13}C_{-}C_{14}C_{-}C_{14}C_{-}C_{14}C_{-}C_{14}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-}C_{-$	119.9 (14)
UIIA—UI2A—UI3A	119.4 (14)	U12U - U13U - U14U	119./(14)

C11A—C12A—H12A	120.3	C8C—C13C—C14C	120.3 (13)
C13A—C12A—H12A	120.3	C15C—C14C—N16C	115.6 (13)
C8A—C13A—C12A	118.7 (14)	C15C—C14C—C13C	127.6 (14)
C8A - C13A - C14A	123.0(13)	N16C - C14C - C13C	1167(13)
C12A - C13A - C14A	118 4 (13)	C14C - C15C - C1C	1287(14)
N16A - C14A - C15A	1172(14)	C14C— $C15C$ — $Se1C$	108.9(11)
N16A C14A C13A	117.2(14) 117.5(12)	C1C $C15C$ SelC	100.9(11) 122.1(10)
$C_{15A} = C_{14A} = C_{15A}$	117.3(12) 125.3(14)	N17C $N16C$ $C14C$	122.1(10) 117.7(13)
C14A = C15A = C15A	123.3(14) 120.6(15)	N17C - N10C - C14C	117.7(13)
C14A = C15A = C1A	150.0(15)	$\frac{1}{100} - \frac{1}{100} - \frac{1}{100} = \frac{1}{100} - \frac{1}{100} = \frac{1}$	110.0(10)
CI4A—CI5A—SeIA	107.1 (11)	CISD—SelD—NI/D	90.6 (9)
CIA—CI5A—SeIA	122.0 (10)	CI4D—SeIE—NI/E	92.9 (15)
NI/A—NI6A—CI4A	116.8 (13)	C2D—C1D—C6D	117.9 (14)
N16A—N17A—Se1A	111.8 (11)	C2D—C1D—C15D	120.0 (13)
C15B—Se1B—N17B	87.6 (7)	C6D—C1D—C15D	122.0 (14)
C2B—C1B—C6B	116.8 (15)	C3D—C2D—C1D	121.5 (16)
C2B—C1B—C15B	120.6 (15)	C3D—C2D—H2D	119.2
C6B—C1B—C15B	122.6 (14)	C1D—C2D—H2D	119.2
C1B—C2B—C3B	122.1 (17)	C2D-C3D-C4D	119.8 (17)
C1B—C2B—H2B	119.0	C2D—C3D—H3D	120.1
C3B—C2B—H2B	119.0	C4D—C3D—H3D	120.1
C4B—C3B—C2B	120.8 (16)	C5D—C4D—C3D	120.0 (17)
C4B—C3B—H3B	119.6	C5D—C4D—H4D	120.0
C2B—C3B—H3B	119.6	C3D—C4D—H4D	120.0
C3B-C4B-C5B	1191(17)	C4D-C5D-C6D	122.0 (16)
C3B-C4B-H4B	120.5	C4D - C5D - H5D	119.0
C5B-C4B-H4B	120.5	C6D - C5D - H5D	119.0
C6B-C5B-C4B	119.8 (17)	$C_{5}D - C_{6}D - C_{1}D$	118.7 (16)
C6B C5B H5B	119.8 (17)	$C_{5D} = C_{6D} = C_{1D}$	110.7(10) 121.2(13)
C4P $C5P$ $H5P$	120.1	$C_{1D} = C_{0D} = S_{7D}$	121.2(13) 110.0(12)
$C_{4}D - C_{3}D - D_{3}D$	120.1 121.4(15)	C1D = C0D = S7D	119.9(12)
	121.4(13)	C0D = 3/D = C0D	99.4 (7) 101.8 (14)
C_{3B} C_{0B} C_{7B}	11/./ (14)	C13D = C8D = C9D	121.8 (14)
C1B—C6B—S/B	120.8 (12)	C13D—C8D—S7D	118.9 (11)
C8B—S7B—C6B	100.5 (6)	C9D—C8D—S7D	119.2 (13)
C13B—C8B—C9B	122.0 (13)	C10D—C9D—C8D	118.6 (16)
