organic compounds

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5-tert-Butyl 1-ethyl 3-amino-1,4,5,6tetrahydropyrrolo[3,4-c]pyrazole-1,5dicarboxylate

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Key indicators: single-crystal X-ray study; T = 296 K; mean σ (C–C) = 0.003 Å; R factor = 0.047; wR factor = 0.128; data-to-parameter ratio = 13.2.

The asymmetric unit of the title compound, C₁₃H₂₀N₄O₄, contains two crystallographically independent molecules in which the dihedral angles between the fused pyrrole and pyrazole rings are 5.06(8) and $1.12(8)^{\circ}$. In the crystal, molecules are linked by intermolecular $N-H\cdots O$ and N- $H \cdots N$ hydrogen bonds into chains parallel to the *b* axis.

Related literature

For general background to potential anticancer kinase inhibitors, see: Fancelli et al. (2005); Gadekar et al. (1968). For the structure of a related compound synthesized by our group, see: Guo et al. (2010).



Experimental

Crystal data

α β

$C_{13}H_{20}N_4O_4$	$\gamma = 85.821 \ (5)^{\circ}$
$M_r = 296.33$	V = 1465.2 (7) Å ³
Triclinic, $P\overline{1}$	Z = 4
a = 10.772 (3) Å	Mo $K\alpha$ radiation
b = 12.180 (4) Å	$\mu = 0.10 \text{ mm}^{-1}$
c = 12.986 (4) Å	T = 296 K
$\alpha = 70.845 \ (5)^{\circ}$	$0.06 \times 0.05 \times 0.04 \text{ mm}$
$\beta = 65.875 \ (4)^{\circ}$	

7444 measured reflections 5102 independent reflections

 $R_{\rm int} = 0.026$

387 parameters

 $\Delta \rho_{\rm max} = 0.26 \text{ e} \text{ Å}^-$

 $\Delta \rho_{\rm min} = -0.32 \text{ e} \text{ Å}^{-3}$

3915 reflections with $I > 2\sigma(I)$

H-atom parameters constrained

Data collection

Bruker APEXII CCD	
diffractometer	
Absorption correction: multi-scan	
(SADABS; Bruker, 2008)	
$T_{\min} = 0.994, \ T_{\max} = 0.996$	

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.047$	
$wR(F^2) = 0.128$	
S = 1.03	
5102 reflections	

Table 1 Hydrogen-bond geometry (Å, °).

$D - H \cdot \cdot \cdot A$	$D-\mathrm{H}$	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
N8-H8"····O4 ⁱ	0.86	2.25	3.069 (3)	160
$N8 - H8' \cdots N2^{ii}$	0.86	2.26	3.087 (3)	163
$N4-H4' \cdots N6^{iii}$	0.90	2.25	3.104 (3)	157
$N4-H4"\cdots O8^{iv}$	0.90	2.36	3.233 (3)	163

Symmetry codes: (i) x + 1, y, z; (ii) x + 1, y + 1, z; (iii) x - 1, y - 1, z; (iv) x - 1, y, z.

Data collection: APEX2 (Bruker, 2008); cell refinement: SAINT (Bruker, 2008); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXTL.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: RZ2580).

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supporting information

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5-*tert*-Butyl 1-ethyl 3-amino-1,4,5,6-tetrahydropyrrolo[3,4-c]pyrazole-1,5-dicarboxylate

Wen-Bin Xia, Xiao-Guang Bai, Hong-Tao Liu and Ju-Xian Wang

S1. Comment

As an extension of our work (Guo *et al.*, 2010) on the development of potential anticancer kinase inhibitors (Fancelli *et al.*, 2005; Gadekar *et al.*, 1968), we have synthesized the title compound and report its crystal structure herein.

The asymmetric unit of the title compound (Fig. 1) contains two crystallographically independent molecules. All bond lengths and angles have normal values. The dihedral angles between the fused pyrrole and pyrazole rings are 5.06 (8) and 1.12 (8)°. The C6/O1/O2/C7 and C9/O4/O3/C10 mean planes form dihedral angles of $5.83(0.09)^\circ$ and $14.86(0.10)^\circ$, respectively, with the mean plane through N1/N2/C2/C1/C3/C4/C5/N3, whereas the O8/C22/O7/C23 and C18/O5/O6/C17 mean planes form dihedral angles of $6.20(0.12)^\circ$ and $5.12(0.13)^\circ$, respectively, with the N5/N6/C14/C15/C16/C20/C21/N7 mean plane. In the crystal structure (Fig.2), molecules are linked by intermolecular N —H…O and N—H…N hydrogen bonds (Table 1) to form chains running parallel to the *b* axis.

S2. Experimental

A solution of ethyl chlorocarbonate (2.90 g, 12 mmol) in THF (30 ml) was slowly added dropwise to a mixture of *tert*butyl 3-aminopyrrolo[3,4-*c*]pyrazole-5(1*H*,4*H*,6*H*)-carboxylate (3.3 g, 11 mmol) and DIEA (8.54 g, 66 mmol) in THF (60 ml) at $0\sim5$ °C. The reaction was kept at the same temperature for 2 h, allowed to reach r.t., and stirred overnight. The obtained mixture was evaporated to dryness and the resulting residue extracted with AcOEt and water. The organic layer was separated, dried over sodium sulfate, and evaporated to dryness. The residue was purified by flash chromatography to give 1.8 g (55%) of the title compound as a white solid. Colourless block crystals suitable for X-ray diffraction were obtained in 2 days by slow evaporation of a methanol solution.

