V = 6343.67 (19) Å³

 $0.18 \times 0.16 \times 0.13~\text{mm}$

64493 measured reflections

13208 independent reflections

7192 reflections with $I > 2\sigma(I)$

constrained

Mo $K\alpha$ radiation $\mu = 0.09 \text{ mm}^-$

Z = 8

T = 293 K

 $R_{\rm int} = 0.046$

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(2RS,3SR,10SR,11RS)-3,10-Diphenoxy-18,21-dioxa-5,8-diazapentacyclo- $[20.4.0.0^{2,5}.0^{8,11}.0^{12,17}]$ hexacosa-1(26),12,14,16,22,24-hexaene-4,9-dione ethyl acetate hemisolvate

I. Suresh,^a Nataraian Arumugam,^b Abdulrahman I. Almansour,^b Usama Karama^b and P. L. Nilantha Lakshman^c*

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Key indicators: single-crystal X-ray study; T = 293 K; mean σ (C–C) = 0.004 Å; R factor = 0.053; wR factor = 0.175; data-to-parameter ratio = 16.2.

In the title compound, $C_{34}H_{30}N_2O_6 \cdot 0.5C_4H_8O_2$, there are two molecules in the asymmetric unit and the structure is stabilized by C-H···O interactions. The two nonsolvent molecules of the asymmetric unit are linked together by a weak $C-H \cdots O$ hydrogen bond. The ethyl acetate molecule is present as a space filler and does not participate in the hydrogen-bonding network.

Related literature

For background to the pharmaceutical applications of β lactam antibiotics, see: Samarendra et al. (1994); Vaccaro & Davis (1998); Vaccaro et al. (1998); Borthwick et al. (1998).



Experimental

Crystal data

 $C_{34}H_{30}N_2O_6 \cdot 0.5(C_4H_8O_2)$ $M_r = 606.65$ Monoclinic, $P2_1/n$ a = 18.037 (3) Å b = 17.201 (3) Å c = 21.589 (4) Å $\beta = 108.722 (1)^{\circ}$

Data collection

Bruker SMART APEX CCD diffractometer Absorption correction: multi-scan (SADABS; Bruker, 1998) $T_{\min} = 0.984, \ T_{\max} = 0.988$

Refinement

813 parameters
H-atom parameters c
$\Delta \rho_{\rm max} = 0.32 \text{ e} \text{ Å}^{-3}$
$\Delta \rho_{\rm min} = -0.24 \text{ e } \text{\AA}^{-3}$

Table 1 Hydrogen-bond geometry (Å, °).

$D - H \cdot \cdot \cdot A$	$D-\mathrm{H}$	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
С53—Н53…О6	0.93	2.52	3.344 (3)	147
$C2-H2 \cdot \cdot \cdot O2$	0.93	2.42	3.250 (3)	149
C32−H32···O1	0.93	2.33	3.178 (3)	151
C66−H66···O7	0.93	2.48	3.299 (3)	147

Data collection: SMART (Bruker, 2001); cell refinement: SAINT (Bruker, 2001); data reduction: SAINT; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: PLATON (Spek, 2009); software used to prepare material for publication: SHELXL97.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: LW2069).

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supporting information

Acta Cryst. (2011). E67, o2203 [doi:10.1107/S1600536811030200]

(2*RS*,3*SR*,10*SR*,11*RS*)-3,10-Diphenoxy-18,21-dioxa-5,8-diazapentacyclo-[20.4.0.0^{2,5}.0^{8,11}.0^{12,17}]hexacosa-1(26),12,14,16,22,24-hexaene-4,9-dione ethyl acetate hemisolvate

J. Suresh, Natarajan Arumugam, Abdulrahman I. Almansour, Usama Karama and P. L. Nilantha Lakshman

S1. Comment

 β -Lactam antibiotics are widely employed in the treatment of bacterial infections(Samarendra *et al.*, 1994). In recent years, several natural β -lactams have been shown to exhibit a high antibacterial activity. 1,3,4-trisubstituted β -lactams were found to be new, potent cholesterol absorption inhibitors (Vaccaro & Davis 1998; Vaccaro *et al.*, 1998) human cytomegalovirus (Borthwick *et al.*, 1998). Furthermore, many anticancer drugs in current use are toxic and thus limited in their efficacy. It is therefore essential to develop novel chemotherapeutic agents with lower levels of toxicity. β -lactam antibiotics have been used for many years with limited or no toxicity. In view of this, the crystal structure determination of the title compound was carried out.

The asymmetric unit of (I) contain two independent molecules, The pair have almost identical geometry. The internal angles of the four-membered rings of the title compound, (I), vary from 85.3 (8) to 96.2 (5)°. The sums of the bond angles at the N atoms are 359.4 (2) and 360.0 (1),359.3 (8) 359.9 (5) for N1, N2,N3 and N4 respectively are in accordance with sp^2 hybridization. The conformation of the molecules is stabilized by weak intramolecular C—H···O and C—H···N interactions, (Table 1). The two non-solvent molecules of the asymmetruc unit are linked together by a weak C —H···O hydrogen bond. The presence of the ethyl acetate solvent as a mere space filler suggests that its contribution to the intermolecular interactions is insignificant but it has nevertheless played a role in crystallization. There is a solvent accessible void of 66.7 Å³ in the structure.

S2. Experimental

A solution of phenoxyacetyl chloride in dry dichloromethane (20 ml) was slowly added to a solution of bisimine (1 mmol) and Et₃N (3.5 mmol) in dichloromethane (20 ml) at 0 °C and the reaction mixture was stirred for 12 h at room temperature. Completion of the reaction evidenced by TLC analysis, the reaction mixture was washed with water (2 X 20 ml), saturated NaHCO₃ (15 ml) and brine (15 ml). The organic layer was dried over anhydrous Na₂SO₄ and concentrated under reduced pressure. The crude product was separated by column chromatography (hexane: ethyl acetate 7:3) gave pure bis- β -lactam in good yield. The product was recrystallized from ethyl acetate by slow evaporation technique. m.p.: 195°C, yield: 48%

S3. Refinement

The H atoms were placed in calculated positions and allowed to ride on their carrier atoms with C—H = 0.93–0.98 Å and $U_{iso} = 1.2U_{eq}(C)$ for CH, CH₂ groups and $U_{iso} = 1.5U_{eq}(C)$ for CH₃ group.



Figure 1

One of the molecule of the two independent molecules and the solvent molecule ethyl acetate of the asymmetric unit(I), showing 10% probability displacement ellipsoids and the atom-numbering scheme. H-atoms are omitted for clarity.



Figure 2

The other molecule of the two independent molecules of the asymmetric unit(I), showing 10% probability displacement ellipsoids and the atom-numbering scheme. H-atoms are omitted for clarity.

(2*RS*,3*SR*,10*SR*,11*RS*)-3,10-Diphenoxy-18,21-dioxa-5,8- diazapentacyclo[20.4.0.0^{2,5}.0^{8,11}.0^{12,17}]hexacosa-1(26),12,14,16,22,24-hexaene-4,9-dione ethyl acetate hemisolvate

Crystal data	
$C_{34}H_{30}N_2O_6 \cdot 0.5(C_4H_8O_2)$	b = 17.201 (3) Å
$M_r = 606.65$	c = 21.589 (4) Å
Monoclinic, $P2_1/n$	$\beta = 108.722 \ (10)^{\circ}$
Hall symbol: -P 2yn	$V = 6343.67 (19) \text{ Å}^3$
a = 18.037 (3) Å	Z = 8

F(000) = 2560 $D_x = 1.270 \text{ Mg m}^{-3}$ Mo Ka radiation, $\lambda = 0.71075 \text{ Å}$ Cell parameters from 2500 reflections $\theta = 2-27^{\circ}$

Data collection

Buiu concention	
Bruker SMART APEX CCD	64493 measured reflections
diffractometer	13208 independent reflections
Radiation source: fine-focus sealed tube	7192 reflections with $I > 2\sigma(I)$
Graphite monochromator	$R_{\rm int} = 0.046$
ω scans	$\theta_{\rm max} = 26.6^\circ, \ \theta_{\rm min} = 1.7^\circ$
Absorption correction: multi-scan	$h = -22 \rightarrow 22$
(SADABS; Bruker, 1998)	$k = -21 \rightarrow 21$
$T_{\min} = 0.984, \ T_{\max} = 0.988$	$l = -27 \rightarrow 27$
Refinement	

 $\mu = 0.09 \text{ mm}^{-1}$

Block, colourless

 $0.18 \times 0.16 \times 0.13 \text{ mm}$

T = 293 K

Secondary atom site location: difference Fourier map Hydrogen site location: inferred from neighbouring sites H-atom parameters constrained $w = 1/[\sigma^2(F_o^2) + (0.0801P)^2 + 1.3813P]$ where $P = (F_o^2 + 2F_c^2)/3$ $(\Delta/\sigma)_{max} < 0.001$ $\Delta\rho_{max} = 0.32$ e Å⁻³ $\Delta\rho_{min} = -0.24$ e Å⁻³

