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# $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$

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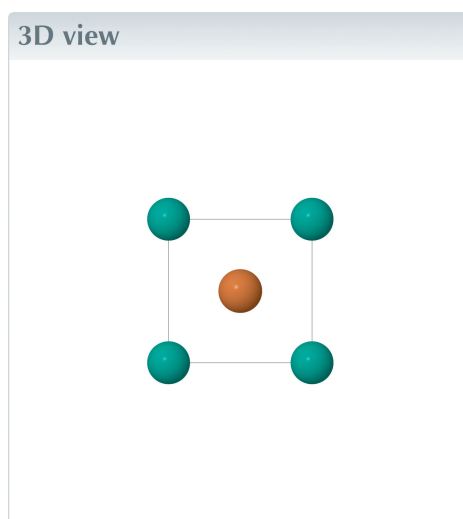
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**Keywords:** crystal structure; high-temperature sintering;  $\beta$  phase; Al–Cu–Fe system.

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**Structural data:** full structural data are available from [iucrdata.iucr.org](http://iucrdata.iucr.org)

The intermetallic phase with composition  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$  was synthesized by high-temperature sintering of a mixture with initial chemical composition  $\text{Al}_{78}\text{Cu}_{48}\text{Fe}_{13}$ .  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$  adopts the CsCl structure type in space-group  $Pm\bar{3}m$ . The structure analysis revealed that one site is co-occupied by Al and Cu with a ratio of 0.88 (5):0.12 (5) and the other is co-occupied by Fe and Cu with a ratio of 0.2 (4):0.8 (4). The Al/Cu ··· Fe/Cu separation is 2.5465 (13) Å.



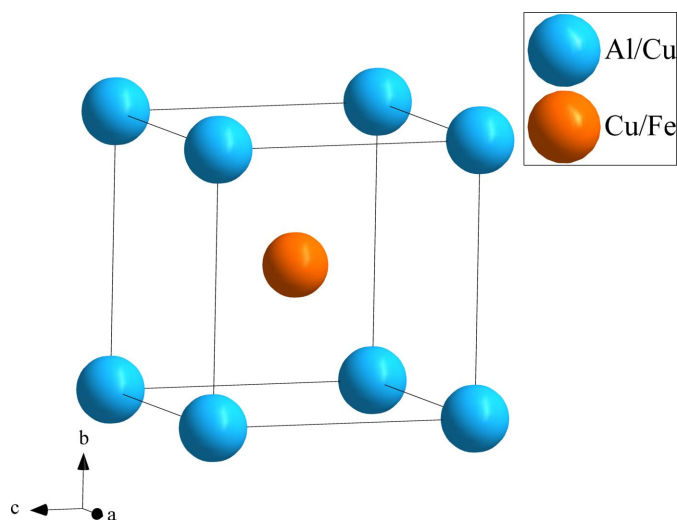
## Structure description

Phases in the ternary Al–Cu–Fe alloy system often have complex crystal structures as well as quasicrystals (QC). For example, an aperiodic diffraction pattern was observed for the alloy with composition  $\text{Al}_{63}\text{Cu}_{24}\text{Fe}_{13}$ , exhibiting tenfold rotation symmetry and characterized as a quasi-crystalline phase, as revealed by the first natural quasicrystal (Bindi *et al.*, 2011). The present phase  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$  belongs to the  $\beta$ -phase in the Al–Cu–Fe system, which is similar to that of the B2–FeAl phase (Rosas & Perez, 1998). Meyer *et al.* (2007) suggested that the  $\beta$ -phase has a b.c.c. crystal structure, and the lattice parameter of  $\beta\text{-Al}_{50}\text{Cu}_{20}\text{Fe}_{30}$  was  $a = 2.925$  Å as determined by X-ray diffraction. Kalmykov *et al.* (2009) studied the Al–Cu–Fe phase diagram at 853 K, and considered that the lattice parameter of the  $\beta\text{-AlCuFe}$  phase increased with the increase of Cu content. The lowest copper content of the  $\beta$ -phase is 7.3 at.% corresponding to a lattice parameter of  $a = 2.9171$  Å, while the  $\beta$ -phase with the highest copper content of 45.5 at.% has  $a = 2.9390$  Å. Shalaeva & Prekul (2011) studied two kinds of  $\beta$ -phases with nominal composition of  $\text{Al}_{50}\text{Cu}_{33}\text{Fe}_{17}$ , namely the  $\beta_1$ - and  $\beta_2$ -phases. The lattice parameters of the two phases were found to be 2.939 and 2.969 Å, respectively, by X-ray diffraction, and the average compositions of the two phases were  $\text{Al}_{51.5}\text{Fe}_{19}\text{Cu}_{29.5}$  and  $\text{Al}_{48.5}\text{Fe}_{13}\text{Cu}_{38.5}$ , respectively, by the electron-probe method. It should be noted that only the lattice parameters of the  $\beta$ -phase have been given in the aforementioned studies while an exact crystal structural model has not been provided. According to the Springer Materials database, there are several crystal-structure models for the  $\beta$ -phase in previous studies;