S3. Refinement

The hydrogen atoms could have been discerned in the difference Fourier map, nevertheless all H atoms were placed at calculated positions and refined as riding, with C—H = 0.96-0.97 Å, N—H = 0.86-0.90 Å, and with $U_{iso}(H) = 1.2 U_{eq}(C, N)$ or 1.5 $U_{eq}(C)$ for methyl H atoms.



Figure 1

The molecular structure of the title compound with displacement ellipsoids drawn at the 30% probability level.



Figure 2

Packing diagram of the title compound viewed along the c axis. Hydrogen bonds are shown as dashed lines.

5-tert-Butyl 1-ethyl 3-amino-1,4,5,6-tetrahydropyrrolo[3,4-c]pyrazole-1,5-dicarboxylate

Crystal data	
$C_{13}H_{20}N_4O_4$	Z = 4
$M_r = 296.33$	F(000) = 632
Triclinic, $P\overline{1}$	$D_{\rm x} = 1.343 {\rm Mg} {\rm m}^{-3}$
Hall symbol: -P 1	Mo <i>K</i> α radiation, $\lambda = 0.71073$ Å
a = 10.772 (3) Å	Cell parameters from 2737 reflections
b = 12.180 (4) Å	$\theta = 2.6 - 28.0^{\circ}$
c = 12.986 (4) Å	$\mu=0.10~\mathrm{mm^{-1}}$
$\alpha = 70.845 \ (5)^{\circ}$	T = 296 K
$\beta = 65.875 \ (4)^{\circ}$	Block, colourless
$\gamma = 85.821 (5)^{\circ}$	$0.06 \times 0.05 \times 0.04 \text{ mm}$
$V = 1465.2 (7) \text{ Å}^3$	
Data collection	
Bruker APEXII CCD	7444 measured reflections
diffractometer	5102 independent reflections
Radiation source: fine-focus sealed tube	3915 reflections with $I > 2\sigma(I)$
Graphite monochromator	$R_{\rm int} = 0.026$
φ and ω scans	$\theta_{\rm max} = 25.0^\circ, \ \theta_{\rm min} = 1.8^\circ$
Absorption correction: multi-scan	$h = -12 \rightarrow 10$
(SADABS; Bruker, 2008)	$k = -12 \rightarrow 14$
$T_{\min} = 0.994, \ T_{\max} = 0.996$	$l = -15 \rightarrow 10$

Refinement

Refinement on F^2	Secondary atom site location: difference Fourier
Least-squares matrix: full	map
$R[F^2 > 2\sigma(F^2)] = 0.047$	Hydrogen site location: inferred from
$wR(F^2) = 0.128$	neighbouring sites
S = 1.03	H-atom parameters constrained
5102 reflections	$w = 1/[\sigma^2(F_o^2) + (0.0632P)^2 + 0.4323P]$
387 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{\rm max} < 0.001$
Primary atom site location: structure-invariant	$\Delta ho_{ m max} = 0.26 \ { m e} \ { m \AA}^{-3}$
direct methods	$\Delta \rho_{\rm min} = -0.32 \text{ e} \text{ Å}^{-3}$

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	x	У	Ζ	$U_{ m iso}*/U_{ m eq}$
O1	0.26829 (15)	0.40073 (13)	0.06447 (14)	0.0348 (4)
O2	0.15420 (17)	0.22918 (13)	0.11483 (14)	0.0383 (4)
O3	0.18836 (13)	0.80172 (12)	0.11637 (12)	0.0248 (3)
O4	-0.02679 (14)	0.86224 (13)	0.15737 (14)	0.0303 (4)
O5	0.28280 (14)	1.06702 (13)	0.45631 (14)	0.0333 (4)
O6	0.39625 (15)	1.23659 (13)	0.41233 (14)	0.0348 (4)
07	0.33735 (13)	0.66947 (12)	0.40945 (12)	0.0263 (3)
O8	0.54850 (14)	0.63169 (12)	0.29063 (12)	0.0264 (3)
N1	0.04383 (17)	0.39313 (15)	0.13325 (15)	0.0266 (4)
N2	-0.08554 (17)	0.34058 (15)	0.17464 (16)	0.0278 (4)
N3	0.03062 (16)	0.69338 (14)	0.12056 (15)	0.0252 (4)
N4	-0.30512 (18)	0.40713 (16)	0.22648 (17)	0.0334 (5)
H4"	-0.3627	0.4607	0.2482	0.050*
H4′	-0.3438	0.3339	0.2641	0.050*
N5	0.50579 (16)	1.08232 (14)	0.36264 (15)	0.0240 (4)
N6	0.63493 (17)	1.14050 (15)	0.30111 (15)	0.0259 (4)
N7	0.51226 (16)	0.79033 (14)	0.34994 (15)	0.0238 (4)
N8	0.85181 (18)	1.08823 (16)	0.19749 (17)	0.0363 (5)
H8′	0.8873	1.1559	0.1818	0.044*
H8"	0.9026	1.0366	0.1726	0.044*
C1	0.0358 (2)	0.50843 (17)	0.12258 (17)	0.0240 (5)
C2	-0.1695 (2)	0.42522 (18)	0.18909 (18)	0.0265 (5)
C3	-0.0945 (2)	0.53222 (18)	0.15632 (18)	0.0239 (5)
C4	-0.1110 (2)	0.65547 (17)	0.15288 (19)	0.0252 (5)
H4D	-0.1435	0.6998	0.0929	0.030*