Special details

Refinement on F^2

 $wR(F^2) = 0.175$

13208 reflections

direct methods

813 parameters 0 restraints

S = 1.02

Least-squares matrix: full

Primary atom site location: structure-invariant

 $R[F^2 > 2\sigma(F^2)] = 0.053$

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and	isotropic or e	quivalent isotropic	displacement	parameters ($(Å^2)$)
	1	1 1	1	1 1	\ <i>/</i>	

	x	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
01	0.58820 (10)	0.50849 (11)	0.49402 (8)	0.0675 (5)	
O2	0.46252 (10)	0.40807 (11)	0.76094 (9)	0.0678 (5)	
03	0.79089 (11)	0.27095 (10)	0.67869 (9)	0.0692 (5)	
04	0.68980 (10)	0.18393 (11)	0.72407 (9)	0.0723 (5)	
05	0.75451 (8)	0.41331 (10)	0.52020 (7)	0.0543 (4)	
06	0.54253 (9)	0.23356 (9)	0.79798 (7)	0.0546 (4)	
N1	0.53463 (10)	0.36778 (11)	0.69396 (9)	0.0482 (5)	
N2	0.62448 (10)	0.43556 (11)	0.59046 (8)	0.0477 (5)	
C1	0.53443 (14)	0.23039 (16)	0.85949 (11)	0.0579 (7)	
C2	0.50667 (17)	0.29204 (19)	0.88634 (13)	0.0738 (8)	
H2	0.4938	0.3387	0.8636	0.089*	
C3	0.49799 (19)	0.2840 (2)	0.94753 (15)	0.0934 (11)	

Н3	0.4790	0.3253	0.9658	0.112*
C4	0.5172 (2)	0.2159 (3)	0.98101 (16)	0.1071 (14)
H4	0.5124	0.2110	1.0225	0.129*
C5	0.5436 (2)	0.1545 (3)	0.95333 (17)	0.1107 (13)
Н5	0.5555	0.1078	0.9760	0.133*
C6	0.55309 (18)	0.16067 (19)	0.89231 (14)	0.0805 (9)
H6	0.5715	0.1190	0.8740	0.097*
C7	0.56993 (12)	0.30462 (13)	0.78045 (10)	0.0451 (5)
H7	0.6143	0.3252	0.8160	0.054*
C8	0.58797 (12)	0.30110 (13)	0.71428 (10)	0.0438 (5)
H8	0.6423	0.3153	0.7197	0.053*
C9	0.51115 (12)	0.36898 (14)	0.74746 (11)	0.0481 (6)
C10	0.56317 (14)	0.22914 (14)	0.67387 (10)	0.0501 (6)
C11	0.48777 (17)	0.2166 (2)	0.63373 (13)	0.0766 (8)
H11	0.4499	0.2545	0.6302	0.092*
C12	0.4673 (2)	0.1484 (3)	0.59849 (16)	0.1033 (12)
H12	0.4158	0.1405	0.5721	0.124*
C13	0.5221 (3)	0.0930 (2)	0.60227 (17)	0.1031 (12)
H13	0.5079	0.0477	0.5778	0.124*
C14	0.5990 (2)	0.10279 (18)	0.64218 (15)	0.0818 (9)
H14	0.6365	0.0649	0.6444	0.098*
C15	0.61848 (16)	0.17077 (15)	0.67866 (12)	0.0593 (6)
C16	0.75889 (17)	0.15158 (17)	0.71566 (17)	0.0795 (9)
H16A	0.7482	0.1332	0.6712	0.095*
H16B	0.7776	0.1082	0.7453	0.095*
C17	0.81814 (16)	0.21491 (17)	0.73031 (15)	0.0751 (8)
H17A	0.8231	0.2385	0.7722	0.090*
H17B	0.8688	0.1946	0.7317	0.090*
C18	0.81363 (13)	0.34669 (15)	0.69163 (10)	0.0488 (6)
C19	0.88309 (14)	0.36788 (17)	0.73889 (11)	0.0582 (7)
H19	0.9157	0.3301	0.7645	0.070*
C20	0.90333 (15)	0.4447 (2)	0.74750 (13)	0.0669 (8)
H20	0.9498	0.4589	0.7793	0.080*
C21	0.85609 (17)	0.50128 (18)	0.70996 (13)	0.0675 (7)
H21	0.8704	0.5534	0.7161	0.081*
C22	0.78640 (15)	0.47960 (15)	0.66253 (11)	0.0559 (6)
H22	0.7543	0.5177	0.6370	0.067*
C23	0.76414 (12)	0.40245 (13)	0.65274 (10)	0.0426 (5)
C24	0.68875 (12)	0.37855 (13)	0.60175 (10)	0.0439 (5)
H24	0.6725	0.3259	0.6090	0.053*
C25	0.68248 (12)	0.39336 (14)	0.52855 (10)	0.0466 (5)
H25	0.6570	0.3500	0.5002	0.056*
C26	0.62359 (12)	0.45784 (15)	0.53028 (10)	0.0482 (6)
C27	0.75411 (12)	0.42248 (14)	0.45610 (10)	0.0476 (5)
C28	0.81786 (15)	0.39355 (18)	0.44128 (12)	0.0685 (8)
H28	0.8577	0.3679	0.4730	0.082*
C29	0.82196 (16)	0.40302 (18)	0.37899 (13)	0.0721 (8)
H29	0.8649	0.3837	0.3690	0.087*

C30	0.76339 (15)	0.44063 (16)	0.33156 (12)	0.0611 (7)
H30	0.7662	0.4462	0.2895	0.073*
C31	0.70102 (14)	0.46967 (15)	0.34697 (11)	0.0546 (6)
H31	0.6615	0.4957	0.3152	0.066*
C32	0.69594 (13)	0.46082 (14)	0.40911 (11)	0.0507 (6)
H32	0.6532	0.4808	0.4190	0.061*
C33	0.58264 (13)	0.46822 (14)	0.63199 (11)	0.0504 (6)
H33A	0.5624	0.5188	0.6149	0.061*
H33B	0.6195	0.4760	0.6755	0.061*
C34	0.51501 (12)	0.41862(15)	0.63752(11)	0.0526(6)
H34A	0.4729	0.4528	0.6391	0.063*
H34R	0.4956	0.3871	0.5983	0.063*
07	0.08612 (10)	-0.03084(12)	0.50260 (9)	0.003
08	-0.02514(11)	0.05004(12) 0.08467(11)	0.30200(9) 0.77821(10)	0.0752(0)
00	0.02514(11) 0.27020(12)	0.00407(11) 0.22602(11)	0.77621(10) 0.67684(9)	0.0750(5)
010	0.27029(12) 0.18251(14)	0.22002(11) 0.31822(12)	0.07004(9)	0.0814(0) 0.0873(6)
010	0.10231(14) 0.23802(8)	0.31822(12) 0.08121(10)	0.73090(10) 0.51517(7)	0.0875(0)
012	0.23893(8) 0.05251(10)	0.08131(10) 0.25116(10)	0.31317(7)	0.0343(4)
012 N2	0.03331(10)	0.23110(10) 0.12280(12)	0.81092(8)	0.0634(3)
N3 N4	0.03988 (10)	0.12389 (12)	0.70555 (9)	0.0316(3)
N4	0.11/30 (10)	0.05203 (11)	0.59366 (8)	0.0495 (5)
C35	0.10/12 (19)	0.2903/(16)	0.86937 (13)	0.068/(/)
C36	0.0732 (3)	0.33826 (19)	0.90397 (16)	0.1016 (12)
H36	0.0191	0.3433	0.8925	0.122*
C37	0.1232 (4)	0.3788 (3)	0.9568 (2)	0.146 (2)
H37	0.1017	0.4126	0.9801	0.176*
C38	0.2030 (4)	0.3706 (3)	0.9758 (3)	0.158 (2)
H38	0.2352	0.3967	1.0123	0.190*
C39	0.2332 (3)	0.3238 (3)	0.9400 (2)	0.1273 (15)
H39	0.2873	0.3184	0.9520	0.153*
C40	0.1864 (2)	0.2834 (2)	0.88599 (16)	0.0918 (10)
H40	0.2087	0.2522	0.8616	0.110*
C41	0.08090 (14)	0.18611 (14)	0.79130 (11)	0.0506 (6)
H41	0.1279	0.1642	0.8232	0.061*
C42	0.09050 (13)	0.19243 (13)	0.72190 (11)	0.0471 (5)
H42	0.1441	0.1811	0.7228	0.057*
C43	0.02096 (14)	0.12327 (14)	0.76097 (11)	0.0521 (6)
C44	0.05858 (15)	0.26504 (16)	0.68418 (11)	0.0562 (6)
C45	-0.01947 (17)	0.2737 (2)	0.64774 (13)	0.0765 (9)
H45	-0.0540	0.2326	0.6448	0.092*
C46	-0.0471 (2)	0.3434 (3)	0.61535 (15)	0.1036 (14)
H46	-0.1000	0.3491	0.5921	0.124*
C47	0.0032 (3)	0.4026 (3)	0.61783 (17)	0.1100 (15)
H47	-0.0149	0.4479	0.5944	0.132*
C48	0.0809 (3)	0.39636 (19)	0.65468 (16)	0.1004 (12)
H48	0.1149	0.4377	0.6571	0.120*
C49	0.1083 (2)	0.32766 (17)	0.68836(13)	0.0713 (8)
C50	0.2471 (2)	0.34862 (19)	0.71346 (19)	0.0998 (11)
H50A	0.2698	0.3930	0.7406	0.120*

