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Tetramethyl 1,1,2-triphenyl-2*H*-1 λ^5 -phosphole-2,3,4,5-tetracarboxylate

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Key indicators: single-crystal X-ray study; T = 293 K; mean σ (C–C) = 0.003 Å; R factor = 0.041; wR factor = 0.128; data-to-parameter ratio = 14.8.

The title compound, $C_{30}H_{27}O_8P$ (1), was formed as one of two products {(1) and (2) [Krawczyk *et al.* (2010). *Acta Cryst.* E66 (cv2753)]} in the reaction of dimethyl acetylenedicarboxylate with triphenylphosphine. The molecule of (1) consists of a five-membered ring, in which the P atom is incorporated. One of the phenyl groups of the triphenylphosphine migrated to a vicinal C atom during the reaction. The five-membered ring of (1) is corrugated [r.m.s. deviation = 0.0719 (8) Å], whereas that in compound (2) is planar, the r.m.s. deviation being only 0.009 (2) Å.

Related literature

For general background to derivatives of dimethylenesuccinic anhydride (fulgides), see: Hadjoudis & Mavridis (2004); Gordaliza *et al.* (1996); Datta *et al.* (2001); Stobbe (1893); Maercker (1965); Shaw *et al.* (1967). For a detailed study of adduct formation from triarylphosphines and acetylenedicarboxylate, see: Waite *et al.* (1971). For related structures, see: Spek (1987); Thomas & Hamor (1993); Krawczyk *et al.* (2010).



Experimental

Crystal data

 C_3

MTr a:

bc:

α β

| $_{0}H_{27}O_{8}P$ | $\gamma = 69.24 \ (4)^{\circ}$ |
|-------------------------|---|
| r = 546.49 | $V = 1373.0 (10) \text{ Å}^3$ |
| iclinic, P1 | Z = 2 |
| = 10.445 (6) Å | Cu $K\alpha$ radiation |
| = 10.897 (4) Å | $\mu = 1.32 \text{ mm}^{-1}$ |
| = 13.778 (4) Å | T = 293 K |
| = 73.93 (3)° | $0.20 \times 0.12 \times 0.04 \text{ mm}$ |
| $= 72.54 \ (4)^{\circ}$ | |

Data collection

| Oxford Diffraction Xealibur |
|--|
| diffractometer with Ruby CCD |
| Absorption correction: analytical |
| (CrysAlis RED; Oxford |
| Diffraction, 2006) |
| $T_{\rm min} = 0.714, T_{\rm max} = 0.885$ |

Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.041$ $wR(F^2) = 0.128$ S = 1.105207 reflections 4503 reflections with $I > 2\sigma(I)$ $R_{\rm int} = 0.032$

20877 measured reflections 5207 independent reflections

352 parameters H-atom parameters not refined
$$\begin{split} &\Delta\rho_{max}=0.33 \text{ e } \text{\AA}^{-3} \\ &\Delta\rho_{min}=-0.24 \text{ e } \text{\AA}^{-3} \end{split}$$

Data collection: *CrysAlis CCD* (Oxford Diffraction, 2006); cell refinement: *CrysAlis RED* (Oxford Diffraction, 2006); data reduction: *CrysAlis RED*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *SHELXTL-NT* (Sheldrick, 2008); software used to prepare material for publication: *SHELXL97*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: CV2752).

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Tetramethyl 1,1,2-triphenyl-2*H*-1λ⁵-phosphole-2,3,4,5-tetracarboxylate

Krzysztof K. Krawczyk, Krystyna Wojtasiewicz, Jan K. Maurin, Ewa Gronowska and Zbigniew Czarnocki

S1. Comment

Several derivatives of dimethylenesuccinic anhydride (fulgides) have been the subject of intensive studies due to their photochromic properties (Hadjoudis & Mavridis, 2004). As early as in 1893 Stobbe (Stobbe, 1893) discovered a very effective synthetic procedure leading to E,E-diarylfulgides. The double Stobbe condensation, after some minor modifications (Gordaliza et al., 1996) still remains the method of choice in the construction of fulgide-type compounds (Datta et al., 2001). However, considering some disadvantages of this procedure, e.g. a need for the use of strong bases, which may cause resinification of some aldehydes, there have been continuous efforts towards development of alternative approaches. Especially the Wittig reaction (Maercker, 1965) between dialkyl bis[triphenylphosphoranylidene]succinates and the appropriate benzaldehydes appeared to be of particular value. The vlide component of the Wittig reaction seemed to be easily accessible by the condensation between triphenylphosphine and dialkyl acetylenedicarboxylate. However, this reaction, performed in diethyl ether, gave tetramethyl 1,1,2-triphenyl- $2H-1\lambda^{5}$ -phosphole-2,3,4,5-tetracarboxylate (1) and another adduct - trimethyl-3-methoxy-4-oxo-5-triphenylphosphoranylidenecyclopent-1-ene- 1,2,3-tricarboxylate in 42% and 21% yield respectively (Shaw et al., 1967). We found, that when dry toluene was used as a solvent, and the reaction was performed at -78°C, (1) was formed in 63% yield, and the other adduct in 28% yield. In the present comunication we report on the crystal structure of compound (1). This structure was already proposed in 1971 (Waite et al., 1971) on the basis of spectral data. The crystal structure of the other adduct could also be determined via singlecrystal diffraction (Krawczyk et al., 2010).

In compound (1) (Fig. 1) two acetyl groups at C2 and C4, respectively, are almost co-planar with the five-membered ring with the dihedral angle of 11.6 (1) and 8.47 (9)°, respectively, whereas the two remaining acetyl groups at C1 and C3 are strongly rotated from the ring plane (the dihedral angles of 67.(1) and 80.51 (8)°, respectively). The phenyl rings bonded to the phosphorous atoms in (1) have similar conformations to that observed at room temperature for the parent triphenylphosphine in both polymorphic structures (Spek, 1987; Thomas & Hamor, 1993) assuring the lowest repulsion of the neighboring fragments.

S2. Experimental

A mixture of acetylenedicarboxylate (0.5 g, 3,52 mmol) in 3 ml of dry toluene was placed in a two-neck round bottom flask, and cooled to -78°C (solid CO₂/acetone bath) with stirring. The solution of triphenylphosphine (0.47 g, 1.80 mmol) in 3 ml of dry toluene was then added dropwise under argon during 20 min. The reaction was then left to reach slowly room temperature overnight. After evaporation of the solvent under reduced pressure, the remaining oil was dissolved in ethyl acetate and purified by column chromatography (Merck silica gel, 230 - 400 mesh, ethyl acetate, and then ethyl acetate/methanol 19:1 as eluent) to obtain tetramethyl-1,1,2- triphenyl-2*H*-1 λ^5 -phosphole-2,3,4,5-tetracarboxylate (1) and trimethyl-3-methoxy-4-oxo-5-triphenylphosphoranylidenecyclopent-1- ene-1,2,3-tricarboxylate (2). Both products could

be easily recrystallized from ethyl acetate/diethyl ether. The 2*H*-phosphole (1) (0.61 g, 63%) had Rf = 0.46 (ethyl acetate) and a melting point of 253–255°C (Waite, *et al.*1971). The second eluted product - (2) (0.27 g, 28%) - showed a green fluorescence in UV light (λ = 365 nm), had Rf = 0.18 (ethyl acetate) and melted at 243–244°C [(Waite *et al.*, 1971), m.p. 222–224°C]. The single-crystal of (1) was obtained by slow evaporation of its ethyl acetate/hexane solution.

S3. Refinement

H atoms were placed in calculated positions and were included in the refinement with $U_{iso}(H) = 1.2U_{eq}(C)$ [1.5 in the case of methyl groups H atoms]. Isotropic displacement parameters for hydrogen atoms bonded to either oxygen or nitrogen atoms were refined independently.



Figure 1

Molecular structure of (1) showing the atomic labelling and 30% probability displacement ellipsoids.