H4E	-0.1721	0.6611	0.2300	0.030*
C5	0.1312 (2)	0.60819 (17)	0.08967 (18)	0.0247 (5)
H5A	0.1848	0.5907	0.1369	0.030*
H5B	0.1914	0.6337	0.0054	0.030*
C6	0.1580 (2)	0.33069 (19)	0.10486 (18)	0.0289 (5)
C7	0.3986 (2)	0.3522 (2)	0.0194 (2)	0.0403 (6)
H7A	0.4667	0.4144	-0.0399	0.048*
H7B	0.3917	0.2983	-0.0191	0.048*
C8	0.4422(3)	0.2901 (3)	0.1178 (2)	0.0500(7)
H8D	0.4388	0.3408	0.1619	0.075*
H8E	0.5337	0.2679	0.0845	0.075*
H8F	0.3822	0.2218	0.1703	0.075*
C9	0.0578(2)	0.79265 (17)	0.13261 (18)	0.073 0.0233(5)
C10	0.0370(2) 0.24457(19)	0.99203(17) 0.90541(17)	0.12164 (18)	0.0230(5)
C11	0.21157(15)	0.90311(17) 0.87316(18)	0.12101(10) 0.10925(19)	0.0236(5)
H11A	0.3815	0.8011	0.1707	0.0200(3)
H11R	0.4315	0.0335	0.1168	0.043*
H11C	0.4371	0.9555	0.0324	0.043*
C12	0.4571 0.1652 (2)	0.0043	0.0324	0.045
U12	0.1052 (2)	0.9255 (2)	0.2469	0.0303 (3)
1112A Ц12D	0.0750	0.9433	0.2466	0.046*
	0.1577	0.9637	0.2400	0.046*
C12	0.1377	1.00221 (12)	0.3038 0.01702 (18)	0.040°
U13	0.2401(2)	1.00661 (16)	0.01703 (18)	0.0279(3)
ПІЗА 1112D	0.2999	0.9927	-0.0339	0.042*
	0.2899	1.0700	0.0100	0.042*
ПІЗС	0.1307	1.0233	0.0239	0.042°
C14	0./1/5(2)	1.00333(17)	0.26074 (18)	0.0242(5)
	0.6416(2)	0.95619 (17)	0.29503(17)	0.0223(4)
C16	0.5126 (2)	0.9/181 (1/)	0.35/43(17)	0.0226 (4)
C1/	0.3930 (2)	1.13870 (19)	0.41168 (18)	0.0272 (5)
	0.1527(2)	1.1110 (2)	0.5106 (2)	0.0393 (6)
HI8A	0.1624	1.1630	0.5500	0.04/*
HI8B	0.0880	1.0467	0.5/04	0.047*
C19	0.0999 (3)	1.1747 (3)	0.4194 (2)	0.0500 (7)
HI9A	0.1563	1.2452	0.3675	0.075*
HI9B	0.0080	1.1935	0.4585	0.075*
H19C	0.1014	1.1266	0.3734	0.075*
C20	0.4166 (2)	0.86791 (17)	0.40609 (18)	0.0245 (5)
H20A	0.3799	0.8369	0.4926	0.029*
H20B	0.3426	0.8839	0.3802	0.029*
C21	0.65594 (19)	0.83642 (17)	0.28762 (18)	0.0227 (4)
H21A	0.6951	0.8374	0.2055	0.027*
H21B	0.7108	0.7922	0.3283	0.027*
C22	0.4724 (2)	0.69102 (17)	0.34557 (17)	0.0223 (4)
C23	0.2682 (2)	0.55632 (18)	0.43977 (19)	0.0269 (5)
C24	0.3325 (2)	0.45964 (18)	0.5035 (2)	0.0318 (5)
H24A	0.4243	0.4547	0.4499	0.048*
H24B	0.2809	0.3872	0.5303	0.048*

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H24C	0.3335	0.4753	0.5710	0.048*	
C25	0.2688 (2)	0.5414 (2)	0.3285 (2)	0.0366 (6)	
H25A	0.2313	0.6073	0.2891	0.055*	
H25B	0.2148	0.4717	0.3500	0.055*	
H25C	0.3607	0.5358	0.2756	0.055*	
C26	0.1261 (2)	0.5688 (2)	0.5249 (2)	0.0355 (6)	
H26A	0.1310	0.5911	0.5876	0.053*	
H26B	0.0732	0.4958	0.5588	0.053*	
H26C	0.0837	0.6274	0.4825	0.053*	