H50B	0.2299	0.3650	0.6681	0.120*
C51	0.3058 (2)	0.2846 (2)	0.72398 (17)	0.0935 (10)
H51A	0.3535	0.3034	0.7177	0.112*
H51B	0.3184	0.2640	0.7680	0.112*
C52	0.30210 (13)	0.15310 (15)	0.68510(11)	0.0536 (6)
C53	0.37626 (15)	0.1362 (2)	0.72771 (13)	0.0705 (8)
H53	0.4073	0.1757	0.7522	0.085*
C54	0.40356 (16)	0.0618 (2)	0.73372 (14)	0.0803 (9)
H54	0.4531	0.0508	0.7625	0.096*
C55	0.35892 (18)	0.0031 (2)	0.69790 (13)	0.0774 (9)
Н55	0.3780	-0.0476	0.7020	0.093*
C56	0.28482 (15)	0.01966 (16)	0.65534 (11)	0.0592 (6)
H56	0.2542	-0.0204	0.6313	0.071*
C57	0.2512 0.25554(12)	0.09451(13)	0.64801(10)	0.071 0.0427(5)
C58	0.17667(12)	0.11307(13)	0.59957 (10)	0.0436(5)
U50 H58	0.1580	0.1652	0.6055	0.052*
C50	0.1530 0.16737(12)	0.1052 0.00423(14)	0.0055	0.032
U50	0.10737(12) 0.1360	0.09423 (14)	0.32033 (10)	0.0474(3)
C60	0.1300	0.1336 0.02564(16)	0.4909	0.057°
C00	0.11048(13)	0.02304(10)	0.35438(11) 0.45046(10)	0.0322(0)
C01	0.23011(12)	0.07508 (14)	0.43046 (10)	0.0461(5)
C62	0.29/14 (10)	0.10742 (19)	0.45459 (15)	0.0752 (9)
H62	0.3367	0.1339	0.4658	0.090*
C63	0.29951 (17)	0.10048 (19)	0.37165 (13)	0.0788 (9)
H63	0.3409	0.1225	0.3609	0.095*
C64	0.24212 (15)	0.06174 (15)	0.32478 (11)	0.0571 (6)
H64	0.2443	0.0574	0.2825	0.069*
C65	0.18145 (14)	0.02940 (14)	0.34073 (11)	0.0516 (6)
H65	0.1422	0.0028	0.3092	0.062*
C66	0.17816 (13)	0.03615 (14)	0.40402 (10)	0.0489 (6)
H66	0.1367	0.0143	0.4147	0.059*
C67	0.08087 (14)	0.02224 (15)	0.63947 (12)	0.0567 (6)
H67A	0.1210	0.0153	0.6815	0.068*
H67B	0.0591	-0.0286	0.6246	0.068*
C68	0.01636 (13)	0.07316 (17)	0.64897 (12)	0.0628 (7)
H68A	-0.0050	0.1049	0.6101	0.075*
H68B	-0.0253	0.0397	0.6526	0.075*
013	0.64589 (13)	0.69087 (14)	0.51650(12)	0.1002 (7)
014	0.67151 (18)	0.64668 (18)	0.61737 (13)	0.1269 (9)
C69	0.5398 (2)	0.6845 (2)	0.5557 (2)	0.1183 (13)
H69A	0.5112	0.6431	0.5285	0.178*
H69B	0.5238	0 7333	0 5340	0.178*
H69C	0.5293	0.6843	0 5965	0.178*
C70	0.6249(2)	0.6732(2)	0.56792 (18)	0.0894(10)
C71	0.0215(2)	0.6741(3)	0.5274(2)	0.1394(17)
H71A	0.7626	0.0791 (3)	0.522 + (2)	0.157*(17)
H71R	0.7394	0.7057	0.5333	0.167*
C72	0.7356(3)	0.6176	0.3333 0.4603(3)	0.107 0.187(3)
U72	0.7550 (5)	0.0917 (4)	0.4069 (5)	0.10/(3)
11/2A	0.07/7	0.0023	0.4200	0.200

supporting information

H72B	0.7874	0.6782	0.4607	0.280*
H72C	0.7270	0.7463	0.4515	0.280*

Atomic displacement parameters $(Å^2)$

	U^{11}	<i>U</i> ²²	<i>U</i> ³³	U^{12}	U^{13}	<i>U</i> ²³
01	0.0629 (10)	0.0937 (14)	0.0532 (10)	0.0301 (10)	0.0288 (8)	0.0327 (10)
O2	0.0679 (11)	0.0809 (13)	0.0716 (12)	0.0114 (10)	0.0459 (10)	0.0080 (10)
O3	0.0805 (12)	0.0558 (12)	0.0588 (11)	0.0143 (10)	0.0050 (9)	0.0102 (9)
O4	0.0673 (11)	0.0669 (12)	0.0752 (13)	0.0155 (9)	0.0121 (10)	-0.0115 (10)
05	0.0451 (8)	0.0895 (12)	0.0327 (8)	0.0076 (8)	0.0188 (7)	0.0068 (8)
O6	0.0673 (10)	0.0610 (10)	0.0375 (8)	-0.0207 (8)	0.0196 (7)	0.0042 (7)
N1	0.0469 (10)	0.0603 (12)	0.0444 (11)	0.0092 (9)	0.0243 (8)	0.0148 (9)
N2	0.0472 (10)	0.0637 (12)	0.0382 (10)	0.0142 (9)	0.0219 (8)	0.0149 (9)
C1	0.0575 (14)	0.0792 (19)	0.0360 (13)	-0.0279 (13)	0.0135 (11)	0.0048 (13)
C2	0.0846 (19)	0.093 (2)	0.0494 (16)	-0.0148 (17)	0.0288 (14)	0.0006 (15)
C3	0.103 (2)	0.133 (3)	0.0557 (19)	-0.039 (2)	0.0420 (17)	-0.010 (2)
C4	0.121 (3)	0.161 (4)	0.0485 (19)	-0.064 (3)	0.0388 (19)	0.002 (2)
C5	0.145 (3)	0.122 (3)	0.065 (2)	-0.044 (3)	0.033 (2)	0.030 (2)
C6	0.099 (2)	0.083 (2)	0.0595 (18)	-0.0216 (18)	0.0262 (16)	0.0180 (16)
C7	0.0476 (12)	0.0528 (14)	0.0373 (12)	-0.0109 (11)	0.0171 (9)	0.0042 (10)
C8	0.0429 (11)	0.0527 (14)	0.0388 (12)	0.0010 (10)	0.0173 (9)	0.0097 (10)
C9	0.0450 (12)	0.0607 (15)	0.0455 (13)	-0.0054 (11)	0.0242 (10)	0.0057 (11)
C10	0.0571 (14)	0.0587 (15)	0.0357 (12)	-0.0058 (12)	0.0168 (10)	0.0061 (11)
C11	0.0685 (17)	0.097 (2)	0.0555 (17)	-0.0120 (16)	0.0076 (14)	-0.0075 (16)
C12	0.102 (3)	0.122 (3)	0.065 (2)	-0.032 (3)	-0.0015 (18)	-0.015 (2)
C13	0.146 (4)	0.083 (3)	0.068 (2)	-0.034 (3)	0.016 (2)	-0.0200 (19)
C14	0.118 (3)	0.0595 (19)	0.0642 (19)	-0.0030 (18)	0.0242 (18)	-0.0039 (15)
C15	0.0758 (17)	0.0550 (16)	0.0455 (14)	-0.0040 (14)	0.0169 (13)	0.0033 (12)
C16	0.083 (2)	0.0571 (18)	0.100 (2)	0.0284 (16)	0.0317 (17)	0.0122 (16)
C17	0.0671 (17)	0.0720 (19)	0.081 (2)	0.0288 (16)	0.0170 (15)	0.0269 (16)
C18	0.0508 (13)	0.0615 (16)	0.0386 (12)	0.0093 (12)	0.0209 (10)	0.0029 (11)
C19	0.0480 (13)	0.085 (2)	0.0441 (14)	0.0124 (13)	0.0180 (11)	0.0007 (13)
C20	0.0535 (15)	0.104 (2)	0.0479 (15)	-0.0090 (16)	0.0226 (12)	-0.0068 (15)
C21	0.0807 (19)	0.0758 (19)	0.0549 (16)	-0.0181 (16)	0.0343 (15)	-0.0066 (15)
C22	0.0660 (15)	0.0625 (17)	0.0456 (14)	0.0029 (13)	0.0268 (12)	0.0063 (12)
C23	0.0492 (12)	0.0527 (14)	0.0335 (11)	0.0052 (11)	0.0237 (10)	0.0066 (10)
C24	0.0487 (12)	0.0501 (13)	0.0368 (12)	0.0055 (10)	0.0193 (10)	0.0067 (10)
C25	0.0458 (12)	0.0620 (15)	0.0340 (11)	0.0037 (11)	0.0157 (9)	0.0049 (10)
C26	0.0426 (12)	0.0682 (16)	0.0375 (12)	0.0073 (11)	0.0182 (10)	0.0117 (11)
C27	0.0485 (12)	0.0650 (15)	0.0334 (12)	-0.0013 (11)	0.0191 (10)	0.0009 (11)
C28	0.0596 (15)	0.105 (2)	0.0479 (15)	0.0214 (15)	0.0276 (12)	0.0132 (14)
C29	0.0701 (17)	0.102 (2)	0.0581 (17)	0.0154 (16)	0.0402 (14)	0.0052 (15)
C30	0.0754 (17)	0.0769 (18)	0.0411 (14)	-0.0081 (14)	0.0327 (13)	0.0011 (13)
C31	0.0622 (15)	0.0638 (16)	0.0398 (13)	-0.0039 (12)	0.0193 (11)	0.0055 (11)
C32	0.0508 (13)	0.0649 (16)	0.0410 (13)	0.0046 (12)	0.0211 (10)	0.0044 (11)
C33	0.0545 (13)	0.0589 (15)	0.0471 (13)	0.0135 (11)	0.0293 (11)	0.0126 (11)
C34	0.0445 (12)	0.0699 (16)	0.0481 (13)	0.0143 (11)	0.0216 (10)	0.0211 (12)

