# organic compounds

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# 9-(7-Fluoro-4-oxo-4H-chromen-3-yl)-3,3,6,6-tetramethyl-2,3,4,5,6,7,8,9-octahydro-1*H*-xanthene-1,8-dione

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Key indicators: single-crystal X-ray study; T = 296 K; mean  $\sigma$ (C–C) = 0.002 Å; R factor = 0.052; wR factor = 0.150; data-to-parameter ratio = 22.4.

In the title compound, C<sub>26</sub>H<sub>25</sub>FO<sub>5</sub>, the terminal cyclohexane rings of the xanthene ring system adopt half-boat conformations. The 4H-chromene ring make a dihedral angle of  $87.94(5)^{\circ}$  with the xanthene ring system and its carbonyl O atom lies above the xanthene O atom. In the crystal, molecules are linked into ribbons propagating along the *a*-axis direction by C-H···O hydrogen bonds. Aromatic  $\pi$ - $\pi$  stacking interactions [centroid–centroid distance = 3.7367(12) Å] also occur.

### **Related literature**

For a related structure and background to the properties and applications of xanthene derivatives, see: Mehdi et al. (2011). For ring conformations, see: Cremer & Pople (1975). For reference bond-length data, see: Allen et al. (1987).



#### Crystal data

C26H25FO5 V = 2264.0 (5) Å<sup>3</sup>  $M_r = 436.46$ Z = 4Monoclinic,  $P2_1/c$ Mo  $K\alpha$  radiation  $\mu = 0.09 \text{ mm}^{-1}$ a = 6.9475 (8) Å b = 18.596 (2) Å T = 296 Kc = 17.559 (2) Å  $0.51 \times 0.38 \times 0.24 \text{ mm}$  $\beta = 93.658 \ (2)^{\circ}$ 

### Data collection

Bruker SMART APEXII DUO CCD diffractometer Absorption correction: multi-scan (SADABS; Bruker, 2009)  $T_{\min} = 0.954, \ T_{\max} = 0.978$ 

### Refinement

| $R[F^2 > 2\sigma(F^2)] = 0.052$ | 293 parameters   |
|---------------------------------|--|
| $wR(F^2) = 0.150$               | H-atom parameters constrained                              |
| S = 1.03                        | $\Delta \rho_{\rm max} = 0.24 \text{ e } \text{\AA}^{-3}$  |
| 6574 reflections                | $\Delta \rho_{\rm min} = -0.22 \text{ e } \text{\AA}^{-3}$ |

21143 measured reflections

 $R_{\rm int} = 0.034$ 

6574 independent reflections

4315 reflections with  $I > 2\sigma(I)$ 

### Table 1

# Hydrogen-bond geometry (Å, °).

 $D - H \cdot \cdot \cdot A$ D-H $H \cdots A$  $D \cdots A$  $D - H \cdot \cdot \cdot A$  $C15-H15B\cdots O4^{i}$ 0.97 2.44 3.3487 (19) 156 C18-H18A···O5<sup>i</sup> 0.97 2.45 3.3821 (19) 162

Symmetry code: (i) x + 1, y, z.

Data collection: APEX2 (Bruker, 2009); cell refinement: SAINT (Bruker, 2009); data reduction: SAINT; program(s) used to solve structure: SHELXTL (Sheldrick, 2008); program(s) used to refine structure: SHELXTL; molecular graphics: SHELXTL; software used to prepare material for publication: SHELXTL and PLATON (Spek, 2009).

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HB6535).

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# supporting information

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# 9-(7-Fluoro-4-oxo-4*H*-chromen-3-yl)-3,3,6,6-tetramethyl-2,3,4,5,6,7,8,9-octahydro-1*H*-xanthene-1,8-dione

## Mohammad Asad, Chuan-Wei Oo, Hasnah Osman, Hoong-Kun Fun and Suhana Arshad

### S1. Comment

As part of our ongoing studies of xanthene derivatives (Mehdi *et al.*, 2011), we now describe the synthesis and structure of the title compound, (I).