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U ³³	U^{12}	U^{13}	U^{23}
01	0.0307 (8)	0.0283 (9)	0.0448 (9)	0.0079 (7)	-0.0123 (7)	-0.0166 (7)
O2	0.0497 (10)	0.0235 (9)	0.0474 (10)	0.0099 (7)	-0.0223 (8)	-0.0171 (7)
O3	0.0228 (7)	0.0174 (7)	0.0364 (8)	0.0017 (6)	-0.0129 (6)	-0.0105 (6)
O4	0.0246 (8)	0.0212 (8)	0.0471 (9)	0.0035 (6)	-0.0139 (7)	-0.0151 (7)
O5	0.0252 (8)	0.0301 (9)	0.0415 (9)	0.0043 (7)	-0.0074 (7)	-0.0165 (7)
O6	0.0394 (9)	0.0243 (9)	0.0429 (9)	0.0074 (7)	-0.0140 (7)	-0.0184 (7)
O7	0.0257 (8)	0.0195 (8)	0.0348 (8)	-0.0016 (6)	-0.0130 (6)	-0.0089 (6)
08	0.0308 (8)	0.0185 (8)	0.0308 (8)	0.0028 (6)	-0.0126 (6)	-0.0094 (6)
N1	0.0303 (9)	0.0179 (9)	0.0328 (10)	0.0031 (7)	-0.0125 (8)	-0.0106 (8)
N2	0.0319 (10)	0.0197 (9)	0.0331 (10)	0.0011 (8)	-0.0137 (8)	-0.0096 (8)
N3	0.0234 (9)	0.0187 (9)	0.0354 (10)	0.0032 (7)	-0.0120 (8)	-0.0115 (8)
N4	0.0298 (10)	0.0221 (10)	0.0455 (11)	-0.0031 (8)	-0.0124 (9)	-0.0103 (9)
N5	0.0252 (9)	0.0170 (9)	0.0291 (9)	0.0010 (7)	-0.0101 (7)	-0.0081 (7)
N6	0.0258 (9)	0.0191 (9)	0.0313 (10)	0.0001 (7)	-0.0100 (8)	-0.0083 (8)
N7	0.0241 (9)	0.0186 (9)	0.0309 (9)	0.0018 (7)	-0.0117 (7)	-0.0103 (7)
N8	0.0266 (10)	0.0200 (10)	0.0557 (13)	-0.0013 (8)	-0.0077 (9)	-0.0156 (9)
C1	0.0319 (11)	0.0191 (11)	0.0244 (10)	0.0021 (9)	-0.0134 (9)	-0.0088 (9)
C2	0.0340 (12)	0.0213 (11)	0.0256 (11)	-0.0009 (9)	-0.0134 (9)	-0.0070 (9)
C3	0.0274 (11)	0.0205 (11)	0.0269 (11)	0.0030 (9)	-0.0128 (9)	-0.0096 (9)
C4	0.0264 (11)	0.0188 (11)	0.0325 (11)	0.0003 (8)	-0.0133 (9)	-0.0090 (9)
C5	0.0267 (11)	0.0209 (11)	0.0290 (11)	0.0040 (9)	-0.0116 (9)	-0.0113 (9)
C6	0.0391 (13)	0.0229 (12)	0.0278 (11)	0.0068 (10)	-0.0148 (10)	-0.0116 (9)
C7	0.0344 (13)	0.0409 (15)	0.0446 (14)	0.0137 (11)	-0.0116 (11)	-0.0210 (12)
C8	0.0479 (15)	0.0555 (18)	0.0545 (17)	0.0147 (13)	-0.0253 (13)	-0.0244 (14)
C9	0.0248 (10)	0.0175 (10)	0.0254 (10)	-0.0007 (9)	-0.0097 (9)	-0.0047 (8)
C10	0.0221 (10)	0.0180 (10)	0.0280 (11)	-0.0034 (8)	-0.0092 (8)	-0.0068 (8)
C11	0.0268 (11)	0.0234 (11)	0.0346 (12)	0.0006 (9)	-0.0130 (9)	-0.0077 (9)
C12	0.0285 (11)	0.0338 (13)	0.0294 (11)	-0.0005 (9)	-0.0108 (9)	-0.0118 (10)
C13	0.0295 (11)	0.0211 (11)	0.0305 (11)	0.0025 (9)	-0.0107 (9)	-0.0074 (9)
C14	0.0284 (11)	0.0176 (11)	0.0270 (11)	0.0006 (9)	-0.0122 (9)	-0.0064 (9)
C15	0.0257 (11)	0.0175 (10)	0.0236 (10)	0.0007 (8)	-0.0108 (9)	-0.0055 (8)
C16	0.0284 (11)	0.0180 (10)	0.0237 (10)	0.0017 (8)	-0.0131 (9)	-0.0064 (8)
C17	0.0314 (12)	0.0255 (12)	0.0273 (11)	0.0054 (9)	-0.0125 (9)	-0.0119 (9)
C18	0.0292 (12)	0.0452 (15)	0.0402 (13)	0.0077 (11)	-0.0044 (10)	-0.0234 (12)
C19	0.0383 (14)	0.0593 (18)	0.0593 (17)	0.0192 (13)	-0.0192(13)	-0.0320 (15)

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C20	0.0247 (10)	0.0210 (11)	0.0285 (11)	0.0015 (8)	-0.0103 (9)	-0.0096 (9)
C21	0.0246 (10)	0.0169 (10)	0.0267 (11)	0.0009 (8)	-0.0110 (9)	-0.0065 (8)
C22	0.0276 (11)	0.0186 (10)	0.0225 (10)	-0.0001 (9)	-0.0148 (9)	-0.0027 (8)
C23	0.0323 (11)	0.0185 (11)	0.0330 (11)	-0.0043 (9)	-0.0175 (10)	-0.0054 (9)
C24	0.0380 (12)	0.0220 (12)	0.0354 (12)	-0.0013 (10)	-0.0192 (10)	-0.0033 (10)
C25	0.0477 (14)	0.0295 (13)	0.0372 (13)	-0.0068 (11)	-0.0231 (11)	-0.0075 (10)
C26	0.0305 (12)	0.0313 (13)	0.0441 (13)	-0.0056 (10)	-0.0174 (10)	-0.0073 (11)