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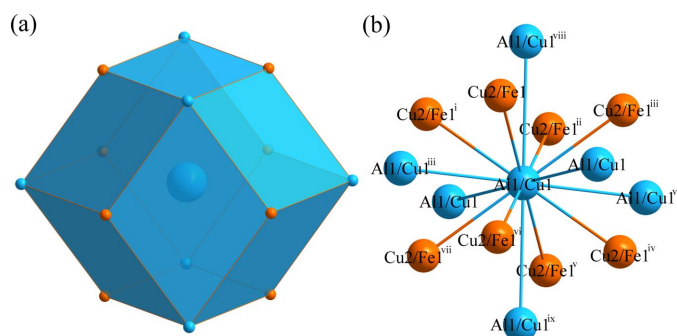


**Figure 1**  
The crystal structure of  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$ .

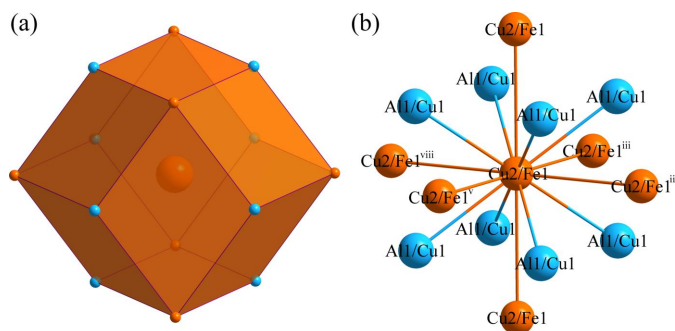
however, such a given structure model only represents a possibility inferred from the composition rather than a refined one.

In the present study, the crystal structure model for the  $\beta$ -phase in the Al–Cu–Fe system has been refined on basis of single-crystal X-ray diffraction data. This phase has similar lattice parameters to the previously reported  $\beta$ -phase. Its chemical composition was refined to be  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$ , in accordance with the complementary EDX results (see Table S1 of the supporting information).

Fig. 1 shows the distribution of the atoms in the unit cell of  $\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$ . The environments of the Al1/Cu1 and Cu2/Fe1 sites are shown in Figs. 2 and 3, respectively. The Al1/Cu1 atom at (0, 0, 0) is centered at a dodecahedron, which is surrounded by six Al1/Cu1 atoms and eight Cu2/Fe1 atoms; conversely, the Cu2/Fe1 site at (1/2, 1/2, 1/2) is surrounded by eight Al1/Cu1 atoms and six Cu2/Fe1 atoms. The shortest Al1/Cu1 to Cu2/Fe1 separation is 2.5465 (13) Å and the shortest Al1/Cu1 to Al1/Cu1 contact is 2.9405 (15) Å.