C13B—C8B—S7B	121.7 (12)	C10D—C9D—H9D	120.7
C9B—C8B—S7B	116.2 (12)	C8D—C9D—H9D	120.7
C10B—C9B—C8B	116.7 (15)	C11D—C10D—C9D	119.9 (17)
C10B—C9B—H9B	121.7	C11D—C10D—H10D	120.0
C8B—C9B—H9B	121.7	C9D—C10D—H10D	120.0
C11B—C10B—C9B	121.0 (14)	C10D-C11D-C12D	123.7 (16)
C11B-C10B-H10B	119.5	C10D-C11D-H11D	118.2
C9B-C10B-H10B	119.5	C12D-C11D-H11D	118.2
C12B—C11B—C10B	119.7 (13)	C11D—C12D—C13D	118.2 (16)
C12B—C11B—H11B	120.1	C11D—C12D—H12D	120.9
C10B—C11B—H11B	120.1	C13D—C12D—H12D	120.9
C11B—C12B—C13B	121.7 (15)	C8D—C13D—C12D	117.6 (14)
C11B—C12B—H12B	119.2	C8D—C13D—C14D	123.3 (13)
C13B-C12B-H12B	119.2	C12D— $C13D$ — $C14D$	1191(14)
	· · / · · ·		*****

C8B—C13B—C12B	118.9 (14)	C15D—C14D—N16D	114 (2)
C8B—C13B—C14B	122.0 (13)	C15D—C14D—C13D	127.1 (14)
C12B—C13B—C14B	119.1 (14)	N16D-C14D-C13D	118 (2)
N16B—C14B—C15B	116.6 (15)	C15D—C14D—Se1E	108.0 (11)
N16B—C14B—C13B	115.5 (12)	C13D—C14D—Se1E	124.9 (12)
C15B—C14B—C13B	127.7 (15)	C14D—C15D—N16E	115 (2)
C14B—C15B—C1B	128.4 (16)	C14D—C15D—C1D	127.1 (13)
C14B—C15B—Se1B	108.0 (12)	N16E—C15D—C1D	118 (2)
C1B—C15B—Se1B	123.5 (11)	C14D—C15D—Se1D	107.3 (11)
N17B—N16B—C14B	118.6 (13)	C1D—C15D—Se1D	125.4 (11)
N16B—N17B—Se1B	109.2 (11)	N17D—N16D—C14D	123 (4)
C15C—Se1C—N17C	87.7 (6)	N16D—N17D—Se1D	104 (3)
C2C—C1C—C6C	119.5 (13)	N17E—N16E—C15D	112 (3)
C2C—C1C—C15C	120.1 (13)	N16E—N17E—Se1E	112 (3)
C6C—C1C—C15C	120.3 (14)		
C6A—C1A—C2A—C3A	0(2)	C15C—C1C—C6C—C5C	176.2 (13)
C15A—C1A—C2A—C3A	-179.8 (14)	C2C—C1C—C6C—S7C	178.2 (11)
C1A—C2A—C3A—C4A	1 (2)	C15C—C1C—C6C—S7C	-4.6 (18)
C2A—C3A—C4A—C5A	-1 (2)	C4C—C5C—C6C—C1C	0(2)
C3A—C4A—C5A—C6A	1 (3)	C4C—C5C—C6C—S7C	-178.9 (12)
C2A—C1A—C6A—C5A	0(2)	C1C—C6C—S7C—C8C	67.0 (12)
C15A—C1A—C6A—C5A	179.7 (14)	C5C—C6C—S7C—C8C	-113.8 (12)
C2A—C1A—C6A—S7A	177.5 (11)	C6C—S7C—C8C—C13C	-67.5 (15)
C15A—C1A—C6A—S7A	-3 (2)	C6C—S7C—C8C—C9C	115.2 (14)
C4A—C5A—C6A—C1A	0 (2)	C13C—C8C—C9C—C10C	-3 (3)
C4A—C5A—C6A—S7A	-178.0 (12)	S7C—C8C—C9C—C10C	174.8 (14)
C1A—C6A—S7A—C8A	65.1 (14)	C8C—C9C—C10C—C11C	3 (3)
C5A—C6A—S7A—C8A	-117.4 (13)	C9C—C10C—C11C—C12C	-3 (3)
C6A—S7A—C8A—C9A	119.9 (12)	C10C—C11C—C12C—C13C	2 (3)