Geometric parameters (Å, °)

O1—C6	1.327 (3)	C7—H7B	0.9700
O1—C7	1.447 (3)	C8—H8D	0.9600
O2—C6	1.202 (3)	C8—H8E	0.9600
O3—C9	1.341 (2)	C8—H8F	0.9600
O3—C10	1.473 (2)	C10—C11	1.507 (3)
O4—C9	1.216 (2)	C10—C13	1.508 (3)
O5—C17	1.328 (2)	C10—C12	1.509 (3)
O5—C18	1.442 (3)	C11—H11A	0.9600
O6—C17	1.198 (3)	C11—H11B	0.9600
O7—C22	1.341 (2)	C11—H11C	0.9600
O7—C23	1.471 (2)	C12—H12A	0.9600
O8—C22	1.216 (2)	C12—H12B	0.9600
N1-C1	1.365 (3)	C12—H12C	0.9600
N1-C6	1.379 (3)	C13—H13A	0.9600
N1—N2	1.390 (2)	C13—H13B	0.9600
N2—C2	1.330 (3)	C13—H13C	0.9600
N3—C9	1.336 (3)	C14—C15	1.430 (3)
N3—C5	1.471 (3)	C15—C16	1.329 (3)
N3—C4	1.472 (2)	C15—C21	1.486 (3)
N4—C2	1.347 (3)	C16—C20	1.484 (3)
N4—H4"	0.8999	C18—C19	1.486 (4)
N4—H4′	0.8999	C18—H18A	0.9700
N5-C16	1.365 (3)	C18—H18B	0.9700
N5—C17	1.373 (3)	C19—H19A	0.9600
N5—N6	1.393 (2)	C19—H19B	0.9600
N6-C14	1.330 (3)	C19—H19C	0.9600
N7—C22	1.339 (3)	C20—H20A	0.9700
N7—C21	1.473 (2)	C20—H20B	0.9700
N7—C20	1.477 (3)	C21—H21A	0.9700
N8—C14	1.338 (3)	C21—H21B	0.9700
N8—H8′	0.8600	C23—C24	1.504 (3)
N8—H8"	0.8600	C23—C26	1.511 (3)
C1—C3	1.329 (3)	C23—C25	1.512 (3)
C1—C5	1.482 (3)	C24—H24A	0.9600
C2—C3	1.429 (3)	C24—H24B	0.9600
C3—C4	1.487 (3)	C24—H24C	0.9600
C4—H4D	0.9700	C25—H25A	0.9600
C4—H4E	0.9700	C25—H25B	0.9600