**Figure 2**  
(a) The dodecahedron formed around the Al1/Cu1 atom at the 1a site; (b) the environment of the Al1/Cu1 atom with displacement ellipsoids given at the 99% probability level. [Symmetry codes: (i)  $x - 1, y - 1, z - 1$ ; (ii)  $x - 1, y, z$ ; (iii)  $x, y - 1, z$ ; (iv)  $x - 1, y - 1, z$ ; (v)  $x, y, z - 1$ ; (vi)  $x - 1, y, z - 1$ ; (vii)  $x, y - 1, z - 1$ ; (viii)  $x, y, z + 1$ ; (ix)  $x, y + 1, z$ .]



**Figure 3**  
(a) The dodecahedron formed around the Cu2/Fe1 atom at the 1b site; (b) the environment of the Cu2/Fe1 atom with displacement ellipsoids given at the 99% probability level. [Symmetry codes: (ii)  $x - 1, y, z$ ; (iii)  $x, y - 1, z$ ; (v)  $x, y, z - 1$ ; (viii)  $x, y, z + 1$ .]

### Synthesis and crystallization

The high-purity elements Al (indicated purity 99.95%; 0.7163 g), Cu (indicated purity 99.99%; 1.0372 g) and Fe (indicated purity 99.9%; 0.2485 g) were mixed in the molar ratio 78:48:13 and ground in an agate mortar. The blended powders were placed into a cemented carbide grinding mound of 9.6 mm diameter and pressed at 4 MPa for about 3 min. The obtained cylindrical block was put into a silica glass tube and vacuum-sealed by a home-made sealing machine. The resulting ampoule then was placed in a furnace (SG-XQL1200) and heated up to 1373 K for 2 h with a heating rate of 10 K  $\text{min}^{-1}$ . The temperature was then reduced to 1073 K for 10 h. Finally, the sample was slowly cooled to room

**Table 1**  
Experimental details.

Crystal data	
Chemical formula	$\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$
$M_r$	93.42
Crystal system, space group	Cubic, $Pm\bar{3}m$
Temperature (K)	299
$a$ (Å)	2.9405 (15)
$V$ (Å <sup>3</sup> )	25.43 (4)
$Z$	1
Radiation type	Mo $K\alpha$
$\mu$ (mm <sup>-1</sup> )	22.36
Crystal size (mm)	0.14 × 0.12 × 0.12
Data collection	
Diffractometer	Bruker D8 Venture Photon 100 CMOS
Absorption correction	Multi-scan (SADABS; Krause et al., 2015)
$T_{\min}, T_{\max}$	0.439, 0.746
No. of measured, independent and observed [ $I > 2\sigma(I)$ ] reflections	385, 14, 14
$R_{\text{int}}$	0.021
$(\sin \theta/\lambda)_{\text{max}}$ (Å <sup>-1</sup> )	0.636
Refinement	
$R[F^2 > 2\sigma(F^2)], wR(F^2), S$	0.013, 0.031, 1.44
No. of reflections	14
No. of parameters	5
$\Delta\rho_{\text{max}}, \Delta\rho_{\text{min}}$ (e Å <sup>-3</sup> )	0.32, -0.48

Computer programs: APEX3 and SAINT (Bruker, 2015), SHELXT2014/5 (Sheldrick, 2015a), SHELXL2017/1 (Sheldrick, 2015b), DIAMOND (Brandenburg & Putz, 2017) and publCIF (Westrip, 2010).

temperature by turning off the furnace power. Suitable pieces of single-crystal grains were broken and selected from the product for single-crystal X-ray diffraction.

### Refinement

Crystal data, data collection and structure refinement details are summarized in Table 1. All atoms in the unit cell occupied the Wyckoff positions. Different choices of refinement are listed in Table S2 of the supporting information. The maximum and minimum residual electron densities in the final difference map are located 0.0 Å and 1.01 Å from the atoms Cu1.

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Lab for Optimizing Metal Product Technology and Performance (No. 22567609H).