Tetramethyl 1,1,2-triphenyl-2*H*-1λ⁵-phosphole-2,3,4,5-tetracarboxylate

| $C_{30}H_{27}O_8P$ | $\gamma = 69.24 \ (4)^{\circ}$ |
|--------------------------------|---|
| $M_r = 546.49$ | $V = 1373.0 (10) \text{ Å}^3$ |
| Triclinic, $P\overline{1}$ | Z = 2 |
| a = 10.445 (6) Å | F(000) = 572 |
| b = 10.897 (4) Å | $D_{\rm x} = 1.322 {\rm Mg} {\rm m}^{-3}$ |
| c = 13.778 (4) Å | Melting point: 527 K |
| $\alpha = 73.93 \ (3)^{\circ}$ | Cu <i>K</i> α radiation, $\lambda = 1.54184$ Å |
| $\beta = 72.54 \ (4)^{\circ}$ | Cell parameters from 13436 reflections |
| | |

 $\theta = 3.4-70.3^{\circ}$ $\mu = 1.32 \text{ mm}^{-1}$ T = 293 K

Data collection

| Oxford Diffraction Xcalibur |
|--|
| diffractometer with Ruby CCD |
| Radiation source: Enhance (Cu) X-ray Source |
| Graphite monochromator |
| Detector resolution: 10.4922 pixels mm ⁻¹ |
| $o \text{ and } \varphi \text{ scans}$ |
| Absorption correction: analytical |
| (CrysAlis RED; Oxford Diffraction, 2006) |
| $T_{\min} = 0.714, \ T_{\max} = 0.885$ |

Refinement

| Refinement on F^2 | Secondary atom site location: difference Fourier |
|---|--|
| Least-squares matrix: full | map |
| $R[F^2 > 2\sigma(F^2)] = 0.041$ | Hydrogen site location: inferred from |
| $wR(F^2) = 0.128$ | neighbouring sites |
| <i>S</i> = 1.10 | H-atom parameters not refined |
| 5207 reflections | $w = 1/[\sigma^2(F_o^2) + (0.0892P)^2 + 0.105P]$ |
| 352 parameters | where $P = (F_o^2 + 2F_c^2)/3$ |
| 0 restraints | $(\Delta/\sigma)_{\rm max} = 0.001$ |
| Primary atom site location: structure-invariant | $\Delta \rho_{\rm max} = 0.33 \text{ e} \text{ Å}^{-3}$ |
| direct methods | $\Delta \rho_{\rm min} = -0.24 \text{ e} \text{ Å}^{-3}$ |

Special details

Experimental. Analytical numeric absorption correction using a multifaceted crystal model based on expressions derived by R.C. Clark & J.S. Reid. (Clark, R. C. & Reid, J. S. (1995). Acta Cryst. A51, 887–897)

Parallelepiped, colourless

20877 measured reflections 5207 independent reflections 4503 reflections with $I > 2\sigma(I)$

 $\theta_{\rm max} = 70.9^\circ, \ \theta_{\rm min} = 3.4^\circ$

 $0.20 \times 0.12 \times 0.04 \text{ mm}$

 $R_{\rm int} = 0.032$

 $h = -12 \rightarrow 12$ $k = -13 \rightarrow 13$ $l = -16 \rightarrow 16$

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

| | x | У | Ζ | $U_{ m iso}$ */ $U_{ m eq}$ | |
|----|--------------|--------------|--------------|-----------------------------|--|
| P1 | 0.87807 (4) | 0.28700 (3) | 0.28773 (3) | 0.03454 (13) | |
| 01 | 0.74905 (14) | 0.07868 (13) | 0.47544 (10) | 0.0626 (4) | |
| O2 | 0.56979 (14) | 0.26500 (16) | 0.47158 (9) | 0.0707 (4) | |
| 03 | 0.38795 (12) | 0.44323 (14) | 0.23622 (10) | 0.0600 (3) | |
| O4 | 0.45565 (13) | 0.23001 (13) | 0.31754 (11) | 0.0608 (3) | |
| 05 | 0.52801 (15) | 0.67511 (12) | 0.19216 (10) | 0.0620 (4) | |
| 06 | 0.58094 (12) | 0.56597 (11) | 0.06301 (8) | 0.0463 (3) | |
| 07 | 0.85225 (13) | 0.62633 (11) | 0.08444 (10) | 0.0549 (3) | |
| 08 | 1.01365 (12) | 0.49540 (11) | 0.17693 (9) | 0.0489 (3) | |
| C1 | 0.72232 (15) | 0.22390 (14) | 0.31095 (11) | 0.0364 (3) | |
| C2 | 0.61807 (15) | 0.34781 (15) | 0.26462 (11) | 0.0383 (3) | |
| | | | | | |