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	С5—Н5А	0.9700	C25—H25C	0.9600
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	С5—Н5В	0.9700	C26—H26A	0.9600
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C7—C8	1.494 (4)	C26—H26B	0.9600
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	С7—Н7А	0.9700	C26—H26C	0.9600
$\begin{array}{llllllllllllllllllllllllllllllllllll$				
$\begin{array}{llllllllllllllllllllllllllllllllllll$	C6—O1—C7	116.59 (18)	C10-C12-H12A	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C9—O3—C10	120.85 (15)	C10-C12-H12B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C17—O5—C18	117.13 (18)	H12A—C12—H12B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C22—O7—C23	121.69 (16)	C10-C12-H12C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C1—N1—C6	128.99 (18)	H12A—C12—H12C	109.5
$\begin{array}{llllllllllllllllllllllllllllllllllll$	C1—N1—N2	110.17 (16)	H12B—C12—H12C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C6—N1—N2	120.78 (17)	C10—C13—H13A	109.5
$\begin{array}{llllllllllllllllllllllllllllllllllll$	C2—N2—N1	104.91 (16)	C10-C13-H13B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C9—N3—C5	124.64 (17)	H13A—C13—H13B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C9—N3—C4	120.16 (17)	C10—C13—H13C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C5—N3—C4	114.81 (15)	H13A—C13—H13C	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C2—N4—H4"	121.4	H13B—C13—H13C	109.5
$\begin{array}{llllllllllllllllllllllllllllllllllll$	C2—N4—H4′	119.3	N6—C14—N8	122.08 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	H4"—N4—H4′	112.9	N6—C14—C15	110.37 (17)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C16—N5—C17	128.92 (17)	N8—C14—C15	127.55 (19)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C16—N5—N6	110.18 (16)	C16—C15—C14	106.07 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C17—N5—N6	120.77 (16)	C16—C15—C21	111.02 (17)
$\begin{array}{cccccc} C22-N7-C21 & 121.67 (17) & C15-C16-N5 & 108.47 (17) \\ C22-N7-C20 & 123.51 (16) & C15-C16-C20 & 114.67 (18) \\ C21-N7-C20 & 114.55 (15) & N5-C16-C20 & 136.80 (18) \\ C14-N8-H8' & 120.0 & 06-C17-O5 & 126.8 (2) \\ C14-N8-H8'' & 120.0 & 05-C17-N5 & 124.59 (19) \\ H8'-N8-H8'' & 120.0 & 05-C18-C19 & 110.85 (19) \\ C3-C1-N1 & 108.48 (18) & 05-C18-C19 & 110.85 (19) \\ C3-C1-C5 & 114.49 (19) & 05-C18-H18A & 109.5 \\ N1-C1-C5 & 136.95 (19) & C19-C18-H18A & 109.5 \\ N2-C2-N4 & 121.98 (19) & 05-C18-H18B & 109.5 \\ N2-C2-C3 & 110.42 (18) & C19-C18-H18B & 109.5 \\ N4-C2-C3 & 127.6 (2) & H18A-C18-H18B & 109.5 \\ C1-C3-C2 & 106.00 (19) & C18-C19-H19A & 109.5 \\ C2-C3-C4 & 111.15 (17) & C18-C19-H19B & 109.5 \\ C2-C3-C4 & 112.74 (19) & H19A-C19-H19B & 109.5 \\ N3-C4-C3 & 100.28 (16) & C18-C19-H19C & 109.5 \\ N3-C4-H4D & 111.7 & H19A-C19-H19C & 109.5 \\ N3-C4-H4E & 111.7 & N7-C20-C16 & 98.60 (15) \\ C3-C4-H4E & 111.7 & N7-C20-C16 & 98.60 (15) \\ C3-C4-H4E & 111.7 & N7-C20-H20A & 112.0 \\ H4D-C4-H4E & 109.5 & C16-C20-H20B & 112.0 \\ N3-C5-C1 & 98.69 (16) & N7-C20-H20B & 112.0 \\ N3-C5-H5A & 112.0 & C16-C20-H20B & 112.0 \\ N3-C5-H5A & 112.0 & N7-C21-C15 & 100.59 (16) \\ \end{array}$	C14—N6—N5	104.90 (16)	C14—C15—C21	142.89 (19)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C22—N7—C21	121.67 (17)	C15—C16—N5	108.47 (17)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C22—N7—C20	123.51 (16)	C15—C16—C20	114.67 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C21—N7—C20	114.55 (15)	N5-C16-C20	136.80 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C14—N8—H8'	120.0	O6—C17—O5	126.8 (2)
H8'-N8-H8"120.0 $05-C17-N5$ $108.57 (17)$ C3-C1-N1 $108.48 (18)$ $05-C18-C19$ $110.85 (19)$ C3-C1-C5 $114.49 (19)$ $05-C18-H18A$ 109.5 N1-C1-C5 $136.95 (19)$ $C19-C18-H18A$ 109.5 N2-C2-N4 $121.98 (19)$ $05-C18-H18B$ 109.5 N2-C2-C3 $110.42 (18)$ $C19-C18-H18B$ 109.5 N4-C2-C3 $127.6 (2)$ $H18A-C18-H18B$ 109.5 C1-C3-C2 $106.00 (19)$ $C18-C19-H19A$ 109.5 C1-C3-C4 $111.15 (17)$ $C18-C19-H19B$ 109.5 C2-C3-C4 $142.74 (19)$ $H19A-C19-H19B$ 109.5 N3-C4-C3 $100.28 (16)$ $C18-C19-H19C$ 109.5 C3-C4-H4D 111.7 $H19B-C19-H19C$ 109.5 C3-C4-H4D 111.7 $H19B-C19-H19C$ 109.5 N3-C4-H4E 111.7 $N7-C20-C16$ $98.60 (15)$ C3-C4-H4E 111.7 $N7-C20-H20A$ 112.0 H4D-C4-H4E 109.5 $C16-C20-H20A$ 112.0 N3-C5-C1 $98.69 (16)$ $N7-C20-H20B$ 112.0 N3-C5-H5A 112.0 $C16-C20-H20B$ 112.0 C1-C5-H5A 112.0 $N7-C21-C15$ $100.59 (16)$	C14—N8—H8"	120.0	O6—C17—N5	124.59 (19)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	H8′—N8—H8"	120.0	O5—C17—N5	108.57 (17)
C3—C1—C5114.49 (19)O5—C18—H18A109.5N1—C1—C5136.95 (19)C19—C18—H18A109.5N2—C2—N4121.98 (19)O5—C18—H18B109.5N2—C2—C3110.42 (18)C19—C18—H18B108.1C1—C3—C2106.00 (19)C18—C19—H19A109.5C1—C3—C4111.15 (17)C18—C19—H19B109.5C2—C3—C4142.74 (19)H19A—C19—H19B109.5N3—C4—C3100.28 (16)C18—C19—H19C109.5C3—C4111.7H19A—C19—H19C109.5C3—C4—H4D111.7H19B—C19—H19C109.5C3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—H5A112.0C16—C20—H20B112.0N3—C5—H5A112.0N7—C20—H20B112.0N3—C5—H5B112.0N7—C21—C15100.59 (16)	C3—C1—N1	108.48 (18)	O5—C18—C19	110.85 (19)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C3—C1—C5	114.49 (19)	O5—C18—H18A	109.5
N2—C2—N4121.98 (19)O5—C18—H18B109.5N2—C2—C3110.42 (18)C19—C18—H18B109.5N4—C2—C3127.6 (2)H18A—C18—H18B108.1C1—C3—C2106.00 (19)C18—C19—H19A109.5C1—C3—C4111.15 (17)C18—C19—H19B109.5C2—C3—C4142.74 (19)H19A—C19—H19B109.5N3—C4—C3100.28 (16)C18—C19—H19C109.5N3—C4—H4D111.7H19A—C19—H19C109.5N3—C4—H4D111.7H19B—C19—H19C109.5N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0N7—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N1—C1—C5	136.95 (19)	C19—C18—H18A	109.5
$\begin{array}{llllllllllllllllllllllllllllllllllll$	N2-C2-N4	121.98 (19)	O5—C18—H18B	109.5
N4—C2—C3127.6 (2)H18A—C18—H18B108.1C1—C3—C2106.00 (19)C18—C19—H19A109.5C1—C3—C4111.15 (17)C18—C19—H19B109.5C2—C3—C4142.74 (19)H19A—C19—H19B109.5N3—C4—C3100.28 (16)C18—C19—H19C109.5N3—C4—H4D111.7H19A—C19—H19C109.5C3—C4—H4D111.7H19B—C19—H19C109.5N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0N7—C21—C15100.59 (16)	N2—C2—C3	110.42 (18)	C19—C18—H18B	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	N4—C2—C3	127.6 (2)	H18A—C18—H18B	108.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C1—C3—C2	106.00 (19)	C18—C19—H19A	109.5
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C1—C3—C4	111.15 (17)	C18—C19—H19B	109.5
N3—C4—C3100.28 (16)C18—C19—H19C109.5N3—C4—H4D111.7H19A—C19—H19C109.5C3—C4—H4D111.7H19B—C19—H19C109.5N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	C2—C3—C4	142.74 (19)	H19A—C19—H19B	109.5
N3—C4—H4D111.7H19A—C19—H19C109.5C3—C4—H4D111.7H19B—C19—H19C109.5N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N3—C4—C3	100.28 (16)	C18—C19—H19C	109.5
C3—C4—H4D111.7H19B—C19—H19C109.5N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N3—C4—H4D	111.7	H19A—C19—H19C	109.5
N3—C4—H4E111.7N7—C20—C1698.60 (15)C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	C3—C4—H4D	111.7	H19B—C19—H19C	109.5
C3—C4—H4E111.7N7—C20—H20A112.0H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N3—C4—H4E	111.7	N7—C20—C16	98.60 (15)
H4D—C4—H4E109.5C16—C20—H20A112.0N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	C3—C4—H4E	111.7	N7—C20—H20A	112.0
N3—C5—C198.69 (16)N7—C20—H20B112.0N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	H4D—C4—H4E	109.5	C16—C20—H20A	112.0
N3—C5—H5A112.0C16—C20—H20B112.0C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N3—C5—C1	98.69 (16)	N7—C20—H20B	112.0
C1—C5—H5A112.0H20A—C20—H20B109.7N3—C5—H5B112.0N7—C21—C15100.59 (16)	N3—C5—H5A	112.0	C16—C20—H20B	112.0
N3—C5—H5B 112.0 N7—C21—C15 100.59 (16)	C1—C5—H5A	112.0	H20A—C20—H20B	109.7
	N3—C5—H5B	112.0	N7—C21—C15	100.59 (16)