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## full crystallographic data

*IUCrData* (2023). **8**, x230870 [https://doi.org/10.1107/S2414314623008702]



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## Aluminium copper iron

*Crystal data*

$\text{Al}_{0.88}\text{Cu}_{0.94}\text{Fe}_{0.18}$

$M_r = 93.42$

Cubic,  $Pm\bar{3}m$

$a = 2.9405$  (15) Å

$V = 25.43$  (4) Å<sup>3</sup>

$Z = 1$

$F(000) = 43$

$D_x = 6.101$  Mg m<sup>-3</sup>

Mo  $K\alpha$  radiation,  $\lambda = 0.71073$  Å

Cell parameters from 367 reflections

$\theta = 6.9$ – $26.9^\circ$

$\mu = 22.36$  mm<sup>-1</sup>

$T = 299$  K

Lump, drak gray

$0.14 \times 0.12 \times 0.12$  mm

*Data collection*

Bruker D8 Venture Photon 100 CMOS  
diffractometer

phi and  $\omega$  scans

Absorption correction: multi-scan  
(SADABS; Krause et al., 2015)

$T_{\min} = 0.439$ ,  $T_{\max} = 0.746$

385 measured reflections

14 independent reflections

14 reflections with  $I > 2\sigma(I)$

$R_{\text{int}} = 0.021$

$\theta_{\max} = 26.9^\circ$ ,  $\theta_{\min} = 6.9^\circ$

$h = -3 \rightarrow 3$

$k = -3 \rightarrow 3$

$l = -3 \rightarrow 3$

*Refinement*

Refinement on  $F^2$

Least-squares matrix: full

$R[F^2 > 2\sigma(F^2)] = 0.013$

$wR(F^2) = 0.031$

$S = 1.44$

14 reflections

5 parameters

0 restraints

Primary atom site location: isomorphous  
structure methods

$w = 1/[\sigma^2(F_o^2) + (0.0246P)^2]$

where  $P = (F_o^2 + 2F_c^2)/3$

$(\Delta/\sigma)_{\max} < 0.001$

$\Delta\rho_{\max} = 0.32$  e Å<sup>-3</sup>

$\Delta\rho_{\min} = -0.48$  e Å<sup>-3</sup>

*Special details*

**Geometry.** All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

*Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (Å<sup>2</sup>)*

	<i>x</i>	<i>y</i>	<i>z</i>	$U_{\text{iso}}^*/U_{\text{eq}}$	Occ. (<1)
Al1	0.000000	0.000000	0.000000	0.0113 (13)	0.88 (5)
Cu1	0.000000	0.000000	0.000000	0.0113 (13)	0.12 (5)

Fe1	0.500000	0.500000	0.500000	0.0105 (6)	0.2 (4)
Cu2	0.500000	0.500000	0.500000	0.0105 (6)	0.8 (4)

*Atomic displacement parameters (Å<sup>2</sup>)*

	$U^{11}$	$U^{22}$	$U^{33}$	$U^{12}$	$U^{13}$	$U^{23}$
All	0.0113 (13)	0.0113 (13)	0.0113 (13)	0.000	0.000	0.000
Cu1	0.0113 (13)	0.0113 (13)	0.0113 (13)	0.000	0.000	0.000
Fe1	0.0105 (6)	0.0105 (6)	0.0105 (6)	0.000	0.000	0.000
Cu2	0.0105 (6)	0.0105 (6)	0.0105 (6)	0.000	0.000	0.000