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | | | | | |
|---|------|--------------|---------------|--------------|-------------|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C3 | 0.67344 (15) | 0.44912 (14) | 0.20778 (11) | 0.0368 (3) |
| C5 $0.68130(17)$ $0.17803(17)$ $0.42808(12)$ $0.0458(4)$ C6 $0.5292(3)$ $0.2358(4)$ $0.58405(17)$ $0.1184(12)$ H6A 0.4466 0.3048 0.6076 $0.178*$ H6B 0.6044 0.2319 0.6123 $0.078*$ C7 $0.47704(16)$ $0.34920(17)$ $0.26968(12)$ $0.0829(7)$ C8 $0.3211(2)$ $0.2186(3)$ $0.3245(2)$ $0.0829(7)$ H8B 0.3063 0.2346 $0.26968(12)$ $0.0439(4)$ C8 $0.3215(2)$ 0.0129 $0.0329(2)$ $0.0329(2)$ C9 $0.58512(16)$ $0.57734(15)$ $0.15500(12)$ $0.0413(3)$ C10 $0.4878(2)$ $0.6777(2)$ $0.00915(16)$ $0.0599(16)$ H10A 0.4925 $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C11 $0.89050(16)$ $0.52834(14)$ 0.1442 $0.099*$ H10C 0.3394 0.6614 0.0500 $0.099*$ H10C | C4 | 0.81626 (15) | 0.43265 (14) | 0.20266 (11) | 0.0381 (3) |
| C6 0.5292 (3) 0.2358 (4) 0.58405 (17) 0.1184 (13) H6A 0.4466 0.3048 0.6076 0.178^* H6B 0.6044 0.2319 0.6123 0.178^* H6C 0.5097 0.1513 0.60655 0.178^* C7 0.47704 (16) 0.34920 (17) 0.26968 (12) 0.0439 (4) C8 0.3211 (2) 0.2186 (3) 0.3245 (2) 0.0829 (7) H8A 0.3063 0.2346 0.25600 0.124^* H8B 0.3063 0.2346 0.2560 0.124^* C9 0.58512 (16) 0.57734 (15) 0.15500 (12) 0.0413 (3) C10 0.4878 (2) 0.6777 (2) 0.00915 (16) 0.05500 0.099^* H10A 0.4926 0.6597 -0.0564 0.099^* H10C 0.35155 0.7566 -0.0021 0.0994 H10C 0.39950 (16) 0.52134 (14) 0.14421 0.0957^* H12A | C5 | 0.68130 (17) | 0.17803 (17) | 0.42808 (12) | 0.0458 (4) |
| H6A 0.4466 0.3048 0.6076 0.178^{*} H6B 0.6044 0.2319 0.6123 0.178^{*} H6C 0.5097 0.1513 0.6065 0.178^{*} H6C $0.47704(16)$ $0.34920(17)$ $0.26968(12)$ $0.0439(4)$ C7 $0.47704(16)$ $0.34920(17)$ $0.26968(12)$ $0.0439(4)$ C8 $0.3211(2)$ $0.2186(3)$ $0.3245(2)$ $0.0829(7)$ H8A 0.3171 0.1304 0.3599 0.124^{*} H8B 0.3063 0.2346 0.2560 0.124^{*} C9 $0.5812(16)$ $0.7774(15)$ $0.15500(12)$ $0.0413(3)$ C10 $0.4878(2)$ $0.6777(2)$ $0.00915(16)$ $0.059(5)$ H10A 0.4926 0.6597 -0.0564 0.999^{*} H10C 0.3934 0.6914 0.5000 0.099^{*} C11 $0.8905(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ $0.5725(2)$ $0.11739(17)$ $0.0631(5)$ H12A 1.1909 0.5410 0.1442 0.095^{*} H12B 1.0622 0.6650 0.1219 0.095^{*} H12C 1.1326 0.5632 0.0463 0.095^{*} H12C 1.1326 0.5632 0.0463 0.095^{*} C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.1227(2)$ $0.0758(6)$ H12C 1.1326 0.6532 $0.1227(2)$ $0.$ | C6 | 0.5292 (3) | 0.2358 (4) | 0.58405 (17) | 0.1184 (13) |
| H6B 0.6044 0.2319 0.6123 0.178^* H6C 0.5097 0.1513 0.6065 0.178^* C7 $0.47704 (16)$ $0.34920 (17)$ $0.26968 (12)$ $0.0829 (7)$ U8 $0.3211 (2)$ $0.2186 (3)$ $0.3245 (2)$ $0.0829 (7)$ H8A 0.3171 0.1304 0.3599 0.124^* H8B 0.3063 0.2346 0.2560 0.124^* C9 $0.58512 (16)$ $0.57734 (15)$ $0.15500 (12)$ $0.0413 (3)$ C10 $0.4878 (2)$ $0.6777 (2)$ $0.00915 (16)$ $0.0695 (5)$ H10A 0.4926 0.6597 -0.0564 0.999^* H10C 0.3934 0.6914 0.0500 0.099^* H10C 0.3934 0.6914 $0.14811 (11)$ $0.0393 (3)$ C12 $1.1076 (2)$ $0.5725 (2)$ $0.11739 (17)$ $0.631 (5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* H12A 0.7991 0.2313 0.1112 $0.066 (5)$ H14 0.7991 0.2313 0.1112 $0.0666 (5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1961 0.2441 0.095^* C17 $0.7855 (3)$ $-0.1097 (2)$ $0.3330 (16)$ $0.2964 (19)$ <tr< td=""><td>H6A</td><td>0.4466</td><td>0.3048</td><td>0.6076</td><td>0.178*</td></tr<> | H6A | 0.4466 | 0.3048 | 0.6076 | 0.178* |
| H6C 0.5097 0.1513 0.6065 0.178^* C7 $0.47704 (16)$ $0.34920 (17)$ $0.2696 (12)$ $0.0439 (4)$ C8 $0.3211 (2)$ $0.2186 (3)$ $0.3245 (2)$ $0.0829 (7)$ H8A 0.3171 0.1304 0.3599 0.124^* H8B 0.3063 0.2346 0.2560 0.124^* H8C 0.2495 0.2833 0.3621 $0.0413 (3)$ C10 $0.4878 (2)$ $0.6777 (2)$ $0.00915 (16)$ $0.0659 (5)$ H10A 0.4926 0.6597 -0.0564 0.099^* H10B 0.5155 0.7566 -0.0021 0.099^* H10C 0.3934 0.6914 0.5000 0.099^* C11 $0.80950 (16)$ $0.52834 (14)$ $0.14811 (11)$ $0.0398 (3)$ C12 $1.1076 (2)$ $0.5725 (2)$ $0.11739 (17)$ $0.0631 (5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12A 1.1092 0.5323 0.0463 0.095^* C13 $0.76060 (16)$ $0.11180 (15)$ $0.24985 (12)$ $0.0417 (3)$ C14 $0.7902 (19)$ $0.4481 (18)$ $0.1428 (14)$ $0.0520 (4)$ H14 0.7991 0.2313 0.1112 $0.666 (5)$ H15 $0.8210 (3)$ $-0.0751 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1961 0.2641 0.095^* C16 $0.8210 (3)$ $-0.0751 (2)$ $0.1277 (2)$ | H6B | 0.6044 | 0.2319 | 0.6123 | 0.178* |
| C7 $0.47704 (16)$ $0.34920 (17)$ $0.26968 (12)$ $0.0439 (4)$ C8 $0.3211 (2)$ $0.1306 (3)$ $0.3245 (2)$ $0.0829 (7)$ H8A 0.3171 0.1304 0.3599 $0.124*$ H8B 0.3063 0.2346 0.2560 $0.124*$ H8C 0.2495 0.2833 0.3621 $0.124*$ C9 $0.85812 (16)$ $0.77734 (15)$ $0.15500 (12)$ $0.0413 (3)$ C10 $0.4878 (2)$ $0.6777 (2)$ $0.00915 (16)$ $0.0659 (5)$ H10A 0.4926 0.6597 -0.0564 $0.099*$ H10B 0.5155 0.7566 -0.0021 $0.099*$ C11 $0.89050 (16)$ $0.52834 (14)$ $0.14811 (11)$ $0.0398 (3)$ C12 $1.1076 (2)$ $0.5725 (2)$ $0.11739 (17)$ $0.0631 (5)$ H12A 1.1909 0.5410 0.1442 $0.095*$ H12B 1.0622 0.6650 0.1219 $0.0497 (3)$ C14 $0.79602 (19)$ $0.14481 (18)$ $0.14288 (14)$ $0.0520 (4)$ H14 $0.79602 (19)$ $0.14481 (18)$ $0.4288 (14)$ $0.0520 (4)$ H15 0.8517 $0.0751 (2)$ $0.1277 (2)$ $0.0758 (2)$ C15 $0.8269 (2)$ $-0.0515 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1961 0.2641 $0.095*$ C13 $0.7554 (2)$ $-0.10671 (18)$ $0.2990 (17)$ $0.0674 (5)$ H15 $0.8210 (3)$ $-0.0751 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0 | H6C | 0.5097 | 0.1513 | 0.6065 | 0.178* |
| C8 $0.3211(2)$ $0.2186(3)$ $0.3245(2)$ $0.0829(7)$ H8A 0.3171 0.1304 0.3599 $0.124*$ H8B 0.3063 0.2346 0.2560 $0.124*$ H8C 0.2495 0.2833 0.3621 $0.124*$ C9 $0.58512(16)$ $0.57734(15)$ $0.15500(12)$ $0.0413(3)$ C10 $0.4878(2)$ $0.6777(2)$ $0.00915(16)$ $0.0659(5)$ H10A 0.4926 0.6597 -0.0564 $0.099*$ H10C 0.3934 0.6914 0.0500 $0.099*$ C11 $0.89050(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ 0.57566 -0.0021 $0.099*$ H12A 1.1999 0.5410 $0.14481(48)$ 0.0550 H12B 1.0622 0.6650 0.1219 $0.095*$ H12C 1.1326 0.5632 0.0443 $0.095*$ H12B 1.0622 0.6650 0.1219 $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.14288(14)$ $0.0520(4)$ H14 0.7991 0.2313 0.1112 $0.062*$ C15 $0.8269(2)$ $0.515(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 $0.091*$ C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.3630 $0.062*$ C15 $0.8269(2)$ $-0.0674(18)$ $0.2996(17)$ $0.0617(5)$ H17 0.7814 < | C7 | 0.47704 (16) | 0.34920 (17) | 0.26968 (12) | 0.0439 (4) |
| H8A 0.3171 0.1304 0.3599 0.124^* H8B 0.3063 0.2346 0.2560 0.124^* H8C 0.2495 0.2833 0.3621 0.124^* C9 $0.58512(16)$ $0.57734(15)$ $0.15500(12)$ $0.0413(3)$ C10 $0.4878(2)$ $0.6777(2)$ $0.00915(16)$ $0.0659(5)$ H10A 0.4926 0.6597 -0.0564 0.099^* H10B 0.5155 0.7566 -0.0021 0.099^* C11 $0.89050(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ $0.5725(2)$ $0.11739(17)$ $0.0631(5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 0.79901 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.08212(17)$ $0.0666(5)$ H15 0.8517 0.0751 0.0103 0.080^* C17 $0.755(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.9961 0.2641 0.095^* C18 $0.7554(2)$ $-0.06733(18)$ $0.29509(17)$ $0.0617(5)$ H17 0.7814 -0.9961 $0.29863(14)$ 0.064^* C19 <td>C8</td> <td>0.3211 (2)</td> <td>0.2186 (3)</td> <td>0.3245 (2)</td> <td>0.0829 (7)</td> | C8 | 0.3211 (2) | 0.2186 (3) | 0.3245 (2) | 0.0829 (7) |
| H8B 0.3063 0.2346 0.2560 0.124^* H8C 0.2495 0.2833 0.3621 0.124^* C9 $0.58512(16)$ $0.57734(15)$ $0.15500(12)$ $0.0413(3)$ C10 $0.4878(2)$ $0.6777(2)$ $0.00915(16)$ $0.0569(5)$ H10A 0.4926 0.6597 -0.0564 0.099^* H10B 0.5155 0.7566 -0.0021 0.099^* C11 $0.89050(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ $0.5725(2)$ $0.11739(17)$ $0.0631(5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.0463 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.14288(14)$ $0.0520(4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.8212(17)$ $0.0666(5)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.96161 $0.25969(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(5)$ H21 1.2241 $-0.0453(18)$ $0.25964($ | H8A | 0.3171 | 0.1304 | 0.3599 | 0.124* |