C6A—S7A—C8A—C13A	-66.5 (13)	C11C—C12C—C13C—C8C	-1 (2)
C13A—C8A—C9A—C10A	1 (2)	C11C—C12C—C13C—C14C	177.8 (15)
S7A-C8A-C9A-C10A	175.0 (11)	C9C—C8C—C13C—C12C	1 (2)
C8A—C9A—C10A—C11A	-3 (2)	S7C-C8C-C13C-C12C	-175.8 (13)
C9A—C10A—C11A—C12A	4 (2)	C9C—C8C—C13C—C14C	-177.3 (15)
C10A—C11A—C12A—C13A	-3 (2)	S7C-C8C-C13C-C14C	5 (2)
C9A—C8A—C13A—C12A	-1 (2)	C12C—C13C—C14C—C15C	-138.0 (16)
S7A—C8A—C13A—C12A	-174.2 (11)	C8C—C13C—C14C—C15C	41 (2)
C9A—C8A—C13A—C14A	177.7 (13)	C12C—C13C—C14C—N16C	37 (2)
S7A-C8A-C13A-C14A	4.3 (19)	C8C—C13C—C14C—N16C	-144.7 (14)
C11A—C12A—C13A—C8A	2 (2)	N16C—C14C—C15C—C1C	-171.6 (14)
C11A—C12A—C13A—C14A	-176.9 (13)	C13C—C14C—C15C—C1C	3 (3)
C8A—C13A—C14A—N16A	-141.8 (14)	N16C—C14C—C15C—Se1C	1.8 (16)
C12A—C13A—C14A—N16A	36.7 (19)	C13C—C14C—C15C—Se1C	176.4 (12)
C8A—C13A—C14A—C15A	42 (2)	C2C—C1C—C15C—C14C	132.5 (17)
C12A—C13A—C14A—C15A	-139.5 (15)	C6C—C1C—C15C—C14C	-45 (2)
N16A—C14A—C15A—C1A	-174.6 (14)	C2C-C1C-C15C-Se1C	-40.2 (18)
C13A—C14A—C15A—C1A	2 (2)	C6C—C1C—C15C—Se1C	142.6 (12)

N16A—C14A—C15A—Se1A	-0.6 (16)	N17C—Se1C—C15C—C14C	-1.4 (11)
C13A—C14A—C15A—Se1A	175.5 (11)	N17C—Se1C—C15C—C1C	172.5 (12)
C2A—C1A—C15A—C14A	135.4 (16)	C15C—C14C—N16C—N17C	-1 (2)
C6A—C1A—C15A—C14A	-44 (2)	C13C—C14C—N16C—N17C	-176.5 (13)
C2A—C1A—C15A—Se1A	-37.8 (19)	C14C—N16C—N17C—Se1C	0.1 (16)
C6A—C1A—C15A—Se1A	142.5 (12)	C15C—Se1C—N17C—N16C	0.8 (11)
N17A—Se1A—C15A—C14A	0.6 (10)	C6D—C1D—C2D—C3D	1 (2)
N17A—Se1A—C15A—C1A	175.3 (12)	C15D—C1D—C2D—C3D	177.6 (15)
C15A—C14A—N16A—N17A	0(2)	C1D-C2D-C3D-C4D	0(3)
C13A—C14A—N16A—N17A	-176.3(13)	C2D-C3D-C4D-C5D	0(3)
C14A - N16A - N17A - Se1A	0.4(17)	C_{3D} C_{4D} C_{5D} C_{6D}	0(3)
C15A— $Se1A$ — $N17A$ — $N16A$	-0.6(11)	C4D - C5D - C6D - C1D	1(2)
C6B-C1B-C2B-C3B	1 (2)	C4D - C5D - C6D - S7D	1766(13)
C15B - C1B - C2B - C3B	-1788(15)	C^2D C^1D C^6D C^5D	-1(2)
C1B - C2B - C3B - C4B	-2(3)	$C_{15} - C_{10} - C_{60} - C_{50}$	-1780(13)
C^{2B} C^{3B} C^{4B} C^{5B}	$\frac{1}{3}$	$C^2D - C^1D - C^6D - S^7D$	-176.8(11)
C_{3B} C_{4B} C_{5B} C_{6B}	2(2)	$C_{15} - C_{10} - C_{60} - S_{70}$	6(2)