*Geometric parameters (Å, °)*

All—Fe1 <sup>i</sup>	2.5465 (13)	All—All <sup>v</sup>	2.9405 (15)
All—Fe1	2.5465 (13)	All—All <sup>viii</sup>	2.9405 (15)
All—Fe1 <sup>ii</sup>	2.5465 (13)	All—All <sup>ix</sup>	2.9405 (15)
All—Fe1 <sup>iii</sup>	2.5465 (13)	Cu1—Cu2	2.5465 (13)
All—Fe1 <sup>iv</sup>	2.5465 (13)	Fe1—Fe1 <sup>viii</sup>	2.9405 (15)
All—Fe1 <sup>v</sup>	2.5465 (13)	Fe1—Fe1 <sup>v</sup>	2.9405 (15)
All—Fe1 <sup>vi</sup>	2.5465 (13)	Fe1—Fe1 <sup>iii</sup>	2.9405 (15)
All—Fe1 <sup>vii</sup>	2.5465 (13)	Fe1—Fe1 <sup>ii</sup>	2.9405 (15)
All—All <sup>iii</sup>	2.9405 (15)		
Fe1 <sup>i</sup> —All—Fe1	180.0	All <sup>x</sup> —Fe1—All	180.0
Fe1 <sup>i</sup> —All—Fe1 <sup>ii</sup>	109.5	All <sup>x</sup> —Fe1—All <sup>xi</sup>	109.5
Fe1—All—Fe1 <sup>ii</sup>	70.529 (1)	All—Fe1—All <sup>xi</sup>	70.529 (1)
Fe1 <sup>i</sup> —All—Fe1 <sup>iii</sup>	109.5	All <sup>x</sup> —Fe1—All <sup>ix</sup>	109.5
Fe1—All—Fe1 <sup>iii</sup>	70.5	All—Fe1—All <sup>ix</sup>	70.5
Fe1 <sup>ii</sup> —All—Fe1 <sup>iii</sup>	109.5	All <sup>xi</sup> —Fe1—All <sup>ix</sup>	109.5
Fe1 <sup>i</sup> —All—Fe1 <sup>iv</sup>	70.529 (1)	All <sup>x</sup> —Fe1—All <sup>xii</sup>	70.529 (1)
Fe1—All—Fe1 <sup>iv</sup>	109.5	All—Fe1—All <sup>xii</sup>	109.5
Fe1 <sup>ii</sup> —All—Fe1 <sup>iv</sup>	70.5	All <sup>xi</sup> —Fe1—All <sup>xii</sup>	70.5
Fe1 <sup>iii</sup> —All—Fe1 <sup>iv</sup>	70.5	All <sup>ix</sup> —Fe1—All <sup>xii</sup>	70.5
Fe1 <sup>i</sup> —All—Fe1 <sup>v</sup>	109.5	All <sup>x</sup> —Fe1—All <sup>viii</sup>	109.5
Fe1—All—Fe1 <sup>v</sup>	70.529 (1)	All—Fe1—All <sup>viii</sup>	70.529 (1)
Fe1 <sup>ii</sup> —All—Fe1 <sup>v</sup>	109.5	All <sup>xi</sup> —Fe1—All <sup>viii</sup>	109.5
Fe1 <sup>iii</sup> —All—Fe1 <sup>v</sup>	109.5	All <sup>ix</sup> —Fe1—All <sup>viii</sup>	109.5
Fe1 <sup>iv</sup> —All—Fe1 <sup>v</sup>	180.0	All <sup>xii</sup> —Fe1—All <sup>viii</sup>	180.0
Fe1 <sup>i</sup> —All—Fe1 <sup>vi</sup>	70.5	All <sup>x</sup> —Fe1—All <sup>xiii</sup>	70.5
Fe1—All—Fe1 <sup>vi</sup>	109.5	All—Fe1—All <sup>xiii</sup>	109.5
Fe1 <sup>ii</sup> —All—Fe1 <sup>vi</sup>	70.5	All <sup>xi</sup> —Fe1—All <sup>xiii</sup>	70.5
Fe1 <sup>iii</sup> —All—Fe1 <sup>vi</sup>	180.0	All <sup>ix</sup> —Fe1—All <sup>xiii</sup>	180.0
Fe1 <sup>iv</sup> —All—Fe1 <sup>vi</sup>	109.5	All <sup>xii</sup> —Fe1—All <sup>xiii</sup>	109.5
Fe1 <sup>v</sup> —All—Fe1 <sup>vi</sup>	70.5	All <sup>viii</sup> —Fe1—All <sup>xiii</sup>	70.5
Fe1 <sup>i</sup> —All—Fe1 <sup>vii</sup>	70.529 (1)	All <sup>x</sup> —Fe1—All <sup>xiv</sup>	70.529 (1)
Fe1—All—Fe1 <sup>vii</sup>	109.5	All—Fe1—All <sup>xiv</sup>	109.5
Fe1 <sup>ii</sup> —All—Fe1 <sup>vii</sup>	180.0	All <sup>xi</sup> —Fe1—All <sup>xiv</sup>	180.0
Fe1 <sup>iii</sup> —All—Fe1 <sup>vii</sup>	70.5	All <sup>ix</sup> —Fe1—All <sup>xiv</sup>	70.5