| H8C 0.2495 0.2833 0.3621 0.124^* C9 $0.58512 (16)$ $0.57734 (15)$ $0.15500 (12)$ $0.0413 (3)$ C10 $0.4878 (2)$ $0.6777 (2)$ $0.00915 (16)$ $0.0659 (3)$ H10A 0.4926 0.6597 -0.0564 0.099^* H10E 0.5155 0.7566 -0.0021 0.099^* H10C 0.3934 0.6914 0.0500 0.099^* C11 $0.89050 (16)$ $0.52834 (14)$ $0.14811 (11)$ $0.0398 (3)$ C12 $1.1076 (2)$ $0.5725 (2)$ $0.11739 (17)$ $0.0631 (5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060 (16)$ $0.11180 (15)$ $0.24985 (12)$ $0.0417 (3)$ C14 0.79901 0.2313 0.1112 0.062^* C15 $0.8269 (2)$ $0.0515 (2)$ $0.8212 (17)$ $0.0666 (5)$ H15 0.8517 0.0751 0.0103 0.808^* C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24922 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ | H8B | 0.3063 | 0.2346 | 0.2560 | 0.124* |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | H8C | 0.2495 | 0.2833 | 0.3621 | 0.124* |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C9 | 0.58512 (16) | 0.57734 (15) | 0.15500 (12) | 0.0413 (3) |
| H10A 0.4926 0.6597 -0.0564 0.099^* H10B 0.5155 0.7566 -0.0021 0.099^* H10C 0.3934 0.6914 0.0500 0.099^* C11 $0.89050(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ $0.5725(2)$ $0.11739(17)$ $0.0631(5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 0.79901 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.8212(17)$ $0.0666(5)$ H15 0.8517 0.0751 0.0103 0.80^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C19 $1.03797(15)$ $0.16713(15)$ $0.24922(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.182(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0651(5)$ H18 0.7319 $-0.0205(2)$ $0.16489(19)$ $0.0516(5)$ < | C10 | 0.4878 (2) | 0.6777 (2) | 0.00915 (16) | 0.0659 (5) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | H10A | 0.4926 | 0.6597 | -0.0564 | 0.099* |
| H10C 0.3934 0.6914 0.0500 0.099^* C11 $0.89050(16)$ $0.52834(14)$ $0.14811(11)$ $0.0398(3)$ C12 $1.1076(2)$ $0.5725(2)$ $0.11739(17)$ $0.0631(5)$ H12A 1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.14288(14)$ $0.0520(4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.08212(17)$ $0.0666(5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H17 0.7844 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C20 $1.0797(15)$ $0.16713(15)$ $0.24022(12)$ $0.088(3)$ C21 $1.1982(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0651(5)$ H21 1.2241 -0.1830 0.1401 0.081^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248(19)$ $0.1049(2)$ $0.1654(15)$ <td< td=""><td>H10B</td><td>0.5155</td><td>0.7566</td><td>-0.0021</td><td>0.099*</td></td<> | H10B | 0.5155 | 0.7566 | -0.0021 | 0.099* |
| C11 $0.89050 (16)$ $0.52834 (14)$ $0.14811 (11)$ $0.0398 (3)$ C12 $1.1076 (2)$ $0.5725 (2)$ $0.11739 (17)$ $0.0631 (5)$ H12A 1.1909 0.5410 0.1442 $0.095*$ H12B 1.0622 0.6650 0.1219 $0.095*$ H12C 1.1326 0.5632 0.0463 $0.095*$ C13 $0.76060 (16)$ $0.11180 (15)$ $0.24985 (12)$ $0.0417 (3)$ C14 $0.79602 (19)$ $0.14481 (18)$ $0.14288 (14)$ $0.0520 (4)$ H14 0.7991 0.2313 0.1112 $0.062*$ C15 $0.8269 (2)$ $0.0515 (2)$ $0.08212 (17)$ $0.0666 (5)$ H15 0.8517 0.0751 0.1033 $0.080*$ C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H17 0.7814 -0.1961 0.2641 $0.095*$ C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 $0.074*$ C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 $0.062*$ C21 $1.1982 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H21 1.2241 -0.180 0.1401 $0.081*$ C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.062*$ C23 $1.24248 (19)$ | H10C | 0.3934 | 0.6914 | 0.0500 | 0.099* |
| C121.1076 (2)0.5725 (2)0.11739 (17)0.0631 (5)H12A1.19090.54100.14420.095*H12B1.06220.66500.12190.095*H12C1.13260.56320.04630.095*C130.76060 (16)0.11180 (15)0.24985 (12)0.0417 (3)C140.79602 (19)0.14481 (18)0.14288 (14)0.0520 (4)H140.79910.23130.11120.0666 (5)C150.8269 (2)0.0515 (2)0.08212 (17)0.0666 (5)H150.85170.07510.01030.80*C160.8210 (3)-0.0755 (2)0.1277 (2)0.0758 (6)H160.8411-0.13820.08700.091*C170.7855 (3)-0.1097 (2)0.2332 (2)0.0795 (7)H170.7814-0.19610.26410.095*C180.7554 (2)-0.01671 (18)0.29509 (17)0.0617 (5)H180.7319-0.04130.36690.074*C201.07591 (19)0.03839 (16)0.29863 (14)0.0514 (4)H201.01970.01520.36300.062*C211.1982 (2)-0.0205 (2)0.16489 (19)0.0674 (5)H211.2241-0.14040.29810.078*C221.2813 (2)-0.0205 (2)0.16489 (19)0.0674 (5)H211.2424 (19)0.12680.04180.070*C231.24248 (19)0.12680.04180.070*C241.11999 (17) <t< td=""><td>C11</td><td>0.89050 (16)</td><td>0.52834 (14)</td><td>0.14811 (11)</td><td>0.0398 (3)</td></t<> | C11 | 0.89050 (16) | 0.52834 (14) | 0.14811 (11) | 0.0398 (3) |
| H12A1.1909 0.5410 0.1442 0.095^* H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.14288(14)$ $0.0520(4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.08212(17)$ $0.0666(5)$ H16 0.8517 0.0751 0.0103 0.080^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ 0.0152 0.3630 0.662^* C21 $1.1982(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H21 $1.2248(19)$ 0.1268 0.0418 0.070^* C23 $1.24248(19)$ 0.1268 $0.0451(4)$ $0.298(6)(15)$ | C12 | 1.1076 (2) | 0.5725 (2) | 0.11739 (17) | 0.0631 (5) |
| H12B 1.0622 0.6650 0.1219 0.095^* H12C 1.1326 0.5632 0.0463 0.095^* C13 $0.76060 (16)$ $0.11180 (15)$ $0.24985 (12)$ $0.0417 (3)$ C14 $0.79602 (19)$ $0.14481 (18)$ $0.14288 (14)$ $0.0520 (4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269 (2)$ $0.0515 (2)$ $0.08212 (17)$ $0.0666 (5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.758 (6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855 (3)$ $-0.1097 (2)$ $0.2332 (2)$ $0.0795 (7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H23 1.2928 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ | H12A | 1.1909 | 0.5410 | 0.1442 | 0.095* |
| H12C1.13260.56320.04630.095*C130.76060 (16)0.11180 (15)0.24985 (12)0.0417 (3)C140.79602 (19)0.14481 (18)0.14288 (14)0.0520 (4)H140.79910.23130.11120.062*C150.8269 (2)0.0515 (2)0.08212 (17)0.0666 (5)H150.85170.07510.01030.080*C160.8210 (3) $-0.0755 (2)$ 0.1277 (2)0.0758 (6)H160.8411 -0.1382 0.08700.091*C170.7855 (3) $-0.1097 (2)$ 0.2332 (2)0.0795 (7)H170.7814 -0.1961 0.26410.095*C180.7554 (2) $-0.01671 (18)$ 0.29069 (17)0.0617 (5)H180.7319 -0.0413 0.36690.074*C191.03797 (15)0.16713 (15)0.24022 (12)0.0386 (3)C201.07591 (19)0.03839 (16)0.29863 (14)0.0514 (4)H201.01970.01520.36300.062*C211.1982 (2) $-0.0205 (2)$ 0.16489 (19)0.0674 (5)H211.2241 -0.1404 0.29810.078*C221.2813 (2) $-0.0205 (2)$ 0.16489 (19)0.0654 (5)H231.29880.12680.04180.070*C241.11999 (17)0.19945 (16)0.14305 (12)0.0452 (4)H241.09310.28400.10260.054*C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3 | H12B | 1.0622 | 0.6650 | 0.1219 | 0.095* |
| C13 $0.76060(16)$ $0.11180(15)$ $0.24985(12)$ $0.0417(3)$ C14 $0.79602(19)$ $0.14481(18)$ $0.14288(14)$ $0.0520(4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.08212(17)$ $0.0666(5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.662^* C21 $1.1982(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2428(19)$ $0.1049(2)$ $0.1654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459(16)$ $0.32367(15)$ 0.4 | H12C | 1.1326 | 0.5632 | 0.0463 | 0.095* |
| C14 $0.79602 (19)$ $0.14481 (18)$ $0.14288 (14)$ $0.0520 (4)$ H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269 (2)$ $0.0515 (2)$ $0.08212 (17)$ $0.0666 (5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855 (3)$ $-0.1097 (2)$ $0.2332 (2)$ $0.0795 (7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.24248 (19)$ $0.1049 (2)$ $0.1654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.$ | C13 | 0.76060 (16) | 0.11180 (15) | 0.24985 (12) | 0.0417 (3) |
| H14 0.7991 0.2313 0.1112 0.062^* C15 $0.8269(2)$ $0.0515(2)$ $0.08212(17)$ $0.0666(5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0651(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999(17)$ $0.1945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459(16)$ $0.32367(15)$ $0.406578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 0.059^* | C14 | 0.79602 (19) | 0.14481 (18) | 0.14288 (14) | 0.0520 (4) |
| C15 $0.8269 (2)$ $0.0515 (2)$ $0.08212 (17)$ $0.0666 (5)$ H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855 (3)$ $-0.1097 (2)$ $0.2332 (2)$ $0.0795 (7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0514 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 0 | H14 | 0.7991 | 0.2313 | 0.1112 | 0.062* |
| H15 0.8517 0.0751 0.0103 0.080^* C16 $0.8210(3)$ $-0.0755(2)$ $0.1277(2)$ $0.0758(6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982(2)$ $-0.05435(18)$ $0.25964(19)$ $0.0514(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459(16)$ $0.32367(15)$ $0.40546(12)$ $0.0422(3)$ C26 $0.97926(18)$ $0.2854(2)$ $0.5545(15)$ $0.0661(4)$ H26 1.0461 0.1693 0.44679 </td <td>C15</td> <td>0.8269 (2)</td> <td>0.0515 (2)</td> <td>0.08212 (17)</td> <td>0.0666 (5)</td> | C15 | 0.8269 (2) | 0.0515 (2) | 0.08212 (17) | 0.0666 (5) |