In the molecular structure, (Fig. 1), the terminal cyclohexane rings (C11–C16 & C17–C22) of the xanthene ring system adopt half boat conformations with puckering parameters Q= 0.4688 (18) Å,  $\Theta$ = 124.2 (2)°,  $\varphi$ = 348.2 (3)° and Q= 0.4638 (17) Å,  $\Theta$ = 54.8 (2)°,  $\varphi$ = 129.1 (2)° (Cremer & Pople, 1975), respectively. The 4*H*-chromene ring (O1/C1–C9) is approximately perpendicular to the xanthene ring system (O2/C10–C22) with dihedral angle of 87.94 (5)°. Bond lengths (Allen *et al.*, 1987) and angles are within normal ranges and comparable to a related structure (Mehdi *et al.*, 2011).

The crystal packing is shown in Fig. 2. The molecules are linked into ribbons along the *a* axis *via* intermolecular C15—H15B···O4 and C18—H18A···O5 hydrogen bonds (Table 1).  $\pi$ - $\pi$  interactions of Cg1···Cg1 = 3.7367 (12) Å [Cg1 is the centroid of the benzene ring (C2–C7); symmetry code: -*x*, 1 - *y*, 2 - *z*] further stabilized the structure.

### **S2. Experimental**

A mixture of 7-fluoro-3-formylchromone (2.60 mmol, 0.50 g) and dimedone (5.20 mmol, 0.73 g) in 30 ml methanol was stirred at room temperature overnight. The reaction progress was monitored by TLC. After the reaction was completed, the precipitate obtained was filtered, washed with methanol and dried. The isolated product was further purified by recrystallization from chloroform-methanol (1:1  $\nu/\nu$ ) to give the pure title compounds as colorless blocks in 92% yield.

### **S3. Refinement**

All H atoms were positioned geometrically [C-H = 0.93-0.98 Å] and refined using a riding model with  $U_{iso}(H) = 1.2$  or 1.5  $U_{eq}(C)$ . A rotating group model was applied to the methyl groups.



# Figure 1

The molecular structure of the title compound with 30% probability displacement ellipsoids.



## Figure 2

The crystal packing of the title compound. The H atoms not involved in the intermolecular interactions (dashed lines) have been omitted for clarity.

## 9-(7-Fluoro-4-oxo-4H-chromen-3-yl)-3,3,6,6-tetramethyl- 2,3,4,5,6,7,8,9-octahydro-1H-xanthene-1,8-dione

| Crystal data  |  |
|---|--|
| $C_{26}H_{25}FO_5$<br>$M_r = 436.46$<br>Monoclinic, $P2_1/c$<br>Hall symbol: -P 2ybc<br>a = 6.9475 (8) Å<br>b = 18.596 (2) Å<br>c = 17.559 (2) Å<br>$\beta = 93.658$ (2)°   | F(000) = 920<br>$D_x = 1.281 \text{ Mg m}^{-3}$<br>Mo K\alpha radiation, $\lambda = 0.71073 \text{ Å}$<br>Cell parameters from 5340 reflections<br>$\theta = 2.5-29.3^{\circ}$<br>$\mu = 0.09 \text{ mm}^{-1}$<br>T = 296  K<br>Block, colourless                        |
| V = 2264.0 (S) A <sup>3</sup><br>Z = 4  | $0.51 \times 0.38 \times 0.24$ mm  |
| Data collection   |  |
| Bruker SMART APEXII DUO CCD<br>diffractometer<br>Radiation source: fine-focus sealed tube<br>Graphite monochromator<br>$\varphi$ and $\omega$ scans<br>Absorption correction: multi-scan<br>( <i>SADABS</i> ; Bruker, 2009)<br>$T_{min} = 0.954, T_{max} = 0.978$ | 21143 measured reflections<br>6574 independent reflections<br>4315 reflections with $I > 2\sigma(I)$<br>$R_{int} = 0.034$<br>$\theta_{max} = 30.0^{\circ}, \theta_{min} = 1.6^{\circ}$<br>$h = -9 \rightarrow 9$<br>$k = -24 \rightarrow 26$<br>$l = -24 \rightarrow 24$ |
| Refinement  |  |
| Refinement on $F^2$<br>Least-squares matrix: full<br>$R[F^2 > 2\sigma(F^2)] = 0.052$<br>$wR(F^2) = 0.150$<br>S = 1.03<br>6574 reflections<br>293 parameters<br>0 restraints   | <ul> <li>Primary atom site location: structure-invariant direct methods</li> <li>Secondary atom site location: difference Fourier map</li> <li>Hydrogen site location: inferred from neighbouring sites</li> <li>H-atom parameters constrained</li> </ul>                |