Fe1 <sup>iv</sup> —Al1—Fe1 <sup>vii</sup>	109.5	Al1 <sup>xii</sup> —Fe1—Al1 <sup>xiv</sup>	109.5
Fe1 <sup>v</sup> —Al1—Fe1 <sup>vii</sup>	70.5	Al1 <sup>viii</sup> —Fe1—Al1 <sup>xiv</sup>	70.5
Fe1 <sup>vi</sup> —Al1—Fe1 <sup>vii</sup>	109.5	Al1 <sup>xiii</sup> —Fe1—Al1 <sup>xiv</sup>	109.5
Fe1 <sup>i</sup> —Al1—Al1 <sup>iii</sup>	54.7	Al1 <sup>x</sup> —Fe1—Fe1 <sup>viii</sup>	54.7
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Fe1 <sup>ii</sup> —Al1—Al1 <sup>iii</sup>	125.3	Al1 <sup>xi</sup> —Fe1—Fe1 <sup>viii</sup>	125.3
Fe1 <sup>iii</sup> —Al1—Al1 <sup>iii</sup>	54.7	Al1 <sup>ix</sup> —Fe1—Fe1 <sup>viii</sup>	125.3
Fe1 <sup>iv</sup> —Al1—Al1 <sup>iii</sup>	54.7	Al1 <sup>xii</sup> —Fe1—Fe1 <sup>viii</sup>	125.3
Fe1 <sup>v</sup> —Al1—Al1 <sup>iii</sup>	125.3	Al1 <sup>viii</sup> —Fe1—Fe1 <sup>viii</sup>	54.7
Fe1 <sup>vi</sup> —Al1—Al1 <sup>iii</sup>	125.3	Al1 <sup>xiii</sup> —Fe1—Fe1 <sup>viii</sup>	54.7
Fe1 <sup>vii</sup> —Al1—Al1 <sup>iii</sup>	54.7	Al1 <sup>xiv</sup> —Fe1—Fe1 <sup>viii</sup>	54.7
Fe1 <sup>i</sup> —Al1—Al1 <sup>v</sup>	54.7	Al1 <sup>x</sup> —Fe1—Fe1 <sup>v</sup>	125.3
Fe1—Al1—Al1 <sup>v</sup>	125.3	Al1—Fe1—Fe1 <sup>v</sup>	54.7
Fe1 <sup>ii</sup> —Al1—Al1 <sup>v</sup>	125.3	Al1 <sup>xi</sup> —Fe1—Fe1 <sup>v</sup>	54.7
Fe1 <sup>iii</sup> —Al1—Al1 <sup>v</sup>	125.3	Al1 <sup>ix</sup> —Fe1—Fe1 <sup>v</sup>	54.7
Fe1 <sup>iv</sup> —Al1—Al1 <sup>v</sup>	125.3	Al1 <sup>xii</sup> —Fe1—Fe1 <sup>v</sup>	54.7
Fe1 <sup>v</sup> —Al1—Al1 <sup>v</sup>	54.7	Al1 <sup>viii</sup> —Fe1—Fe1 <sup>v</sup>	125.3
Fe1 <sup>vi</sup> —Al1—Al1 <sup>v</sup>	54.7	Al1 <sup>xiii</sup> —Fe1—Fe1 <sup>v</sup>	125.3
Fe1 <sup>vii</sup> —Al1—Al1 <sup>v</sup>	54.7	Al1 <sup>xiv</sup> —Fe1—Fe1 <sup>v</sup>	125.3
Al1 <sup>iii</sup> —Al1—Al1 <sup>v</sup>	90.0	Fe1 <sup>viii</sup> —Fe1—Fe1 <sup>v</sup>	180.0
Fe1 <sup>i</sup> —Al1—Al1 <sup>viii</sup>	125.3	Al1 <sup>x</sup> —Fe1—Fe1 <sup>iii</sup>	125.3
Fe1—Al1—Al1 <sup>viii</sup>	54.7	Al1—Fe1—Fe1 <sup>iii</sup>	54.7