C4B-C5B-C6B-C1B	$\frac{2}{-3}(2)$	C5D - C6D - S7D - C8D	1153(13)
C4B = C5B = C6B = S7B	$\frac{3(2)}{1732(12)}$	C1D - C6D - S7D - C8D	-69.0(13)
C^{2B} C^{1B} C^{6B} C^{5B}	1/3.2(12)	C6D = S7D = C8D = C13D	64 6 (14)
C15B-C1B-C6B-C5B	-1790(14)	C6D = S7D = C8D = C9D	-1125(14)
C^{2B} C^{1B} C^{6B} S^{7B}	-1743(11)	C13D - C8D - C9D - C10D	4 (3)
C15B-C1B-C6B-S7B	5(2)	S7D - C8D - C9D - C10D	-1792(14)
C5B-C6B-S7B-C8B	$\frac{1184(12)}{1184(12)}$	C8D - C9D - C10D - C11D	-3(3)
C1B - C6B - S7B - C8B	-65.9(14)	C9D - C10D - C11D - C12D	2(3)
C6B = S7B = C8B = C13B	63.7(13)	C10D - C11D - C12D - C13D	$\frac{2}{-2}$ (3)
C6B = S7B = C8B = C9B	-1198(12)	C9D - C8D - C13D - C12D	-4(2)
C13B - C8B - C9B - C10B	1 (2)	S7D - C8D - C13D - C12D	178.9(12)
S7B-C8B-C9B-C10B	-1750(11)	C9D - C8D - C13D - C14D	178.3(12)
C8B - C9B - C10B - C11B	-2(2)	S7D - C8D - C13D - C14D	1 (2)
C9B-C10B-C11B-C12B	2(2)	C11D - C12D - C13D - C8D	3(2)
C10B $C11B$ $C12B$ $C13B$	$\frac{2}{-1}(2)$	C11D - C12D - C13D - C14D	-1790(16)
C9B-C8B-C13B-C12B	0(2)	C8D - C13D - C14D - C15D	-47(2)
S7B-C8B-C13B-C12B	1761(10)	$C_{12}D_{-}C_{13}D_{-}C_{14}D_{-}C_{15}D_{$	1351(17)
C9B - C8B - C13B - C14B	-1782(13)	C8D - C13D - C14D - N16D	144(3)
S7B-C8B-C13B-C14B	-1.9(18)	C12D $C13D$ $C14D$ $N16D$	-33(3)
C11B - C12B - C13B - C8B	0(2)	C8D— $C13D$ — $C14D$ — $Se1F$	1362(15)
C11B - C12B - C13B - C14B	177.9(13)	C12D $C13D$ $C14D$ Self	-41(2)
C8B-C13B-C14B-N16B	1413(13)	N17F—Se1F—C14D—C15D	-1.0(19)
C12B $C13B$ $C14B$ $N16B$	-367(18)	N17E—Se1E—C14D—C13D	1760(19)
C8B-C13B-C14B-C15B	-44(2)	C13D - C14D - C15D - N16F	-174(2)
C12B— $C13B$ — $C14B$ — $C15B$	1385(16)	SelE—C14D—C15D—N16E	3(3)
N16B— $C14B$ — $C15B$ — $C1B$	175 8 (14)	N16D - C14D - C15D - C1D	170(3)
C13B— $C14B$ — $C15B$ — $C1B$	1 (3)	C13D - C14D - C15D - C1D	1(3)
N16B—C14B—C15B—Se1B	-1.0 (16)	Se1E—C14D—C15D—C1D	178.0 (13)
C13B— $C14B$ — $C15B$ — $Se1B$	-176.1(11)	N16D—C14D—C15D—Se1D	-5 (3)
C2B— $C1B$ — $C15B$ — $C14B$	-139.9 (16)	C13D— $C14D$ — $C15D$ — $Se1D$	-174.3 (13)
C6B—C1B—C15B—C14B	40 (2)	C2D—C1D—C15D—C14D	-135.1 (17)
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