 $w = 1/[\sigma^{2}(F_{o}^{2}) + (0.0621P)^{2} + 0.5163P] \qquad \Delta \rho_{\max} = 0.24 \text{ e } \text{\AA}^{-3}$ where  $P = (F_{o}^{2} + 2F_{c}^{2})/3 \qquad \Delta \rho_{\min} = -0.22 \text{ e } \text{\AA}^{-3}$  $(\Delta/\sigma)_{\max} = 0.001$ 

### Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

| Fractional atomic coordinates | and isotropic | or equivalent isotro | pic displacement | parameters | $(Å^2)$ | ļ |
|-------------------------------|---------------|----------------------|------------------|------------|---------|---|
|-------------------------------|---------------|----------------------|------------------|------------|---------|---|

|      | x             | У            | Ζ            | $U_{ m iso}$ */ $U_{ m eq}$ |  |
|------|---------------|--------------|--------------|-----------------------------|--|
| F1   | 0.0382 (3)    | 0.36000 (10) | 1.08974 (8)  | 0.1100 (6)                  |  |
| 01   | -0.25037 (17) | 0.46251 (7)  | 0.86767 (7)  | 0.0562 (3)                  |  |
| O2   | 0.29558 (13)  | 0.54942 (6)  | 0.61824 (6)  | 0.0400 (2)                  |  |
| 03   | 0.26966 (16)  | 0.48699 (8)  | 0.77520 (7)  | 0.0599 (4)                  |  |
| O4   | -0.21687 (16) | 0.66244 (8)  | 0.73490 (8)  | 0.0624 (4)                  |  |
| 05   | -0.25611 (16) | 0.40218 (7)  | 0.62320 (8)  | 0.0626 (4)                  |  |
| C1   | -0.2364 (2)   | 0.48941 (9)  | 0.79629 (10) | 0.0467 (4)                  |  |
| H1A  | -0.3502       | 0.5028       | 0.7692       | 0.056*                      |  |
| C2   | -0.0864 (3)   | 0.43986 (9)  | 0.90721 (10) | 0.0491 (4)                  |  |
| C3   | -0.1071 (3)   | 0.41034 (11) | 0.97924 (11) | 0.0654 (5)                  |  |
| H3A  | -0.2278       | 0.4060       | 0.9988       | 0.079*                      |  |
| C4   | 0.0547 (4)    | 0.38826 (12) | 1.01969 (12) | 0.0713 (6)                  |  |
| C5   | 0.2370 (4)    | 0.39369 (13) | 0.99353 (12) | 0.0735 (6)                  |  |
| H5A  | 0.3447        | 0.3783       | 1.0233       | 0.088*                      |  |
| C6   | 0.2552 (3)    | 0.42249 (11) | 0.92207 (11) | 0.0612 (5)                  |  |
| H6A  | 0.3768        | 0.4260       | 0.9031       | 0.073*                      |  |
| C7   | 0.0939 (2)    | 0.44652 (9)  | 0.87767 (9)  | 0.0462 (4)                  |  |
| C8   | 0.1115 (2)    | 0.47825 (9)  | 0.80182 (9)  | 0.0438 (4)                  |  |
| C9   | -0.0704 (2)   | 0.49818 (9)  | 0.76172 (9)  | 0.0402 (3)                  |  |
| C10  | -0.07496 (19) | 0.52939 (8)  | 0.68162 (8)  | 0.0384 (3)                  |  |
| H10A | -0.2097       | 0.5382       | 0.6642       | 0.046*                      |  |
| C11  | 0.03248 (19)  | 0.59992 (8)  | 0.68064 (8)  | 0.0379 (3)                  |  |
| C12  | -0.0564 (2)   | 0.66493 (9)  | 0.71072 (9)  | 0.0444 (4)                  |  |
| C13  | 0.0533 (2)    | 0.73440 (10) | 0.70679 (12) | 0.0560 (4)                  |  |
| H13A | 0.0127        | 0.7664       | 0.7464       | 0.067*                      |  |
| H13B | 0.0203        | 0.7571       | 0.6579       | 0.067*                      |  |
| C14  | 0.2729 (2)    | 0.72520 (9)  | 0.71637 (10) | 0.0455 (4)                  |  |
| C15  | 0.3311 (2)    | 0.67069 (9)  | 0.65689 (9)  | 0.0426 (3)                  |  |
| H15A | 0.3234        | 0.6934       | 0.6071       | 0.051*                      |  |
| H15B | 0.4642        | 0.6566       | 0.6685       | 0.051*                      |  |
| C16  | 0.20817 (19)  | 0.60537 (8)  | 0.65378 (8)  | 0.0368 (3)                  |  |
| C17  | 0.18772 (19)  | 0.48912 (8)  | 0.60097 (8)  | 0.0354 (3)                  |  |