| C16 $0.8210 (3)$ $-0.0755 (2)$ $0.1277 (2)$ $0.0758 (6)$ H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855 (3)$ $-0.1097 (2)$ $0.2332 (2)$ $0.0795 (7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 0.059^* | H15 | 0.8517 | 0.0751 | 0.0103 | 0.080* |
| H16 0.8411 -0.1382 0.0870 0.091^* C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982(2)$ $-0.05435(18)$ $0.25964(19)$ $0.0651(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459(16)$ $0.32367(15)$ $0.446578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 0.059^* | C16 | 0.8210 (3) | -0.0755 (2) | 0.1277 (2) | 0.0758 (6) |
| C17 $0.7855(3)$ $-0.1097(2)$ $0.2332(2)$ $0.0795(7)$ H17 0.7814 -0.1961 0.2641 $0.095*$ C18 $0.7554(2)$ $-0.01671(18)$ $0.29509(17)$ $0.0617(5)$ H18 0.7319 -0.0413 0.3669 $0.074*$ C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 $0.062*$ C21 $1.1982(2)$ $-0.05435(18)$ $0.25964(19)$ $0.0651(5)$ H21 1.2241 -0.1404 0.2981 $0.078*$ C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 $0.070*$ C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 $0.054*$ C25 $0.88459(16)$ $0.32367(15)$ $0.40546(12)$ $0.0422(3)$ C26 $0.97926(18)$ $0.24694(18)$ $0.46578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 $0.059*$ | H16 | 0.8411 | -0.1382 | 0.0870 | 0.091* |
| H17 0.7814 -0.1961 0.2641 0.095^* C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 0.059^* | C17 | 0.7855 (3) | -0.1097 (2) | 0.2332 (2) | 0.0795 (7) |
| C18 $0.7554 (2)$ $-0.01671 (18)$ $0.29509 (17)$ $0.0617 (5)$ H18 0.7319 -0.0413 0.3669 $0.074*$ C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 $0.062*$ C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H21 1.2241 -0.1404 0.2981 $0.078*$ C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H22 1.3643 -0.0830 0.1401 $0.081*$ C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 $0.070*$ C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 $0.054*$ C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 $0.059*$ | H17 | 0.7814 | -0.1961 | 0.2641 | 0.095* |
| H18 0.7319 -0.0413 0.3669 0.074^* C19 $1.03797(15)$ $0.16713(15)$ $0.24022(12)$ $0.0386(3)$ C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982(2)$ $-0.05435(18)$ $0.25964(19)$ $0.0651(5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459(16)$ $0.32367(15)$ $0.40546(12)$ $0.0422(3)$ C26 $0.97926(18)$ $0.24694(18)$ $0.46578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 0.059^* | C18 | 0.7554 (2) | -0.01671 (18) | 0.29509 (17) | 0.0617 (5) |
| C19 $1.03797 (15)$ $0.16713 (15)$ $0.24022 (12)$ $0.0386 (3)$ C20 $1.07591 (19)$ $0.03839 (16)$ $0.29863 (14)$ $0.0514 (4)$ H20 1.0197 0.0152 0.3630 0.062^* C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H21 1.2241 -0.1404 0.2981 0.078^* C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 0.059^* | H18 | 0.7319 | -0.0413 | 0.3669 | 0.074* |
| C20 $1.07591(19)$ $0.03839(16)$ $0.29863(14)$ $0.0514(4)$ H20 1.0197 0.0152 0.3630 $0.062*$ C21 $1.1982(2)$ $-0.05435(18)$ $0.25964(19)$ $0.0651(5)$ H21 1.2241 -0.1404 0.2981 $0.078*$ C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 $0.081*$ C23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 $0.070*$ C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 $0.054*$ C25 $0.88459(16)$ $0.32367(15)$ $0.40546(12)$ $0.0422(3)$ C26 $0.97926(18)$ $0.24694(18)$ $0.46578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 $0.059*$ | C19 | 1.03797 (15) | 0.16713 (15) | 0.24022 (12) | 0.0386 (3) |
| H201.01970.01520.36300.062*C211.1982 (2) $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H211.2241 -0.1404 0.2981 $0.078*$ C221.2813 (2) $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H221.3643 -0.0830 0.1401 $0.081*$ C231.24248 (19) $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H231.2988 0.1268 0.0418 $0.070*$ C241.11999 (17) $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H241.0931 0.2840 0.1026 $0.054*$ C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 $0.059*$ | C20 | 1.07591 (19) | 0.03839 (16) | 0.29863 (14) | 0.0514 (4) |
| C21 $1.1982 (2)$ $-0.05435 (18)$ $0.25964 (19)$ $0.0651 (5)$ H21 1.2241 -0.1404 0.2981 $0.078*$ C22 $1.2813 (2)$ $-0.0205 (2)$ $0.16489 (19)$ $0.0674 (5)$ H22 1.3643 -0.0830 0.1401 $0.081*$ C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 $0.070*$ C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 $0.054*$ C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 $0.059*$ | H20 | 1.0197 | 0.0152 | 0.3630 | 0.062* |
| H21 1.2241 -0.1404 0.2981 $0.078*$ C22 1.2813 (2) -0.0205 (2) 0.16489 (19) 0.0674 (5)H22 1.3643 -0.0830 0.1401 $0.081*$ C23 1.24248 (19) 0.1049 (2) 0.10654 (15) 0.0586 (5)H23 1.2988 0.1268 0.0418 $0.070*$ C24 1.11999 (17) 0.19945 (16) 0.14305 (12) 0.0452 (4)H24 1.0931 0.2840 0.1026 $0.054*$ C25 0.88459 (16) 0.32367 (15) 0.40546 (12) 0.0422 (3)C26 0.97926 (18) 0.24694 (18) 0.46578 (13) 0.0492 (4)H26 1.0461 0.1693 0.4469 $0.059*$ C27 0.9748 (2) 0.2854 (2) 0.55454 (15) 0.0661 (5) | C21 | 1.1982 (2) | -0.05435 (18) | 0.25964 (19) | 0.0651 (5) |
| C22 $1.2813(2)$ $-0.0205(2)$ $0.16489(19)$ $0.0674(5)$ H22 1.3643 -0.0830 0.1401 $0.081*$ C23 $1.24248(19)$ $0.1049(2)$ $0.10654(15)$ $0.0586(5)$ H23 1.2988 0.1268 0.0418 $0.070*$ C24 $1.11999(17)$ $0.19945(16)$ $0.14305(12)$ $0.0452(4)$ H24 1.0931 0.2840 0.1026 $0.054*$ C25 $0.88459(16)$ $0.32367(15)$ $0.40546(12)$ $0.0422(3)$ C26 $0.97926(18)$ $0.24694(18)$ $0.46578(13)$ $0.0492(4)$ H26 1.0461 0.1693 0.4469 $0.059*$ C27 $0.9748(2)$ $0.2854(2)$ $0.55454(15)$ $0.0661(5)$ | H21 | 1.2241 | -0.1404 | 0.2981 | 0.078* |
| H22 1.3643 -0.0830 0.1401 0.081^* C23 $1.24248 (19)$ $0.1049 (2)$ $0.10654 (15)$ $0.0586 (5)$ H23 1.2988 0.1268 0.0418 0.070^* C24 $1.11999 (17)$ $0.19945 (16)$ $0.14305 (12)$ $0.0452 (4)$ H24 1.0931 0.2840 0.1026 0.054^* C25 $0.88459 (16)$ $0.32367 (15)$ $0.40546 (12)$ $0.0422 (3)$ C26 $0.97926 (18)$ $0.24694 (18)$ $0.46578 (13)$ $0.0492 (4)$ H26 1.0461 0.1693 0.4469 0.059^* C27 $0.9748 (2)$ $0.2854 (2)$ $0.55454 (15)$ $0.0661 (5)$ | C22 | 1.2813 (2) | -0.0205 (2) | 0.16489 (19) | 0.0674 (5) |
| C231.24248 (19)0.1049 (2)0.10654 (15)0.0586 (5)H231.29880.12680.04180.070*C241.11999 (17)0.19945 (16)0.14305 (12)0.0452 (4)H241.09310.28400.10260.054*C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3)C260.97926 (18)0.24694 (18)0.46578 (13)0.0492 (4)H261.04610.16930.44690.059*C270.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | H22 | 1.3643 | -0.0830 | 0.1401 | 0.081* |
| H231.29880.12680.04180.070*C241.11999 (17)0.19945 (16)0.14305 (12)0.0452 (4)H241.09310.28400.10260.054*C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3)C260.97926 (18)0.24694 (18)0.46578 (13)0.0492 (4)H261.04610.16930.44690.059*C270.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | C23 | 1.24248 (19) | 0.1049 (2) | 0.10654 (15) | 0.0586 (5) |
| C241.11999 (17)0.19945 (16)0.14305 (12)0.0452 (4)H241.09310.28400.10260.054*C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3)C260.97926 (18)0.24694 (18)0.46578 (13)0.0492 (4)H261.04610.16930.44690.059*C270.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | H23 | 1.2988 | 0.1268 | 0.0418 | 0.070* |
| H241.09310.28400.10260.054*C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3)C260.97926 (18)0.24694 (18)0.46578 (13)0.0492 (4)H261.04610.16930.44690.059*C270.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | C24 | 1.11999 (17) | 0.19945 (16) | 0.14305 (12) | 0.0452 (4) |
| C250.88459 (16)0.32367 (15)0.40546 (12)0.0422 (3)C260.97926 (18)0.24694 (18)0.46578 (13)0.0492 (4)H261.04610.16930.44690.059*C270.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | H24 | 1.0931 | 0.2840 | 0.1026 | 0.054* |
| C26 0.97926 (18) 0.24694 (18) 0.46578 (13) 0.0492 (4) H26 1.0461 0.1693 0.4469 0.059* C27 0.9748 (2) 0.2854 (2) 0.55454 (15) 0.0661 (5) | C25 | 0.88459 (16) | 0.32367 (15) | 0.40546 (12) | 0.0422 (3) |
| H261.04610.16930.44690.059* $C27$ 0.9748 (2)0.2854 (2)0.55454 (15)0.0661 (5) | C26 | 0.97926 (18) | 0.24694 (18) | 0.46578 (13) | 0.0492 (4) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | H26 | 1.0461 | 0.1693 | 0.4469 | 0.059* |
| -0.27 $0.7740(2)$ $0.2034(2)$ $0.33434(13)$ $0.0001(3)$ | C27 | 0.9748 (2) | 0.2854 (2) | 0.55454 (15) | 0.0661 (5) |