Fe1 <sup>ii</sup> —Al1—Al1 <sup>viii</sup>	54.7	Al1 <sup>xi</sup> —Fe1—Fe1 <sup>iii</sup>	54.7
Fe1 <sup>iii</sup> —Al1—Al1 <sup>viii</sup>	54.7	Al1 <sup>ix</sup> —Fe1—Fe1 <sup>iii</sup>	125.3
Fe1 <sup>iv</sup> —Al1—Al1 <sup>viii</sup>	54.7	Al1 <sup>xii</sup> —Fe1—Fe1 <sup>iii</sup>	125.3
Fe1 <sup>v</sup> —Al1—Al1 <sup>viii</sup>	125.3	Al1 <sup>viii</sup> —Fe1—Fe1 <sup>iii</sup>	54.7
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Al1 <sup>iii</sup> —Al1—Al1 <sup>viii</sup>	90.0	Fe1 <sup>viii</sup> —Fe1—Fe1 <sup>iii</sup>	90.0
Al1 <sup>v</sup> —Al1—Al1 <sup>viii</sup>	180.0	Fe1 <sup>v</sup> —Fe1—Fe1 <sup>iii</sup>	90.0
Fe1 <sup>i</sup> —Al1—Al1 <sup>ix</sup>	125.3	Al1 <sup>x</sup> —Fe1—Fe1 <sup>ii</sup>	125.3
Fe1—Al1—Al1 <sup>ix</sup>	54.7	Al1—Fe1—Fe1 <sup>ii</sup>	54.7
Fe1 <sup>ii</sup> —Al1—Al1 <sup>ix</sup>	54.7	Al1 <sup>xi</sup> —Fe1—Fe1 <sup>ii</sup>	125.3
Fe1 <sup>iii</sup> —Al1—Al1 <sup>ix</sup>	125.3	Al1 <sup>ix</sup> —Fe1—Fe1 <sup>ii</sup>	54.7
Fe1 <sup>iv</sup> —Al1—Al1 <sup>ix</sup>	125.3	Al1 <sup>xii</sup> —Fe1—Fe1 <sup>ii</sup>	125.3
Fe1 <sup>v</sup> —Al1—Al1 <sup>ix</sup>	54.7	Al1 <sup>viii</sup> —Fe1—Fe1 <sup>ii</sup>	54.7
Fe1 <sup>vi</sup> —Al1—Al1 <sup>ix</sup>	54.7	Al1 <sup>xiii</sup> —Fe1—Fe1 <sup>ii</sup>	125.3
Fe1 <sup>vii</sup> —Al1—Al1 <sup>ix</sup>	125.3	Al1 <sup>xiv</sup> —Fe1—Fe1 <sup>ii</sup>	54.7
Al1 <sup>iii</sup> —Al1—Al1 <sup>ix</sup>	180.0	Fe1 <sup>viii</sup> —Fe1—Fe1 <sup>ii</sup>	90.0
Al1 <sup>v</sup> —Al1—Al1 <sup>ix</sup>	90.0	Fe1 <sup>v</sup> —Fe1—Fe1 <sup>ii</sup>	90.0
Al1 <sup>viii</sup> —Al1—Al1 <sup>ix</sup>	90.0	Fe1 <sup>iii</sup> —Fe1—Fe1 <sup>ii</sup>	90.0

Symmetry codes: (i)  $x-1, y-1, z-1$ ; (ii)  $x-1, y, z$ ; (iii)  $x, y-1, z$ ; (iv)  $x-1, y-1, z$ ; (v)  $x, y, z-1$ ; (vi)  $x-1, y, z-1$ ; (vii)  $x, y-1, z-1$ ; (viii)  $x, y, z+1$ ; (ix)  $x, y+1, z$ ; (x)  $x+1, y+1, z+1$ ; (xi)  $x+1, y, z$ ; (xii)  $x+1, y+1, z$ ; (xiii)  $x+1, y, z+1$ ; (xiv)  $x, y+1, z+1$ .