07	0.0749 (12)	0.0944 (14)	0.0594 (11)	-0.0356 (11)	0.0341 (9)	-0.0355 (10)
08	0.0878 (13)	0.0758 (13)	0.0845 (14)	-0.0058 (11)	0.0600 (11)	-0.0011 (10)
09	0.0924 (14)	0.0577 (13)	0.0716 (13)	-0.0242 (11)	-0.0050 (10)	-0.0041 (10)
O10	0.1087 (16)	0.0700 (13)	0.0707 (14)	-0.0264 (12)	0.0113 (12)	0.0074 (11)
011	0.0440 (8)	0.0917 (13)	0.0311 (8)	-0.0079 (8)	0.0167 (6)	-0.0012 (8)
012	0.0800 (11)	0.0635 (11)	0.0474 (10)	0.0159 (9)	0.0216 (9)	-0.0108 (8)
N3	0.0498 (11)	0.0667 (13)	0.0455 (11)	-0.0117 (10)	0.0253 (9)	-0.0141 (9)
N4	0.0491 (10)	0.0665 (13)	0.0386 (10)	-0.0179 (9)	0.0223 (8)	-0.0150 (9)
C35	0.103 (2)	0.0580 (17)	0.0463 (15)	-0.0021 (16)	0.0264 (15)	0.0010 (13)
C36	0.167 (3)	0.077 (2)	0.073 (2)	0.003 (2)	0.057 (2)	-0.0237 (18)
C37	0.249 (6)	0.098 (3)	0.100 (4)	-0.018 (4)	0.066 (4)	-0.048 (3)
C38	0.229 (7)	0.122 (4)	0.094 (4)	-0.050 (5)	0.012 (4)	-0.036 (3)
C39	0.138 (4)	0.112 (3)	0.104 (3)	-0.036 (3)	0.000 (3)	-0.011 (3)
C40	0.104 (3)	0.084 (2)	0.075 (2)	-0.008(2)	0.0113 (19)	-0.0140 (18)
C41	0.0604 (14)	0.0524 (14)	0.0397 (13)	0.0122 (11)	0.0171 (11)	-0.0046 (11)
C42	0.0459 (12)	0.0529 (14)	0.0460 (13)	0.0001 (11)	0.0196 (10)	-0.0070 (11)
C43	0.0567 (14)	0.0582 (15)	0.0508 (14)	0.0069 (12)	0.0304 (11)	-0.0009 (11)
C44	0.0662 (16)	0.0708 (18)	0.0381 (13)	0.0129 (14)	0.0256 (11)	-0.0018(12)
C45	0.0727 (18)	0.117 (3)	0.0509 (16)	0.0300 (18)	0.0350 (14)	0.0157 (16)
C46	0.113 (3)	0.161 (4)	0.0489 (18)	0.076 (3)	0.0432 (19)	0.030 (2)
C47	0.184 (5)	0.101 (3)	0.053 (2)	0.066 (3)	0.048 (3)	0.018 (2)
C48	0.183 (4)	0.055 (2)	0.058 (2)	0.014 (2)	0.032 (2)	0.0022 (16)
C49	0.107 (2)	0.0581 (18)	0.0475 (16)	0.0031 (17)	0.0233 (16)	-0.0022(13)
C50	0.130 (3)	0.061 (2)	0.105 (3)	-0.048(2)	0.034 (2)	-0.0126 (19)
C51	0.097 (2)	0.073 (2)	0.097 (3)	-0.045 (2)	0.0135 (19)	-0.0191 (19)
C52	0.0526 (14)	0.0641 (17)	0.0454 (14)	-0.0168 (12)	0.0172 (11)	0.0019 (12)
C53	0.0490 (15)	0.107 (3)	0.0533 (16)	-0.0250 (16)	0.0127 (12)	-0.0007 (16)
C54	0.0500 (16)	0.137 (3)	0.0536 (17)	0.0135 (19)	0.0158 (13)	0.0057 (19)
C55	0.084 (2)	0.101 (2)	0.0478 (16)	0.0341 (19)	0.0209 (15)	0.0052 (16)
C56	0.0702 (16)	0.0669 (18)	0.0413 (13)	0.0053 (13)	0.0189 (12)	-0.0057 (12)
C57	0.0461 (12)	0.0563 (15)	0.0304 (11)	-0.0085 (11)	0.0188 (9)	-0.0011 (10)
C58	0.0445 (12)	0.0527 (14)	0.0359 (11)	-0.0063(10)	0.0163 (9)	-0.0038(10)
C59	0.0430 (12)	0.0665 (16)	0.0340 (12)	-0.0027(11)	0.0143 (9)	-0.0018(11)
C60	0.0435 (12)	0.0775 (18)	0.0381 (12)	-0.0106(12)	0.0167 (10)	-0.0148(12)
C61	0.0471 (12)	0.0612 (15)	0.0330 (11)	-0.0030(11)	0.0169 (10)	0.0027 (10)
C62	0.0686 (17)	0.114 (2)	0.0489 (15)	-0.0386(17)	0.0273 (13)	-0.0134(15)
C63	0.0793 (19)	0.116 (3)	0.0559 (17)	-0.0335(18)	0.0419 (15)	-0.0120(16)
C64	0.0710 (16)	0.0698 (17)	0.0387 (13)	0.0068 (13)	0.0291 (12)	0.0011 (12)
C65	0.0555 (13)	0.0596 (15)	0.0407 (13)	0.0043 (12)	0.0171 (10)	-0.0047(11)
C66	0.0466 (12)	0.0619 (15)	0.0415 (13)	-0.0039(11)	0.0188 (10)	0.0009 (11)
C67	0.0663(15)	0.0621(16)	0.0539(14)	-0.0193(12)	0.0365(12)	-0.0153(12)
C68	0.0493(13)	0.091(2)	0.0537(15)	-0.0201(13)	0.0249(11)	-0.0268(14)
013	0.0974 (16)	0.091(2) 0.1138(19)	0.0950(17)	0.0201(13)	0.0219(11) 0.0389(13)	0.0200(11) 0.0220(14)
014	0.144 (2)	0.143 (3)	0.0833 (18)	0.0065 (19)	0.0226 (17)	0.0098(17)
C69	0 123 (3)	0 116 (3)	0 137 (4)	0.025 (3)	0.071 (3)	0.013(3)
C70	0.117(3)	0.080(2)	0.073(2)	-0.003(2)	0.032(2)	0.013(3)
C71	0.096 (3)	0.000(2) 0.187(5)	0.075(2)	0.003(2)	0.052(2)	0.046(4)
C72	0.090(3)	0.107(3)	0.190 (6)	0.013(3)	0.090(3)	0.040(4)
012	0.157 (+)	0.201 (7)	0.170 (0)	(ד) 110.0	(ד) דעטיט	0.000 (3)

Geometric parameters (Å, °)