| H27 | 1.0402 | 0.2343 | 0.5944 | 0.079* |
|--------------------------|--|--|--|--|
| C28 | 0.8755 (3) | 0.3978 (3) | 0.58435 (17) | 0.0789 (6) |
| H28 | 0.8729 | 0.4227 | 0.6444 | 0.095* |
| C29 | 0.7807 (3) | 0.4726 (3) | 0.5259 (2) | 0.0965 (9) |
| H29 | 0.7122 | 0.5484 | 0.5467 | 0.116* |
| C30 | 0.7848 (3) | 0.4378 (2) | 0.43626 (18) | 0.0789 (7) |
| H30 | 0.7203 | 0.4910 | 0.3961 | 0.095* |
| C29 H29 C30 H30 | 0.7807 (3) 0.7122 0.7848 (3) 0.7203 | 0.4726 (3) 0.5484 0.4378 (2) 0.4910 | 0.5259 (2) 0.5467 0.43626 (18) 0.3961 | 0.0965 (9) 0.116* 0.0789 (7) 0.095* |

Atomic displacement parameters $(Å^2)$

| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | | U^{11} | U ²² | U^{33} | U^{12} | U^{13} | U^{23} |
|--|-----|-------------|-----------------|-------------|---------------|---------------|---------------|
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | P1 | 0.0331 (2) | 0.0310 (2) | 0.0361 (2) | -0.00411 (15) | -0.01189 (14) | -0.00373 (14) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O1 | 0.0660 (8) | 0.0580 (8) | 0.0472 (7) | -0.0097 (7) | -0.0169 (6) | 0.0087 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O2 | 0.0576 (8) | 0.0871 (10) | 0.0400 (6) | 0.0074 (7) | -0.0074 (6) | -0.0113 (6) |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | O3 | 0.0386 (6) | 0.0697 (8) | 0.0637 (8) | -0.0056 (6) | -0.0192 (5) | -0.0055 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O4 | 0.0423 (6) | 0.0612 (8) | 0.0795 (9) | -0.0201 (6) | -0.0157 (6) | -0.0060 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O5 | 0.0722 (8) | 0.0435 (6) | 0.0633 (7) | 0.0130 (6) | -0.0303 (6) | -0.0223 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O6 | 0.0543 (6) | 0.0410 (6) | 0.0410 (6) | -0.0028 (5) | -0.0215 (5) | -0.0068 (4) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | O7 | 0.0622 (7) | 0.0400 (6) | 0.0618 (7) | -0.0175 (6) | -0.0285 (6) | 0.0100 (5) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 08 | 0.0456 (6) | 0.0440 (6) | 0.0573 (7) | -0.0155 (5) | -0.0196 (5) | 0.0015 (5) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C1 | 0.0332 (7) | 0.0361 (7) | 0.0372 (7) | -0.0083 (6) | -0.0099 (5) | -0.0031 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C2 | 0.0346 (7) | 0.0391 (7) | 0.0380 (7) | -0.0039 (6) | -0.0117 (6) | -0.0077 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C3 | 0.0379 (7) | 0.0347 (7) | 0.0356 (7) | -0.0014 (6) | -0.0139 (6) | -0.0093 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C4 | 0.0395 (7) | 0.0309 (7) | 0.0404 (7) | -0.0051 (6) | -0.0144 (6) | -0.0026 (5) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C5 | 0.0428 (8) | 0.0503 (9) | 0.0406 (8) | -0.0146 (7) | -0.0097 (6) | -0.0017 (7) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C6 | 0.0901 (19) | 0.162 (3) | 0.0423 (11) | 0.0193 (19) | -0.0018 (11) | -0.0134 (15) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C7 | 0.0366 (7) | 0.0540 (9) | 0.0395 (7) | -0.0072 (7) | -0.0096 (6) | -0.0133 (7) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C8 | 0.0564 (12) | 0.0940 (17) | 0.1114 (19) | -0.0385 (12) | -0.0180 (12) | -0.0192 (15) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C9 | 0.0412 (8) | 0.0369 (7) | 0.0422 (8) | -0.0004 (6) | -0.0156 (6) | -0.0099 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C10 | 0.0837 (14) | 0.0527 (10) | 0.0630 (11) | -0.0071 (10) | -0.0465 (11) | 0.0017 (9) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C11 | 0.0455 (8) | 0.0315 (7) | 0.0417 (7) | -0.0076 (6) | -0.0149 (6) | -0.0054 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C12 | 0.0531 (10) | 0.0639 (11) | 0.0758 (13) | -0.0278 (9) | -0.0145 (9) | -0.0047 (10) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C13 | 0.0370 (7) | 0.0365 (7) | 0.0516 (8) | -0.0076 (6) | -0.0147 (6) | -0.0077 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C14 | 0.0590 (10) | 0.0472 (9) | 0.0503 (9) | -0.0108 (8) | -0.0158 (8) | -0.0129 (7) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C15 | 0.0774 (13) | 0.0631 (12) | 0.0621 (11) | -0.0089 (10) | -0.0212 (10) | -0.0260 (9) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C16 | 0.0861 (15) | 0.0580 (12) | 0.0943 (17) | -0.0055 (11) | -0.0352 (13) | -0.0363 (12) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C17 | 0.0990 (17) | 0.0417 (10) | 0.1046 (19) | -0.0212 (11) | -0.0300 (14) | -0.0160 (11) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C18 | 0.0737 (12) | 0.0437 (9) | 0.0665 (11) | -0.0186 (9) | -0.0187 (10) | -0.0042 (8) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C19 | 0.0345 (7) | 0.0354 (7) | 0.0441 (7) | -0.0036 (6) | -0.0146 (6) | -0.0075 (6) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C20 | 0.0491 (9) | 0.0397 (8) | 0.0572 (10) | -0.0055 (7) | -0.0166 (8) | -0.0014 (7) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | C21 | 0.0596 (11) | 0.0380 (9) | 0.0876 (14) | 0.0051 (8) | -0.0289 (11) | -0.0087 (9) |
| $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ | C22 | 0.0480 (10) | 0.0590 (11) | 0.0890 (15) | 0.0070 (9) | -0.0155 (10) | -0.0343 (11) |
| C24 0.0459 (8) 0.0445 (8) 0.0433 (8) -0.0083 (7) -0.0120 (7) -0.0099 (7) C25 0.0444 (8) 0.0421 (8) 0.0414 (7) -0.0109 (7) -0.0132 (6) -0.0085 (6) C26 0.0490 (9) 0.0516 (9) 0.0455 (8) -0.0133 (8) -0.0167 (7) -0.0026 (7) C27 0.0751 (13) 0.0788 (14) 0.0506 (10) -0.0234 (11) -0.0307 (9) -0.0029 (9) C28 0.1066 (18) 0.0837 (15) 0.0560 (11) -0.0224 (14) -0.0288 (12) -0.0244 (11) | C23 | 0.0475 (9) | 0.0654 (11) | 0.0585 (10) | -0.0068 (8) | -0.0037 (8) | -0.0272 (9) |
| C25 0.0444 (8) 0.0421 (8) 0.0414 (7) -0.0109 (7) -0.0132 (6) -0.0085 (6) C26 0.0490 (9) 0.0516 (9) 0.0455 (8) -0.0133 (8) -0.0167 (7) -0.0026 (7) C27 0.0751 (13) 0.0788 (14) 0.0506 (10) -0.0234 (11) -0.0307 (9) -0.0029 (9) C28 0.1066 (18) 0.0837 (15) 0.0560 (11) -0.0224 (14) -0.0288 (12) -0.0244 (11) | C24 | 0.0459 (8) | 0.0445 (8) | 0.0433 (8) | -0.0083 (7) | -0.0120 (7) | -0.0099 (7) |
| C26 0.0490 (9) 0.0516 (9) 0.0455 (8) -0.0133 (8) -0.0167 (7) -0.0026 (7) C27 0.0751 (13) 0.0788 (14) 0.0506 (10) -0.0234 (11) -0.0307 (9) -0.0029 (9) C28 0.1066 (18) 0.0837 (15) 0.0560 (11) -0.0224 (14) -0.0288 (12) -0.0244 (11) | C25 | 0.0444 (8) | 0.0421 (8) | 0.0414 (7) | -0.0109 (7) | -0.0132 (6) | -0.0085 (6) |
| C27 0.0751 (13) 0.0788 (14) 0.0506 (10) -0.0234 (11) -0.0307 (9) -0.0029 (9) C28 0.1066 (18) 0.0837 (15) 0.0560 (11) -0.0224 (14) -0.0288 (12) -0.0244 (11) | C26 | 0.0490 (9) | 0.0516 (9) | 0.0455 (8) | -0.0133 (8) | -0.0167 (7) | -0.0026 (7) |
| C28 0.1066 (18) 0.0837 (15) 0.0560 (11) -0.0224 (14) -0.0288 (12) -0.0244 (11) | C27 | 0.0751 (13) | 0.0788 (14) | 0.0506 (10) | -0.0234 (11) | -0.0307 (9) | -0.0029 (9) |
| | C28 | 0.1066 (18) | 0.0837 (15) | 0.0560 (11) | -0.0224 (14) | -0.0288 (12) | -0.0244 (11) |