C1 C5 U5D	112.0		111 7
	112.0	$N = C_{21} = H_{21}A$	111.7
H5A—C5—H5B	109.7	CI5-C21-H2IA	111.7
02-00-01	127.0 (2)	$N = C_2 = H_2 B$	111.7
02-C6-N1	123.8 (2)	C15—C21—H21B	111./
OI—C6—NI	109.18 (18)	H21A—C21—H21B	109.4
01	111.1 (2)	08—C22—N7	124.23 (18)
01—C7—H7A	109.4	08—C22—O7	126.38 (18)
С8—С7—Н7А	109.4	N7—C22—O7	109.38 (18)
O1—C7—H7B	109.4	O7—C23—C24	110.13 (16)
С8—С7—Н7В	109.4	O7—C23—C26	101.64 (17)
H7A—C7—H7B	108.0	C24—C23—C26	109.97 (18)
C7—C8—H8D	109.5	O7—C23—C25	109.88 (16)
С7—С8—Н8Е	109.5	C24—C23—C25	112.93 (19)
H8D—C8—H8E	109.5	C26—C23—C25	111.72 (18)
C7—C8—H8F	109.5	C23—C24—H24A	109.5
H8D—C8—H8F	109.5	C23—C24—H24B	109.5
H8E—C8—H8F	109.5	H24A—C24—H24B	109.5
O4—C9—N3	123.50 (18)	C23—C24—H24C	109.5
O4—C9—O3	126.06 (18)	H24A—C24—H24C	109.5
N3—C9—O3	110.43 (18)	H24B—C24—H24C	109.5
O3-C10-C11	102.22 (16)	C23—C25—H25A	109.5
03-010-013	108.64 (16)	C23—C25—H25B	109.5
$C_{11} - C_{10} - C_{13}$	111 19 (16)	H25A—C25—H25B	109.5
03-C10-C12	111.02 (15)	C_{23} C_{25} H_{25}	109.5
$C_{11} - C_{10} - C_{12}$	110.02(13) 110.14(18)	$H_{25}^{-} = H_{25}^{-} = H_{$	109.5
C_{13} C_{10} C_{12}	113.09(18)	$H_{25R} = C_{25} = H_{25C}$	109.5
$C_{10} = C_{10} = C_{12}$	100 5	C_{23} C_{26} H_{26A}	109.5
$C_{10} = C_{11} = H_{11}$	109.5	C_{23} C_{26} H_{26} H_{26}	109.5
	109.5	C_{23} C_{20} C	109.5
	109.5	$H_{20}A = C_{20} = H_{20}B$	109.5
	109.5	C23-C20-H26C	109.5
HIIA—CII—HIIC	109.5	$H_{2}bA = C_{2}b = H_{2}bC$	109.5
HIIB—CII—HIIC	109.5	H26B—C26—H26C	109.5
$C1_N1_N2_C2$	-0.5(2)	C9 - 03 - C10 - C13	-67.0(2)
$C_1 = N_1 = N_2 = C_2$	-178.02(18)	$C_{9} = 03 = C_{10} = C_{13}$	580(2)
$C_{16} = N_{1} = N_{2} = C_{2}$	-0.5(2)	N5 N6 C14 N8	-170.34(10)
C17 N5 N6 C14	-176.67.(18)	$N_{5} = N_{6} = C_{14} = N_{6}$	179.34(19)
$C_1 = N_0 = N_0 = C_1 + C_2$	170.07(10)	$N_{0} = N_{0} = C_{14} = C_{15}$	-0.5(2)
$C_0 = N_1 = C_1 = C_3$	1/7.0(2)	$N_{0} = C_{14} = C_{15} = C_{10}$	-0.3(2)
$N_2 - N_1 - C_1 - C_3$	0.4(2)	$N_{0} = C_{14} = C_{15} = C_{16}$	1/9.4(2)
C_{0} NI C_{1} C_{5}	-5.9(4)	$N_0 - C_1 4 - C_1 5 - C_2 1$	-1/9.0(3)
N2—N1—C1—C5	176.8 (2)	N8—C14—C15—C21	0.9 (4)
N1—N2—C2—N4	178.65 (18)	C14—C15—C16—N5	0.2 (2)
N1—N2—C2—C3	0.4 (2)	C21—C15—C16—N5	179.20 (16)
N1—C1—C3—C2	-0.1 (2)	C14—C15—C16—C20	-177.62 (17)
C5—C1—C3—C2	-177.45 (17)	C21—C15—C16—C20	1.4 (3)
N1—C1—C3—C4	177.00 (17)	C17—N5—C16—C15	175.96 (19)
C5—C1—C3—C4	-0.4 (3)	N6—N5—C16—C15	0.2 (2)
N2—C2—C3—C1	-0.2 (2)	C17—N5—C16—C20	-7.0 (4)