01—C26	1.208 (3)	O11—C59	1.407 (2)	
O2—C9	1.213 (3)	O12—C35	1.403 (3)	
O3—C18	1.368 (3)	O12—C41	1.406 (3)	
O3—C17	1.436 (3)	N3—C43	1.350 (3)	
O4—C15	1.363 (3)	N3—C68	1.446 (3)	
O4—C16	1.428 (3)	N3—C42	1.463 (3)	
O5—C27	1.390 (2)	N4—C60	1.349 (3)	
O5—C25	1.410 (2)	N4—C67	1.446 (3)	
O6—C1	1.383 (3)	N4—C58	1.476 (3)	
O6—C7	1.415 (2)	C35—C40	1.364 (4)	
N1—C9	1.352 (3)	C35—C36	1.380 (4)	
N1—C34	1.448 (3)	C36—C37	1.394 (6)	
N1—C8	1.471 (3)	C36—H36	0.9300	
N2—C26	1.350 (3)	C37—C38	1.370 (7)	
N2-C33	1.457 (3)	С37—Н37	0.9300	
N2-C24	1.478 (3)	C38—C39	1.346 (7)	
C1—C2	1.377 (4)	C38—H38	0.9300	
C1—C6	1.379 (4)	C39—C40	1.387 (5)	
C2—C3	1.386 (4)	С39—Н39	0.9300	
C2—H2	0.9300	C40—H40	0.9300	
C3—C4	1.362 (5)	C41—C43	1.520 (3)	
С3—Н3	0.9300	C41—C42	1.566 (3)	
C4—C5	1.373 (5)	C41—H41	0.9800	
C4—H4	0.9300	C42—C44	1.501 (3)	
C5—C6	1.386 (4)	C42—H42	0.9800	
С5—Н5	0.9300	C44—C45	1.383 (4)	
С6—Н6	0.9300	C44—C49	1.385 (4)	
С7—С9	1.540 (3)	C45—C46	1.397 (5)	
C7—C8	1.565 (3)	C45—H45	0.9300	
С7—Н7	0.9800	C46—C47	1.355 (6)	
C8—C10	1.498 (3)	C46—H46	0.9300	
С8—Н8	0.9800	C47—C48	1.375 (6)	
C10—C11	1.375 (3)	C47—H47	0.9300	
C10—C15	1.396 (3)	C48—C49	1.392 (4)	
C11—C12	1.382 (5)	C48—H48	0.9300	
C11—H11	0.9300	C50—C51	1.493 (5)	
C12—C13	1.355 (5)	C50—H50A	0.9700	
C12—H12	0.9300	C50—H50B	0.9700	
C13—C14	1.389 (5)	C51—H51A	0.9700	
С13—Н13	0.9300	C51—H51B	0.9700	
C14—C15	1.390 (4)	C52—C53	1.389 (4)	
C14—H14	0.9300	C52—C57	1.389 (3)	
C16—C17	1.487 (4)	C53—C54	1.363 (4)	
C16—H16A	0.9700	С53—Н53	0.9300	
C16—H16B	0.9700	C54—C55	1.366 (4)	
C17—H17A	0.9700	C54—H54	0.9300	

C17 U17D	0.0700	055 056	1 207 (4)
	0.9700	C55—C56	1.387 (4)
C18—C19	1.387 (3)	C55—H55	0.9300
C18—C23	1.393 (3)	C56—C57	1.381 (3)
C19—C20	1.368 (4)	С56—Н56	0.9300
С19—Н19	0.9300	C57—C58	1.505 (3)
C20—C21	1.373 (4)	C58—C59	1.565 (3)
C20—H20	0.9300	С58—Н58	0.9800
C21—C22	1.393 (4)	C59—C60	1.538 (3)
C21—H21	0.9300	С59—Н59	0.9800
C22—C23	1.383 (3)	C61—C66	1.369 (3)
С22—Н22	0.9300	C61—C62	1.374 (3)
C23—C24	1.506 (3)	C62—C63	1.374 (3)
C24—C25	1.569 (3)	C62—H62	0.9300
C24—H24	0.9800	C63—C64	1.366 (4)
C25—C26	1.544 (3)	С63—Н63	0.9300
C25—H25	0.9800	C64—C65	1 367 (3)
C_{27} C	1 372 (3)	C64—H64	0.9300
C_{27} C_{32}	1.372(3)	C65C66	1 391 (3)
C_{2}^{2}	1.382(3)	C65 H65	0.0300
C_{20} C_{29} C	0.0300	C66 H66	0.9300
C20—F120	0.9300	C67 - C68	0.9300
$C_{29} = C_{30}$	1.374 (4)	C(7 - U(7))	1.322 (3)
C29—H29	0.9500	$C_0/-H_0/A$	0.9700
C30—C31	1.366 (3)	C6/—H6/B	0.9700
C30—H30	0.9300	C68—H68A	0.9700
C31—C32	1.382 (3)	C68—H68B	0.9700
C31—H31	0.9300	O13—C70	1.319 (4)
С32—Н32	0.9300	O13—C71	1.464 (4)
C33—C34	1.524 (3)	O14—C70	1.216 (4)
C33—H33A	0.9700	C69—C70	1.484 (5)
С33—Н33В	0.9700	C69—H69A	0.9600
C34—H34A	0.9700	С69—Н69В	0.9600
C34—H34B	0.9700	С69—Н69С	0.9600
O7—C60	1.216 (3)	C71—C72	1.428 (6)
O8—C43	1.212 (3)	C71—H71A	0.9700
O9—C52	1.367 (3)	C71—H71B	0.9700
O9—C51	1.429 (3)	С72—Н72А	0.9600
O10—C49	1.369 (4)	С72—Н72В	0.9600
Q10—C50	1,434 (4)	С72—Н72С	0.9600
011-C61	1 386 (2)	0/2 11/20	0.0000
	1.500 (2)		
C18—O3—C17	118 4 (2)	C40-C35-O12	124 3 (3)
$C_{15} - O_{4} - C_{16}$	120 3 (2)	$C_{36} - C_{35} - O_{12}$	1144(3)
$C_{27} - C_{25}$	116 36 (16)	C_{35} C_{35} $-C_{12}$ C_{35} $-C_{37}$	1173(<i>A</i>)
$C_{2} = -05 = -025$	116.00 (10)	$C_{35} = C_{30} = C_{37}$	121.2 (4)
$C_1 = 0_0 = 0_1$	110.40(10) 120.60(10)	$C_{33} = C_{30} = H_{30}$	121.3
$C_{2} = 101 = 0.54$	150.00(19)	$C_{2}^{2} = C_{2}^{2} = C_{2}^{2}$	121.3
$C_{24} = 0$	90.39 (10) 122 OC (17)	$C_{20} = C_{27} = U_{27}$	122.3 (3)
C_{34} N1 C_{32}	132.96 (17)	$C_{3\delta}$ C_{37} H_{37}	118.8
C26—N2—C33	129.37 (19)	C36—C37—H37	118.8

C26—N2—C24	96.51 (16)	C39—C38—C37	118.0 (5)
C33—N2—C24	133.49 (17)	С39—С38—Н38	121.0
$C_{2}-C_{1}-C_{6}$	121.0 (2)	С37—С38—Н38	121.0
$C_{2}-C_{1}-C_{6}$	122.6 (2)	C_{38} C_{39} C_{40}	122.2 (5)
C6-C1-O6	1164(3)	C38—C39—H39	118.9
C1 - C2 - C3	119 5 (3)	C40-C39-H39	118.9
C1 - C2 - H2	120.3	C_{35} C_{40} C_{39}	118.7 (4)
$C_3 - C_2 - H_2$	120.3	$C_{35} - C_{40} - H_{40}$	120.6
C_{4} C_{3} C_{2} C_{2}	120.3 (4)	C_{39} C_{40} H_{40}	120.6
$C_4 - C_3 - H_3$	119.9	012-C41-C43	116 36 (19)
C2_C3_H3	119.9	012 - C41 - C42	118 80 (19)
$C_{2} = C_{3} = C_{4} = C_{5}$	119.7 (3)	C_{43} C_{41} C_{42}	85 36 (16)
$C_3 - C_4 - H_4$	120.1	012-C41-H41	111.3
C5_C4_H4	120.1	C_{43} C_{41} H_{41}	111.5
C_{4} C_{5} C_{6}	120.1 121.4(A)	C42 - C41 - H41	111.5
$C_4 = C_5 = H_5$	110.3	$C_{+2} = C_{+1} = \Pi_{+1}$	111.5 115.9(2)
C4 C5 H5	119.3	$N_{3} = C_{42} = C_{44}$	85 74 (16)
$C_0 = C_3 = H_3$	119.5	$N_{3} = C_{42} = C_{41}$	33.74(10)
$C_1 = C_0 = C_3$	110.1 (3)	$V_{44} = V_{42} = V_{41}$	112.05 (10)
$C_1 = C_0 = H_0$	121.0	$N_{3} = C_{42} = 1142$	112.3
C_{3} C_{0} C_{1} C_{0}	121.0 110.80(17)	$C_{44} - C_{42} - H_{42}$	112.5
06 67 68	113.00(17) 112.91(19)	$C_{41} - C_{42} - 1142$	112.3 132.2(2)
00-07-08	115.01(10) 95.20(15)	$0^{\circ} - C^{43} - N^{\circ}$	132.2(2)
$C_{9} - C_{7} - C_{8}$	65.59 (15) 111 9	$V_{0} = C_{43} = C_{41}$	130.1(2)
$O_0 - C_1 - H_1$	111.8	$N_{3} = C_{43} = C_{41}$	91.09(17)
C9-C7-H7	111.8	C45 - C44 - C49	118.2(3)
$C_8 - C_7 - H_7$	111.8	C43 - C44 - C42	122.8 (3)
NI = C8 = C10	115.24 (18)	C49 - C44 - C42	119.0 (2)
NI = C8 = C7	86.23 (15)	C44 - C45 - C46	120.8 (3)
	116.93 (17)	C44—C45—H45	119.6
NI = C8 = H8	112.0	C46—C45—H45	119.6
C10 - C8 - H8	112.0	C47 - C46 - C45	119.9 (4)
C/-C8-H8	112.0	C47—C46—H46	120.0
02—C9—N1	131.5 (2)	C45—C46—H46	120.0
02-09-07	137.0 (2)	C46—C47—C48	120.6 (4)
N1—C9—C7	91.51 (17)	C46—C47—H47	119.7
C11—C10—C15	118.2 (3)	C48—C47—H47	119.7
C11—C10—C8	123.2 (2)	C47—C48—C49	119.5 (4)
C15—C10—C8	118.6 (2)	С47—С48—Н48	120.2
C10—C11—C12	121.1 (3)	C49—C48—H48	120.2
С10—С11—Н11	119.5	010	115.1 (2)
C12—C11—H11	119.5	010	123.9 (3)
C13—C12—C11	120.2 (3)	C44—C49—C48	120.8 (3)
C13—C12—H12	119.9	010	106.7 (3)
C11—C12—H12	119.9	010—C50—H50A	110.4
C12—C13—C14	121.1 (3)	C51—C50—H50A	110.4
C12—C13—H13	119.5	010—C50—H50B	110.4
C14—C13—H13	119.5	C51—C50—H50B	110.4
C13—C14—C15	118.3 (3)	H50A—C50—H50B	108.6