| C29 | 0.116 (2) | 0.0873 (17) | 0.0825 (16) | 0.0170 (16) | -0.0434 (15) | -0.0498 (14) |
|-----|-------------|-------------|-------------|-------------|--------------|--------------|
| C30 | 0.0877 (15) | 0.0693 (13) | 0.0761 (14) | 0.0194 (12) | -0.0430 (12) | -0.0377 (11) |

Geometric parameters (Å, °)

| P1—C4 | 1.7342 (17) | C12—H12C | 0.9600 |
|------------|-------------|---------------|-------------|
| P1—C19 | 1.7872 (19) | C13—C18 | 1.379 (2) |
| P1—C25 | 1.8001 (16) | C13—C14 | 1.383 (2) |
| P1—C1 | 1.8921 (17) | C14—C15 | 1.384 (3) |
| O1—C5 | 1.201 (2) | C14—H14 | 0.9300 |
| O2—C5 | 1.314 (2) | C15—C16 | 1.367 (3) |
| O2—C6 | 1.453 (3) | C15—H15 | 0.9300 |
| O3—C7 | 1.204 (2) | C16—C17 | 1.365 (4) |
| O4—C7 | 1.347 (2) | C16—H16 | 0.9300 |
| O4—C8 | 1.426 (2) | C17—C18 | 1.395 (3) |
| O5—C9 | 1.192 (2) | C17—H17 | 0.9300 |
| O6—C9 | 1.3220 (19) | C18—H18 | 0.9300 |
| O6—C10 | 1.440 (2) | C19—C24 | 1.384 (2) |
| O7—C11 | 1.2078 (19) | C19—C20 | 1.395 (2) |
| O8—C11 | 1.357 (2) | C20—C21 | 1.384 (3) |
| O8—C12 | 1.436 (2) | С20—Н20 | 0.9300 |
| C1—C2 | 1.521 (2) | C21—C22 | 1.369 (3) |
| C1—C5 | 1.526 (2) | C21—H21 | 0.9300 |
| C1—C13 | 1.543 (2) | C22—C23 | 1.369 (3) |
| C2—C3 | 1.367 (2) | C22—H22 | 0.9300 |
| C2—C7 | 1.448 (2) | C23—C24 | 1.385 (3) |
| C3—C4 | 1.420 (2) | С23—Н23 | 0.9300 |
| С3—С9 | 1.503 (2) | C24—H24 | 0.9300 |
| C4—C11 | 1.429 (2) | C25—C26 | 1.375 (2) |
| С6—Н6А | 0.9600 | C25—C30 | 1.386 (3) |
| С6—Н6В | 0.9600 | C26—C27 | 1.382 (3) |
| С6—Н6С | 0.9600 | C26—H26 | 0.9300 |
| C8—H8A | 0.9600 | C27—C28 | 1.366 (3) |
| C8—H8B | 0.9600 | С27—Н27 | 0.9300 |
| C8—H8C | 0.9600 | C28—C29 | 1.355 (4) |
| C10—H10A | 0.9600 | C28—H28 | 0.9300 |
| C10—H10B | 0.9600 | C29—C30 | 1.374 (3) |
| C10—H10C | 0.9600 | С29—Н29 | 0.9300 |
| C12—H12A | 0.9600 | С30—Н30 | 0.9300 |
| C12—H12B | 0.9600 | | |
| C4—P1—C19 | 118.31 (8) | O8—C12—H12C | 109.5 |
| C4—P1—C25 | 111.01 (8) | H12A—C12—H12C | 109.5 |
| C19—P1—C25 | 110.45 (8) | H12B—C12—H12C | 109.5 |
| C4—P1—C1 | 95.25 (8) | C18—C13—C14 | 118.39 (16) |
| C19—P1—C1 | 110.67 (8) | C18—C13—C1 | 124.08 (16) |
| C25—P1—C1 | 110.13 (8) | C14—C13—C1 | 117.46 (14) |
| C5—O2—C6 | 116.29 (17) | C13—C14—C15 | 121.17 (18) |

| C7—O4—C8 | 116.36 (17) | C13—C14—H14 | 119.4 |
|---|--------------------------|--|-------------------|
| C9—O6—C10 | 115.99 (13) | C15—C14—H14 | 119.4 |
| C11—O8—C12 | 116.43 (14) | C16—C15—C14 | 120.0 (2) |
| C2—C1—C5 | 115.65 (13) | C16—C15—H15 | 120.0 |
| C2-C1-C13 | 109.52 (12) | C14—C15—H15 | 120.0 |
| $C_{5}-C_{1}-C_{13}$ | 113 31 (13) | C17-C16-C15 | 119 67 (19) |
| C2-C1-P1 | 101 49 (10) | C17 - C16 - H16 | 120.2 |
| $C_{2} = C_{1} = P_{1}$ | 105.46 (10) | C_{15} C_{16} H_{16} | 120.2 |
| C_{13} C_{1} P_{1} | 110.62 (10) | C16-C17-C18 | 120.2 120.8(2) |
| $C_3 C_2 C_7$ | 123.29(14) | C_{16} C_{17} H_{17} | 110.6 |
| $C_3 = C_2 = C_1$ | 125.29(14) 114.70(13) | $C_{10} = C_{17} = H_{17}$ | 110.6 |
| $C_{3} - C_{2} - C_{1}$ | 114.70(13) 121.52(14) | $C_{13} = C_{17} = 117$ | 119.0 120.0(2) |
| $C^2 = C^2 = C^4$ | 121.32(14) 118.22(14) | $C_{13} = C_{18} = C_{17}$ | 120.0 (2) |
| $C_2 = C_3 = C_4$ | 110.35(14) 121.27(14) | C13 - C18 - H18 | 120.0 |
| $C_2 = C_3 = C_9$ | 121.37(14) | C1/-C18-H18 | 120.0 |
| $C_4 - C_3 - C_9$ | 120.20 (14) | C_{24} C_{19} C_{20} C_{24} C_{10} P_{1} | 119.92 (15) |
| | 125.85 (14) | C24—C19—P1 | 120.09 (12) |
| C3—C4—P1 | 108.19 (12) | C20—C19—P1 | 119.89 (13) |
| CII—C4—PI | 125.44 (12) | C21—C20—C19 | 119.24 (18) |
| 01 | 124.05 (16) | C21—C20—H20 | 120.4 |
| O1—C5—C1 | 123.65 (15) | C19—C20—H20 | 120.4 |
| O2—C5—C1 | 112.10 (14) | C22—C21—C20 | 120.56 (18) |
| O2—C6—H6A | 109.5 | C22—C21—H21 | 119.7 |
| O2—C6—H6B | 109.5 | C20—C21—H21 | 119.7 |
| H6A—C6—H6B | 109.5 | C23—C22—C21 | 120.22 (17) |
| O2—C6—H6C | 109.5 | С23—С22—Н22 | 119.9 |
| Н6А—С6—Н6С | 109.5 | C21—C22—H22 | 119.9 |
| H6B—C6—H6C | 109.5 | C22—C23—C24 | 120.53 (18) |
| O3—C7—O4 | 122.88 (15) | С22—С23—Н23 | 119.7 |
| O3—C7—C2 | 125.66 (17) | C24—C23—H23 | 119.7 |
| O4—C7—C2 | 111.46 (14) | C23—C24—C19 | 119.47 (16) |
| O4—C8—H8A | 109.5 | C23—C24—H24 | 120.3 |
| O4—C8—H8B | 109.5 | C19—C24—H24 | 120.3 |
| H8A—C8—H8B | 109.5 | C26—C25—C30 | 118.85 (16) |
| O4—C8—H8C | 109.5 | C26—C25—P1 | 124.91 (13) |
| H8A—C8—H8C | 109.5 | C30—C25—P1 | 116.24 (13) |
| H8B—C8—H8C | 109.5 | C25—C26—C27 | 119.85 (18) |
| 05-09-06 | 125.55 (14) | C25—C26—H26 | 120.1 |
| 05-09-03 | 123 73 (14) | C27—C26—H26 | 120.1 |
| 06-09-03 | 110 72 (12) | C_{28} C_{27} C_{26} | 120.73(19) |
| 06-C10-H10A | 109 5 | C_{28} C_{27} H_{27} | 119.6 |
| O6-C10-H10B | 109.5 | $C_{26} - C_{27} - H_{27}$ | 119.6 |
| H10A - C10 - H10B | 109.5 | C29 - C28 - C27 | 119.59 (19) |
| 06-C10-H10C | 109.5 | C_{29} C_{28} H_{28} | 120.2 |
| | 109.5 | $C_{2} = C_{2} = H_{2}$ | 120.2 |
| H10R C10 $H10C$ | 109.5 | C_{2}^{-} C_{20}^{-} C_{20}^{-} C_{20}^{-} | 120.2 120.7(2) |
| $07_{11} 08$ | 109.5 | $C_{20} = C_{20} = C_{30}$ | 120.7 (2) |
| 07 - 011 - 00 | 122.07(14) 126.20(15) | $\begin{array}{cccccccccccccccccccccccccccccccccccc$ | 117.0 |
| 0^{-11} 0^{-11} 0^{-11} 0^{-11} | 120.20(13) 110.02(12) | $C_{20} = C_{27} = C_{27}$ | 117.0 |
| 00-011-04 | 110.75(13) | U27-UJU-U2J | 120.2 (2) |