| C18  | 0.2912 (2)   | 0.43901 (8)  | 0.55154 (9)  | 0.0406 (3) |
|------|--------------|--------------|--------------|------------|
| H18A | 0.4275       | 0.4393       | 0.5674       | 0.049*     |
| H18B | 0.2773       | 0.4558       | 0.4992       | 0.049*     |
| C19  | 0.2145 (2)   | 0.36198 (9)  | 0.55528 (9)  | 0.0423 (3) |
| C20  | -0.0053 (2)  | 0.36473 (9)  | 0.54550 (10) | 0.0474 (4) |
| H20A | -0.0428      | 0.3803       | 0.4940       | 0.057*     |
| H20B | -0.0557      | 0.3166       | 0.5517       | 0.057*     |
| C21  | -0.0958 (2)  | 0.41424 (9)  | 0.60100 (9)  | 0.0420 (3) |
| C22  | 0.01150 (19) | 0.47845 (8)  | 0.62625 (8)  | 0.0367 (3) |
| C23  | 0.3742 (3)   | 0.79644 (10) | 0.70260 (13) | 0.0630 (5) |
| H23A | 0.3381       | 0.8132       | 0.6520       | 0.094*     |
| H23B | 0.5113       | 0.7895       | 0.7080       | 0.094*     |
| H23C | 0.3369       | 0.8313       | 0.7392       | 0.094*     |
| C24  | 0.3312 (3)   | 0.69813 (11) | 0.79693 (10) | 0.0565 (5) |
| H24A | 0.4685       | 0.6916       | 0.8022       | 0.085*     |
| H24B | 0.2684       | 0.6531       | 0.8054       | 0.085*     |
| H24C | 0.2934       | 0.7327       | 0.8337       | 0.085*     |
| C25  | 0.2778 (3)   | 0.32836 (10) | 0.63219 (11) | 0.0555 (4) |
| H25A | 0.2259       | 0.2806       | 0.6348       | 0.083*     |
| H25B | 0.2313       | 0.3571       | 0.6726       | 0.083*     |
| H25C | 0.4161       | 0.3262       | 0.6375       | 0.083*     |
| C26  | 0.2962 (3)   | 0.31780 (11) | 0.49147 (12) | 0.0645 (5) |
| H26A | 0.2458       | 0.2698       | 0.4925       | 0.097*     |
| H26B | 0.4343       | 0.3163       | 0.4987       | 0.097*     |
| H26C | 0.2600       | 0.3396       | 0.4431       | 0.097*     |
|      |              |              |              |            |