C13—C14—H14	120.9	O9—C51—C50	106.1 (3)
C15—C14—H14	120.9	O9—C51—H51A	110.5
O4—C15—C14	123.7 (3)	C50—C51—H51A	110.5
O4—C15—C10	114.9 (2)	O9—C51—H51B	110.5
C14—C15—C10	121.2 (3)	C50—C51—H51B	110.5
O4—C16—C17	106.5 (2)	H51A—C51—H51B	108.7
O4—C16—H16A	110.4	O9—C52—C53	123.6 (2)
C17—C16—H16A	110.4	O9—C52—C57	116.1 (2)
O4—C16—H16B	110.4	C53—C52—C57	120.4(3)
C17—C16—H16B	110.4	C54—C53—C52	120.1(3)
H16A—C16—H16B	108.6	C54—C53—H53	120.0
03-C17-C16	106.4(2)	C52—C53—H53	120.0
O_3 C_{17} H_{17A}	110.4	$C_{52} = C_{53} = H_{55}$	120.0 120.7(3)
C16-C17-H17A	110.4	$C_{53} - C_{54} - H_{54}$	120.7 (3)
$O_3 C_{17} H_{17R}$	110.4	C55 C54 H54	119.6
C16 C17 H17B	110.4	$C_{55} - C_{54} - C_{55} - C_{56}$	119.0
1174 177 $117D$	109.4	$C_{54} = C_{55} = C_{50}$	119.4 (5)
HI/A - CI/-HI/B	108.0	С54—С55—П55	120.3
03 - 018 - 012	122.8(2)	С50—С55—Н55	120.3
03-018-023	116.1 (2)	$C_{5}/-C_{5}$	121.3 (3)
C19 - C18 - C23	121.0 (2)	С57—С56—Н56	119.3
C20—C19—C18	119.5 (3)	С55—С56—Н56	119.4
С20—С19—Н19	120.2	C56—C57—C52	118.2 (2)
C18—C19—H19	120.2	C56—C57—C58	121.3 (2)
C19—C20—C21	121.1 (3)	C52—C57—C58	120.6 (2)
С19—С20—Н20	119.5	N4—C58—C57	114.02 (18)
C21—C20—H20	119.5	N4—C58—C59	85.72 (15)
C20—C21—C22	119.1 (3)	C57—C58—C59	115.33 (17)
C20—C21—H21	120.4	N4—C58—H58	113.0
C22—C21—H21	120.4	С57—С58—Н58	113.0
C23—C22—C21	121.2 (2)	С59—С58—Н58	113.0
C23—C22—H22	119.4	O11—C59—C60	120.8 (2)
C21—C22—H22	119.4	O11—C59—C58	113.64 (17)
C22—C23—C18	118.0 (2)	C60—C59—C58	85.43 (15)
C22—C23—C24	121.6 (2)	О11—С59—Н59	111.5
C18—C23—C24	120.4 (2)	С60—С59—Н59	111.5
N2—C24—C23	114.57 (18)	С58—С59—Н59	111.5
N2-C24-C25	85.82 (15)	07—C60—N4	132.2 (2)
C_{23} C_{24} C_{25}	11663(17)	07-C60-C59	1365(2)
N2-C24-H24	112.4	N4—C60—C59	91 30 (18)
C_{23} C_{24} H_{24}	112.4	C_{66} C_{61} C_{62}	1199(2)
$C_{25} = C_{24} = H_{24}$	112.1	$C_{66} = C_{61} = 011$	123.28(18)
05-025-024	110.82 (10)	C62 - C61 - 011	125.20(10) 116.8(2)
05 - C25 - C25	113 38 (17)	C61 - C62 - C63	110.0(2) 119.7(2)
$C_{25} = C_{25} = C_{24}$	85 41 (15)	C61 - C62 - C63	120.2
05 025 125	111.0	C_{62} C_{62} H_{62}	120.2
$C_{23} = C_{23} = H_{23}$	111.7	C64 C63 C62	120.2
$C_{20} = C_{23} = \Pi_{23}$	111.9	C64 C63 H63	121.1(2)
C_{24} C_{23} Π_{23}	111.9	C(2) = C(2) = H(2)	119.4
UI-U20-IN2	132.0 (2)	C02-C03-H03	119.4

O1—C26—C25	136.64 (19)	C63—C64—C65	119.3 (2)
N2—C26—C25	91.35 (17)	С63—С64—Н64	120.3
C32—C27—C28	119.9 (2)	С65—С64—Н64	120.3
C32—C27—O5	123.30 (19)	C64—C65—C66	120.2 (2)
C28—C27—O5	116.8 (2)	С64—С65—Н65	119.9
C29—C28—C27	119.5 (2)	С66—С65—Н65	119.9
C29—C28—H28	120.3	C61—C66—C65	119.8 (2)
С27—С28—Н28	120.3	С61—С66—Н66	120.1
C30—C29—C28	120.9 (2)	С65—С66—Н66	120.1
С30—С29—Н29	119.6	N4—C67—C68	115.0 (2)
С28—С29—Н29	119.6	N4—C67—H67A	108.5
C31—C30—C29	119.1 (2)	С68—С67—Н67А	108.5
C31—C30—H30	120.4	N4—C67—H67B	108.5
C29—C30—H30	120.4	C68—C67—H67B	108.5
C_{30} $-C_{31}$ $-C_{32}$	120.8 (2)	H67A—C67—H67B	107.5
C_{30} C_{31} H_{31}	119.6	N3—C68—C67	1155(2)
C_{32} C_{31} H_{31}	119.6	N3—C68—H68A	108.4
$C_{27} - C_{32} - C_{31}$	119.8 (2)	C67 - C68 - H68A	108.4
$C_{27} = C_{32} = H_{32}$	120.1	N3-C68-H68B	108.4
$C_{31} = C_{32} = H_{32}$	120.1	C67 - C68 - H68B	108.4
$N_2 - C_{33} - C_{34}$	1120.1 114.7(2)	H68A - C68 - H68B	107.5
N2_C33_H33A	108.6	C70-013-C71	107.5 115.7(3)
C_{34} C_{33} H_{33A}	108.6	C70-C69-H69A	109.5
N2_C33_H33B	108.6	C70 - C69 - H69R	109.5
C34—C33—H33B	108.6	H69A - C69 - H69B	109.5
H33A_C33_H33B	107.6	C70 - C69 - H69C	109.5
N1_C34_C33	114 73 (18)	H69A - C69 - H69C	109.5
N1 C34 H34A	108.6	H60B C60 H60C	109.5
C_{33} C_{34} H_{34A}	108.6	014-070-013	107.5 121 4 (4)
N1_C34_H34B	108.6	014 - C70 - C69	121.4(4) 126.2(4)
C_{33} C_{34} H_{34B}	108.6	013 - C70 - C69	120.2(4) 1123(3)
H34A_C34_H34B	107.6	C72 - C71 - 013	112.3(3)
$C_{52} = 00 = C_{51}$	107.0 118.7(2)	C72 C71 H71A	110.2 (4)
$C_{32} = 0^{-1} = 0^{-1}$	118.7(2)	$O_{12} = C_{11} = H_{11} A$	110.5
$C_{4}^{61} = 010 - 050$	116.9(2) 116.70(16)	C72 $C71$ $H71B$	110.5
$C_{35} = 012 = C_{41}$	117.5(2)	$C_{12} = C_{11} = H_{11} = H_{11}$	110.5
$C_{33} = 012 = 041$	117.5(2) 130.9(2)	H71A C71 H71B	108.7
$C_{+3} = 113 = C_{00}$	150.9(2)	$\Gamma \Gamma $	100.7
C43 - 103 - C42	30.04(17) 133.00(18)	C71 C72 H72R	109.5
C60 NA C67	133.09(18) 131.1(2)	$H_{72A} = C_{72} = H_{72B}$	109.5
C60 N4 C58	151.1(2) 06.23(16)	11/2A = C/2 = 11/2B	109.5
C67 N4 C58	90.23(10) 132.03(17)	$H_{1} = C_{12} = H_{12} = H_$	109.5
$C_{0} = 104 - C_{3} = 0.000$	132.03(17) 121.2(2)	$H_{2}^{2} = C_{2}^{2} = H_{2}^{2} C_{2}^{2}$	109.5
C40—C33—C30	121.3 (3)	$\Pi/2D - C/2 - \Pi/2C$	109.5
C7—O6—C1—C2	39.0 (3)	C40—C35—C36—C37	-0.4 (5)
C7—O6—C1—C6	-143.2 (2)	O12—C35—C36—C37	179.8 (3)
C6—C1—C2—C3	0.5 (4)	C35—C36—C37—C38	-1.9 (7)
O6—C1—C2—C3	178.2 (2)	C36—C37—C38—C39	2.6 (9)