-178.3(2)	N6—N5—C16—C20	177.3 (2)
-175.7 (3)	C18—O5—C17—O6	0.6 (3)
6.1 (4)	C18—O5—C17—N5	-179.03 (17)
-165.54 (18)	C16—N5—C17—O6	-180.0 (2)
7.5 (2)	N6—N5—C17—O6	-4.6 (3)
-4.2 (2)	C16—N5—C17—O5	-0.4 (3)
171.2 (3)	N6—N5—C17—O5	175.03 (16)
165.14 (19)	C17—O5—C18—C19	86.1 (3)
-7.6 (2)	C22—N7—C20—C16	-166.46 (18)
4.7 (2)	C21—N7—C20—C16	7.7 (2)
-171.7 (2)	C15—C16—C20—N7	-5.4 (2)
4.9 (3)	N5-C16-C20-N7	177.7 (2)
-174.19 (18)	C22—N7—C21—C15	167.14 (18)
-178.0 (2)	C20—N7—C21—C15	-7.1 (2)
-0.9 (3)	C16—C15—C21—N7	3.3 (2)
1.1 (3)	C14—C15—C21—N7	-178.2 (3)
178.17 (16)	C21—N7—C22—O8	-0.6 (3)
-86.4 (2)	C20—N7—C22—O8	173.13 (19)
179.44 (19)	C21—N7—C22—O7	-179.94 (16)
-8.2 (3)	C20—N7—C22—O7	-6.2 (3)
-2.0 (3)	C23—O7—C22—O8	12.3 (3)
170.39 (16)	C23—O7—C22—N7	-168.41 (16)
-3.2 (3)	C22—O7—C23—C24	55.5 (2)
178.21 (16)	C22—O7—C23—C26	172.01 (17)
175.42 (17)	C22—O7—C23—C25	-69.6 (2)
	-178.3 (2) -175.7 (3) 6.1 (4) -165.54 (18) 7.5 (2) -4.2 (2) 171.2 (3) 165.14 (19) -7.6 (2) 4.7 (2) -171.7 (2) 4.9 (3) -174.19 (18) -178.0 (2) -0.9 (3) 1.1 (3) 178.17 (16) -86.4 (2) 179.44 (19) -8.2 (3) -2.0 (3) 170.39 (16) -3.2 (3) 175.42 (17)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Hydrogen-bond geometry (Å, °)

D—H···A	<i>D</i> —Н	H···A	D··· A	<i>D</i> —H…A
N8—H8"…O4 ⁱ	0.86	2.25	3.069 (3)	160
N8—H8′····N2 ⁱⁱ	0.86	2.26	3.087 (3)	163
$N4$ — $H4'$ ··· $N6^{iii}$	0.90	2.25	3.104 (3)	157
N4—H4" \cdots O8 ^{iv}	0.90	2.36	3.233 (3)	163

Symmetry codes: (i) *x*+1, *y*, *z*; (ii) *x*+1, *y*+1, *z*; (iii) *x*-1, *y*-1, *z*; (iv) *x*-1, *y*, *z*.