Atomic displacement parameters  $(\mathring{A}^2)$ 

|     | $U^{11}$    | $U^{22}$    | U <sup>33</sup> | $U^{12}$     | $U^{13}$    | <i>U</i> <sup>23</sup> |
|-----|-------------|-------------|-----------------|--------------|-------------|------------------------|
| F1  | 0.1401 (15) | 0.1261 (13) | 0.0658 (8)      | 0.0020 (11)  | 0.0231 (9)  | 0.0400 (8)             |
| 01  | 0.0411 (6)  | 0.0750 (8)  | 0.0545 (7)      | -0.0079 (6)  | 0.0193 (5)  | 0.0016 (6)             |
| O2  | 0.0267 (5)  | 0.0454 (6)  | 0.0489 (6)      | -0.0015 (4)  | 0.0099 (4)  | -0.0043 (5)            |
| 03  | 0.0291 (5)  | 0.0953 (10) | 0.0562 (7)      | 0.0035 (6)   | 0.0084 (5)  | 0.0158 (7)             |
| O4  | 0.0302 (6)  | 0.0743 (9)  | 0.0838 (9)      | 0.0068 (5)   | 0.0124 (6)  | -0.0161 (7)            |
| 05  | 0.0307 (6)  | 0.0703 (9)  | 0.0874 (10)     | -0.0117 (5)  | 0.0089 (6)  | -0.0105 (7)            |
| C1  | 0.0328 (7)  | 0.0583 (10) | 0.0502 (9)      | -0.0036 (7)  | 0.0112 (6)  | -0.0029 (7)            |
| C2  | 0.0518 (9)  | 0.0494 (9)  | 0.0476 (9)      | -0.0067 (7)  | 0.0141 (7)  | -0.0031 (7)            |
| C3  | 0.0758 (13) | 0.0663 (13) | 0.0569 (11)     | -0.0111 (10) | 0.0256 (10) | 0.0029 (9)             |
| C4  | 0.0988 (17) | 0.0660 (13) | 0.0505 (11)     | -0.0014 (12) | 0.0167 (11) | 0.0118 (9)             |
| C5  | 0.0844 (15) | 0.0763 (15) | 0.0595 (12)     | 0.0116 (12)  | 0.0021 (11) | 0.0148 (10)            |
| C6  | 0.0567 (11) | 0.0704 (13) | 0.0569 (11)     | 0.0086 (9)   | 0.0069 (8)  | 0.0093 (9)             |
| C7  | 0.0450 (8)  | 0.0495 (9)  | 0.0449 (8)      | -0.0012 (7)  | 0.0085 (7)  | -0.0006 (7)            |
| C8  | 0.0337 (7)  | 0.0547 (9)  | 0.0437 (8)      | 0.0001 (6)   | 0.0067 (6)  | 0.0002 (7)             |
| C9  | 0.0281 (6)  | 0.0493 (9)  | 0.0441 (8)      | -0.0018 (6)  | 0.0086 (6)  | -0.0037 (7)            |
| C10 | 0.0198 (6)  | 0.0507 (9)  | 0.0448 (8)      | 0.0012 (5)   | 0.0042 (5)  | -0.0020 (6)            |
| C11 | 0.0256 (6)  | 0.0478 (8)  | 0.0403 (7)      | 0.0026 (6)   | 0.0022 (5)  | -0.0018 (6)            |
| C12 | 0.0278 (7)  | 0.0563 (10) | 0.0487 (9)      | 0.0072 (6)   | -0.0007 (6) | -0.0057 (7)            |
| C13 | 0.0418 (9)  | 0.0516 (10) | 0.0745 (12)     | 0.0079 (7)   | 0.0023 (8)  | -0.0099 (9)            |