C1—C2—C3—C4	0.4 (5)	C37—C38—C39—C40	-1.0(8)
C2—C3—C4—C5	-1.4 (5)	C36—C35—C40—C39	1.9 (5)
C3—C4—C5—C6	1.5 (6)	O12—C35—C40—C39	-178.4 (3)
C2-C1-C6-C5	-0.4 (4)	C38—C39—C40—C35	-1.2 (7)
O6—C1—C6—C5	-178.2 (3)	C35—O12—C41—C43	150.9 (2)
C4—C5—C6—C1	-0.6 (5)	C35—O12—C41—C42	-109.3(2)
C1—O6—C7—C9	-88.7 (2)	C43—N3—C42—C44	-108.3(2)
C1—O6—C7—C8	172.60 (19)	C68—N3—C42—C44	71.3 (3)
C9—N1—C8—C10	112.63 (19)	C43—N3—C42—C41	8.43 (18)
C34—N1—C8—C10	-69.8 (3)	C68—N3—C42—C41	-172.0(3)
C9—N1—C8—C7	-5.46 (17)	O12—C41—C42—N3	-125.1(2)
C34—N1—C8—C7	172.1 (2)	C43—C41—C42—N3	-7.46 (16)
06—C7—C8—N1	125.40 (18)	012-C41-C42-C44	-8.3(3)
C9-C7-C8-N1	4.78 (15)	C43—C41—C42—C44	109.4 (2)
Q6—C7—C8—C10	8.9 (3)	C68—N3—C43—O8	-6.5(5)
C9—C7—C8—C10	-111.7(2)	C42 - N3 - C43 - O8	173.1 (3)
$C_{34} N_{1} C_{9} O_{2}$	7 3 (4)	C68 - N3 - C43 - C41	171.8(2)
C8—N1—C9—O2	-175.1(3)	C42 - N3 - C43 - C41	-8.66(18)
C34—N1—C9—C7	-172.1(2)	012-C41-C43-08	-53.8(4)
C8—N1—C9—C7	5.54 (18)	C42-C41-C43-O8	-173.8(3)
06—C7—C9—O2	60.6 (4)	012-C41-C43-N3	128.0 (2)
C8-C7-C9-O2	175.5 (3)	C42—C41—C43—N3	8.07 (17)
06—C7—C9—N1	-120.1(2)	N3-C42-C44-C45	15.0 (3)
C8-C7-C9-N1	-5.19 (16)	C41—C42—C44—C45	-83.2(3)
N1—C8—C10—C11	-18.3 (3)	N3—C42—C44—C49	-168.2(2)
C7—C8—C10—C11	80.8 (3)	C41—C42—C44—C49	93.5 (3)
N1—C8—C10—C15	163.82 (19)	C49—C44—C45—C46	0.9 (4)
C7—C8—C10—C15	-97.1 (2)	C42—C44—C45—C46	177.6 (2)
C15—C10—C11—C12	-0.7 (4)	C44—C45—C46—C47	2.0 (4)
C8-C10-C11-C12	-178.5 (3)	C45—C46—C47—C48	-3.3 (5)
C10-C11-C12-C13	-1.0 (5)	C46—C47—C48—C49	1.7 (5)
C11—C12—C13—C14	1.1 (6)	C50—O10—C49—C44	142.0 (3)
C12—C13—C14—C15	0.5 (5)	C50—O10—C49—C48	-42.6 (4)
C16—O4—C15—C14	32.2 (4)	C45—C44—C49—O10	173.0 (2)
C16—O4—C15—C10	-151.8 (2)	C42—C44—C49—O10	-3.9(3)
C13—C14—C15—O4	173.6 (3)	C45—C44—C49—C48	-2.5(4)
C13—C14—C15—C10	-2.2 (4)	C42—C44—C49—C48	-179.4(2)
C11—C10—C15—O4	-173.8 (2)	C47—C48—C49—O10	-173.8(3)
C8—C10—C15—O4	4.1 (3)	C47—C48—C49—C44	1.3 (5)
C11—C10—C15—C14	2.3 (4)	C49—O10—C50—C51	-130.4(3)
C8-C10-C15-C14	-179.8 (2)	C52—O9—C51—C50	-164.1 (2)
C15—O4—C16—C17	134.4 (3)	O10—C50—C51—O9	66.6 (3)
C18—O3—C17—C16	153.4 (2)	C51—O9—C52—C53	-15.0(4)
O4—C16—C17—O3	-68.4 (3)	C51—O9—C52—C57	164.8 (2)
C17—O3—C18—C19	27.5 (3)	O9—C52—C53—C54	179.3 (2)
C17—O3—C18—C23	-154.7 (2)	C57—C52—C53—C54	-0.5 (4)
O3—C18—C19—C20	177.7 (2)	C52—C53—C54—C55	0.4 (4)
C23—C18—C19—C20	0.0 (3)	C53—C54—C55—C56	-0.4 (4)