| O8—C12—H12A | 109.5 | C29—C30—H30 | 119.9 |
|--|--------------------------|-------------------------------------|--------------------------|
| O8—C12—H12B | 109.5 | C25—C30—H30 | 119.9 |
| H12A—C12—H12B | 109.5 | | |
| | | | |
| C4—P1—C1—C2 | -12.94 (10) | C12—O8—C11—O7 | -8.6 (2) |
| C19—P1—C1—C2 | -135.88 (10) | C12—O8—C11—C4 | 171.39 (14) |
| C25—P1—C1—C2 | 101.72 (11) | C3—C4—C11—O7 | -13.6 (3) |
| C4—P1—C1—C5 | -133.91 (11) | P1-C4-C11-O7 | 175.67 (13) |
| C19—P1—C1—C5 | 103.16 (11) | C3—C4—C11—O8 | 166.45 (13) |
| C25—P1—C1—C5 | -19.25 (12) | P1—C4—C11—O8 | -4.29 (19) |
| C4—P1—C1—C13 | 103.22 (11) | C2-C1-C13-C18 | -129.20(17) |
| C19—P1—C1—C13 | -19.72(12) | C5-C1-C13-C18 | 1.6 (2) |
| C25—P1—C1—C13 | -142.12 (11) | P1—C1—C13—C18 | 119.74 (16) |
| $C_{5}-C_{1}-C_{2}-C_{3}$ | 124.77 (14) | C2-C1-C13-C14 | 47.76 (18) |
| $C_{13} - C_{1} - C_{2} - C_{3}$ | -105.73(14) | C5-C1-C13-C14 | 178.51 (14) |
| P1-C1-C2-C3 | 11.24 (14) | P1-C1-C13-C14 | -63.30(17) |
| $C_{5}-C_{1}-C_{2}-C_{7}$ | -63.05(18) | C18 - C13 - C14 - C15 | -0.6(3) |
| $C_{13} - C_{1} - C_{2} - C_{7}$ | 66 44 (17) | C1 - C13 - C14 - C15 | -17772(17) |
| P1 - C1 - C2 - C7 | -17659(11) | C13 - C14 - C15 - C16 | 0.8(3) |
| $C_{7}^{-}C_{2}^{-}C_{3}^{-}C_{4}^{-}$ | -175.57(13) | C_{14} C_{15} C_{16} C_{17} | -0.5(4) |
| $C_1 - C_2 - C_3 - C_4$ | -3.56(19) | $C_{14} = C_{15} = C_{10} = C_{17}$ | -0.1(4) |
| $C_1 C_2 C_3 C_4$ | 67(2) | $C_{13} = C_{10} = C_{17} = C_{18}$ | 0.1(4) |
| $C_1 = C_2 = C_3 = C_9$ | 17876(12) | C1 = C13 = C18 = C17 | 176.03(18) |
| $C_1 - C_2 - C_3 - C_9$ | -170.76(12) | C1 = C13 = C18 = C17 | 170.93(10) |
| $C_2 - C_3 - C_4 - C_{11}$ | -1/9.20(14) | $C_{10} - C_{17} - C_{18} - C_{13}$ | 0.4(4) |
| $C_{2} = C_{3} = C_{4} = C_{11}$ | -1.3(2) | C4 - F1 - C19 - C24 | 9.30 (13) |
| $C_2 = C_3 = C_4 = P_1$ | -7.20(10) | C_{23} P_{1} C_{19} C_{24} | -119.90 (13) |
| $C_{2} = C_{3} = C_{4} = P_{1}$ | 1/0.51(10) 128.76(11) | C1 = P1 = C19 = C24 | 117.88(13) |
| C19— $P1$ — $C4$ — $C3$ | 128.70 (11) | C4 - P1 - C19 - C20 | -166.72(12) |
| C_{25} P_{1} C_{4} C_{3} | -102.04(12) | C_{25} P_{1} C_{19} C_{20} | 63.82 (15) 58.40 (15) |
| CI - PI - C4 - C3 | 11.88 (11) | C1 = P1 = C19 = C20 | -58.40 (15) |
| C19—P1—C4—C11 | -59.14 (15) | $C_{24} = C_{19} = C_{20} = C_{21}$ | 2.1 (3) |
| C25—P1—C4—C11 | 70.06 (15) | PI-CI9-C20-C21 | 178.33 (14) |
| CI-PI-C4-CII | -176.01(13) | C19—C20—C21—C22 | 0.0 (3) |
| C6-O2-C5-O1 | 0.0 (3) | C20—C21—C22—C23 | -1.5(3) |
| C6 | -175.0 (2) | C21—C22—C23—C24 | 0.9 (3) |
| C2-C1-C5-O1 | 176.41 (15) | C22—C23—C24—C19 | 1.2 (3) |
| C13—C1—C5—O1 | 48.8 (2) | C20—C19—C24—C23 | -2.7 (2) |
| P1-C1-C5-O1 | -72.36 (19) | P1—C19—C24—C23 | -178.96 (13) |
| C2C1C5O2 | -8.5 (2) | C4—P1—C25—C26 | -149.65 (14) |
| C13—C1—C5—O2 | -136.16 (15) | C19—P1—C25—C26 | -16.38 (17) |
| P1—C1—C5—O2 | 102.70 (15) | C1—P1—C25—C26 | 106.15 (16) |
| C8—O4—C7—O3 | 1.7 (3) | C4—P1—C25—C30 | 30.89 (19) |
| C8—O4—C7—C2 | -178.33 (17) | C19—P1—C25—C30 | 164.16 (17) |
| C3—C2—C7—O3 | -9.5 (2) | C1—P1—C25—C30 | -73.31 (19) |
| C1—C2—C7—O3 | 179.04 (15) | C30—C25—C26—C27 | -0.9 (3) |
| C3—C2—C7—O4 | 170.58 (14) | P1-C25-C26-C27 | 179.64 (15) |
| C1—C2—C7—O4 | -0.9 (2) | C25—C26—C27—C28 | 1.3 (3) |
| C10-06-C9-O5 | -6.5(3) | C26—C27—C28—C29 | -0.3 (4) |

| С10—О6—С9—С3 | 173.85 (15) | C27—C28—C29—C30 | -0.9 (5) |
|--------------|-------------|-----------------|-----------|
| C2—C3—C9—O5 | 94.9 (2) | C28—C29—C30—C25 | 1.3 (5) |
| C4—C3—C9—O5 | -82.8 (2) | C26—C25—C30—C29 | -0.4 (4) |
| C2—C3—C9—O6 | -85.44 (17) | P1-C25-C30-C29 | 179.1 (2) |
| C4—C3—C9—O6 | 96.92 (17) | | |