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C18—C19—C20—C21	-0.2 (3)	C54—C55—C56—C57	0.6 (4)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C19—C20—C21—C22	0.2 (4)	C55—C56—C57—C52	-0.7(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C20—C21—C22—C23	0.1 (3)	C55—C56—C57—C58	177.1 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C21—C22—C23—C18	-0.2(3)	O9—C52—C57—C56	-179.2(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{21} - C_{22} - C_{23} - C_{24}$	179.76 (19)	C53—C52—C57—C56	0.6 (3)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	03-C18-C23-C22	-177.61(18)	09-C52-C57-C58	30(3)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	C19 - C18 - C23 - C22	0.2(3)	C_{53} C_{52} C_{57} C_{58}	-1772(2)
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	03-C18-C23-C24	2.4(3)	C60 - N4 - C58 - C57	-106.8(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C19 - C18 - C23 - C24	-179.81(18)	C67 - N4 - C58 - C57	649(3)
$ \begin{array}{c} 10 & 10 & 10 & 10 & 10 & 10 & 10 & 10 $	$C_{26} = N_{2} = C_{24} = C_{23}$	109.9 (2)	C60 - N4 - C58 - C59	9 08 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C_{33} N2 C_{24} C_{23}	-613(3)	C67 - N4 - C58 - C59	-1792(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{26} N_{2} C_{24} C_{25}$	-7.52(18)	$C_{56} - C_{57} - C_{58} - N_4$	369(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{20} = N_2 = C_{24} = C_{25}$	-1787(2)	C_{2} C_{2	-14529(19)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C_{22} C_{23} C_{24} C_{25} C_{23} C_{24} C_{23} C	-323(3)	$C_{52} = C_{57} = C_{58} = C_{59}$	-60.0(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{22} = C_{23} = C_{24} = N_2$	147.69(18)	$C_{50} = C_{57} = C_{58} = C_{59}$	117.8(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{10} = C_{23} = C_{24} = N_2$	(13)	$C_{52} - C_{51} - C_{58} - C_{59}$	117.3(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{22} = C_{23} = C_{24} = C_{25}$	-1143(2)	$C_{01} = 011 = C_{00} = C_{00}$	(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{18} - C_{23} - C_{24} - C_{23}$	-114.3(2) -85.4(2)	N4 C58 C59 O11	-1/1.2/(19) -120.7(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{27} = 05 = C_{25} = C_{20}$	-63.4(2)	$N4 - C_{50} - C_{59} - O_{11}$	-129.7(2)
$\begin{split} & (22-24-223-03) & (12)(13) & (13) & (14)-(33-03)-(20) & (10)(16)(2) \\ & (223-224-225-05) & (11,7)(3) & (257-058-059-060) & (106,7)(2) \\ & (224-225-226) & (258-14-060-07) & (10,7)(2) \\ & (23-24-225-226-01) & (-1,5)(4) & (267-144-060-07) & (10,7)(3) \\ & (23-12-226-01) & (-1,7)(3) & (258-14)-060-07 & (-5,6)(4) \\ & (24-12-226-225) & (17,9)(4) & (21)(1-059-060-07) & (-5,6)(4) \\ & (24-12-226-025) & (12,9)(4) & (21)(1-059-060-07) & (-1,7)(4) \\ & (24-12-226-226-01) & (59,4)(4) & (011-059-060-07) & (-1,7)(4)(3) \\ & (24-225-226-01) & (59,4)(4) & (011-059-060-07) & (-1,7)(4)(3) \\ & (24-225-026-01) & (59,4)(4) & (011-059-060-07) & (-1,7)(4)(3) \\ & (24-225-026-01) & (59,4)(4) & (011-059-060-07) & (-1,7)(4)(3) \\ & (24-225-026-02) & (-1,2)(5) & (259-011-061-066) & (-40,3)(3) \\ & (24-025-026-02) & (-1,2)(5) & (259-011-061-062) & (14,2)(4) \\ & (25-05-027-028) & (-1,2)(3) & (06-061-062) & (06) & (14) \\ & (25-05-027-028) & (-1,3)(8)(2) & (011-061-062) & (-63) & (17,4)(3) \\ & (23-027-028-029) & (-0,5)(4) & (061-062) & (-63) & (-1,4)(4) \\ & (229-030-031) & (0,8)(4) & (062-063-064-065) & (0,0)(5) \\ & (27-028-029-030-031) & (0,8)(4) & (062-063-064-065) & (0,1)(4) \\ & (229-030-031-032) & (-0,7)(4) & (011-061-066-065) & (-1,7)(0)(2) \\ & (228-027-032-031) & (0,6)(4) & (264-065-066) & (0,2)(4) \\ & (28-029-030-031) & (0,8)(4) & (062-063-064-065) & (0,1)(4) \\ & (29-030-031-032) & (-0,7)(4) & (011-061-066-065) & (-1,7)(0)(2) \\ & (228-027-032-031) & (1,7)(9)(2) & (260-14-065) & (-0,3)(4) \\ & (05-027-032-031) & (1,7)(9)(2) & (260-14-065) & (-1,3)(4) \\ & (26-12-063-03-034) & (-1,7)(9)(2) & (260-14-065-066) & (-1,2)(3) \\ & (24-12-03-03) & (-1,2)(3) & (-1,3) & $	$C_2/-O_3-C_{23}-C_{24}$	170.11(19) 127.12(10)	$C_{3} = C_{3} = C_{3} = C_{3} = C_{3}$	-13.1(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$N_2 = C_2 4 = C_2 5 = 05$	127.13(19)	N4 - C38 - C39 - C60	-7.93(10)
$\begin{split} & \text{N2} = -224225226 & -108.9 & (2) & -05407 & -17.0 & (3) \\ & \text{C23} = -224225226 & -108.9 & (2) & -15.5 & (4) & -0.7 & -170.9 & (3) \\ & \text{C33} = -N2226 - 01 & -1.5 & (4) & -0.7 & -170.4 & (600.59 & -9.21 & (18) \\ & \text{C33} = -N2226 - 01 & -173.3 & (3) & -0.58N40.60 - 0.7 & -56.5 & (4) \\ & \text{C24} - N22260.25 & 7.62 & (18) & -0.580.590.60 - 0.7 & -171.4 & (3) \\ & \text{O5}0.250.26 - 0.1 & 59.4 & (4) & -0.110.590.60 - 0.7 & -171.4 & (3) \\ & \text{O5}0.250.26 - 0.1 & 59.4 & (4) & -0.110.590.60 - 0.7 & -171.4 & (3) \\ & \text{O5}0.250.26 - 0.1 & 73.8 & (3) & -0.580.590.60 - 0.7 & -171.4 & (3) \\ & \text{O5}0.250.26 - 0.1 & 73.8 & (3) & -0.580.590.60 - 0.8 & 8.66 & (17) \\ & \text{O5}0.250.26 - 0.1 & -71.5 & (17) & -0.590.60 - 0.8 & 8.66 & (17) \\ & \text{O5}0.250.26 - 0.2 & -71.15 & (17) & -0.590.60 - 0.8 & 8.66 & (17) \\ & \text{O5}0.250.26 - 0.2 & -71.5 & (17) & -0.59 - 0.010.610.66 & -40.3 & (3) \\ & \text{C24}0.250.26 - 0.2 & -71.5 & (17) & -0.59 - 0.010.610.62 & -0.42 & (2) \\ & \text{C25}0.50.270.28 & -139.8 & (2) & -0.110.610.620.63 & -0.1 & (4) \\ & \text{C25} - 0.50.270.28 & -139.8 & (2) & -0.110.610.620.63 & -0.1 & (4) \\ & \text{C25}0.50.270.280.29 & -0.5 & (4) & -0.610.660.65 & -0.1 & (4) \\ & \text{C28}0.290.30 & -0.2 & (5) & -0.630.64 & -0.1 & (5) \\ & \text{O5}0.270.280.29 & -0.7 & (4) & -0.10.660.65 & -0.1 & (4) \\ & \text{C28}0.290.31 & 0.6 & (4) & -0.640.650.66 & 0.2 & (4) \\ & \text{C28}0.270.220.31 & 0.6 & (4) & -0.640.660.65 & -177.0 & (2) \\ & \text{C28}0.270.320.31 & 0.6 & (4) & -0.640.670.68 & -10.3 & (4) \\ & \text{O5}0.270.320.31 & 0.6 & (4) & -0.640.680.67 & -0.12.1 & (3) \\ & \text{C28}0.270.320.31 & 0.6 & (4) & -0.640.680.67 & -0.8 & 5 & (4) \\ & \text{C9} - N10.340.33 & -0.42 & (3) & -0.640.7$	$C_{23} = C_{24} = C_{25} = C_{26}$	11.7(3)	$C_{57} = C_{58} = C_{59} = C_{60}$	100.7(2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$N_2 = C_2 4 = C_2 5 = C_2 6$	0.34(10)	$C_{0} = N_{1} = C_{0} = 07$	-1.0(3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{23} = C_{24} = C_{25} = C_{26}$	-108.9(2)	$C_{38} = N_{4} = C_{60} = C_{7}$	170.9 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{33} = N_2 = C_{26} = O_1$	-1.5(4)	$C_{6} - N_{4} - C_{60} - C_{59}$	1/8.9 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$C_{24} = N_{2} = C_{26} = O_{1}$	-1/3.3(3)	C_{58} N4 C_{60} C59	-9.21 (18)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C_{33} N2 C_{26} C_{25}	1/9.4 (2)	011-059-060-07	-56.5 (4)
$\begin{array}{llllllllllllllllllllllllllllllllllll$	C24—N2—C26—C25	7.62 (18)	C58—C59—C60—O7	-1/1.4 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	05-025-01	59.4 (4)	011—C59—C60—N4	123.5 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C24—C25—C26—O1	173.8 (3)	C58—C59—C60—N4	8.66 (17)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O5—C25—C26—N2	-121.5 (2)	C59—O11—C61—C66	-40.3 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C24—C25—C26—N2	-7.15 (17)	C59—O11—C61—C62	142.4 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C25—O5—C27—C32	42.8 (3)	C66—C61—C62—C63	0.1 (4)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C25—O5—C27—C28	-139.8 (2)	O11—C61—C62—C63	177.4 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C32—C27—C28—C29	-0.5(4)	C61—C62—C63—C64	-0.1(5)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O5—C27—C28—C29	-178.0 (3)	C62—C63—C64—C65	0.0 (5)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C27—C28—C29—C30	-0.2 (5)	C63—C64—C65—C66	0.2 (4)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C28—C29—C30—C31	0.8 (4)	C62—C61—C66—C65	0.1 (4)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C29—C30—C31—C32	-0.7 (4)	O11—C61—C66—C65	-177.0 (2)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C28—C27—C32—C31	0.6 (4)	C64—C65—C66—C61	-0.3 (4)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	O5—C27—C32—C31	177.9 (2)	C60—N4—C67—C68	-112.9 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C30—C31—C32—C27	0.0 (4)	C58—N4—C67—C68	78.0 (3)
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	C26—N2—C33—C34	107.1 (3)	C43—N3—C68—C67	-112.1 (3)
C9—N1—C34—C33 112.5 (3) N4—C67—C68—N3 -97.4 (3) C8—N1—C34—C33 -64.3 (3) C71—O13—C70—O14 2.0 (5) N2—C33—C34—N1 95.2 (2) C71—O13—C70—C69 -174.3 (4) C41—O12—C35—C40 17.9 (4) C70—O13—C71—C72 175.5 (4) C41—O12—C35—C36 -162.4 (2) C70—O13—C71—C72 175.5 (4)	C24—N2—C33—C34	-84.2 (3)	C42—N3—C68—C67	68.5 (4)
C8—N1—C34—C33 -64.3 (3) C71—O13—C70—O14 2.0 (5) N2—C33—C34—N1 95.2 (2) C71—O13—C70—C69 -174.3 (4) C41—O12—C35—C40 17.9 (4) C70—O13—C71—C72 175.5 (4) C41—O12—C35—C36 -162.4 (2) -162.4 (2) -162.4 (2)	C9—N1—C34—C33	112.5 (3)	N4—C67—C68—N3	-97.4 (3)
N2—C33—C34—N1 95.2 (2) C71—O13—C70—C69 -174.3 (4) C41—O12—C35—C40 17.9 (4) C70—O13—C71—C72 175.5 (4) C41—O12—C35—C36 -162.4 (2) -162.4 (2) -162.4 (2)	C8—N1—C34—C33	-64.3 (3)	C71—O13—C70—O14	2.0 (5)
C41—O12—C35—C40 17.9 (4) C70—O13—C71—C72 175.5 (4) C41—O12—C35—C36 -162.4 (2) C70—O13—C71—C72 175.5 (4)	N2-C33-C34-N1	95.2 (2)	C71—O13—C70—C69	-174.3 (4)
C41—O12—C35—C36 –162.4 (2)	C41—O12—C35—C40	17.9 (4)	C70—O13—C71—C72	175.5 (4)
	C41—O12—C35—C36	-162.4 (2)		

D—H···A	<i>D</i> —Н	$H \cdots A$	$D \cdots A$	D—H··· A	
С53—Н53…О6	0.93	2.52	3.344 (3)	147	
С2—Н2…О2	0.93	2.42	3.250 (3)	149	
C32—H32…O1	0.93	2.33	3.178 (3)	151	
С66—Н66…О7	0.93	2.48	3.299 (3)	147	

Hydrogen-bond geometry (Å, °)