| C14 | 0.0379 (8)  | 0.0469 (9)  | 0.0517 (9)  | -0.0029 (6) | 0.0044 (6)  | -0.0069 (7) |
|-----|-------------|-------------|-------------|-------------|-------------|-------------|
| C15 | 0.0324 (7)  | 0.0503 (9)  | 0.0456 (8)  | -0.0048 (6) | 0.0070 (6)  | -0.0011 (7) |
| C16 | 0.0278 (6)  | 0.0450 (8)  | 0.0377 (7)  | 0.0022 (6)  | 0.0028 (5)  | -0.0009 (6) |
| C17 | 0.0280 (6)  | 0.0414 (8)  | 0.0367 (7)  | 0.0003 (5)  | 0.0019 (5)  | 0.0020 (6)  |
| C18 | 0.0342 (7)  | 0.0466 (8)  | 0.0418 (8)  | 0.0029 (6)  | 0.0088 (6)  | 0.0014 (6)  |
| C19 | 0.0376 (7)  | 0.0465 (9)  | 0.0430 (8)  | 0.0029 (6)  | 0.0054 (6)  | 0.0001 (7)  |
| C20 | 0.0415 (8)  | 0.0520 (10) | 0.0479 (9)  | -0.0032 (7) | -0.0034 (7) | -0.0050 (7) |
| C21 | 0.0281 (7)  | 0.0509 (9)  | 0.0461 (8)  | 0.0004 (6)  | -0.0031 (6) | 0.0030 (7)  |
| C22 | 0.0250 (6)  | 0.0462 (8)  | 0.0388 (7)  | 0.0018 (5)  | 0.0009 (5)  | 0.0010 (6)  |
| C23 | 0.0614 (12) | 0.0505 (11) | 0.0772 (13) | -0.0082 (8) | 0.0057 (10) | -0.0060 (9) |
| C24 | 0.0476 (10) | 0.0734 (12) | 0.0486 (9)  | -0.0106 (8) | 0.0038 (7)  | -0.0075 (9) |
| C25 | 0.0487 (9)  | 0.0567 (11) | 0.0611 (11) | 0.0096 (8)  | 0.0034 (8)  | 0.0174 (9)  |
| C26 | 0.0683 (12) | 0.0607 (12) | 0.0662 (12) | 0.0054 (9)  | 0.0177 (10) | -0.0122 (9) |
|     |             |             |             |             |             |             |

Geometric parameters (Å, °)

| F1—C4    | 1.349 (2)   | C14—C23  | 1.527 (2)   |
|----------|-------------|----------|-------------|
| 01—C1    | 1.359 (2)   | C14—C15  | 1.528 (2)   |
| O1—C2    | 1.363 (2)   | C14—C24  | 1.532 (2)   |
| O2—C17   | 1.3719 (18) | C15—C16  | 1.484 (2)   |
| O2—C16   | 1.3744 (17) | C15—H15A | 0.9700      |
| O3—C8    | 1.2317 (18) | C15—H15B | 0.9700      |
| O4—C12   | 1.2192 (18) | C17—C22  | 1.3433 (18) |
| O5—C21   | 1.2243 (18) | C17—C18  | 1.489 (2)   |
| C1—C9    | 1.3470 (19) | C18—C19  | 1.531 (2)   |
| C1—H1A   | 0.9300      | C18—H18A | 0.9700      |
| C2—C7    | 1.391 (2)   | C18—H18B | 0.9700      |
| C2—C3    | 1.395 (3)   | C19—C20  | 1.526 (2)   |
| C3—C4    | 1.354 (3)   | C19—C25  | 1.527 (2)   |
| С3—НЗА   | 0.9300      | C19—C26  | 1.528 (2)   |
| C4—C5    | 1.378 (3)   | C20—C21  | 1.507 (2)   |
| C5—C6    | 1.378 (3)   | C20—H20A | 0.9700      |
| C5—H5A   | 0.9300      | C20—H20B | 0.9700      |
| С6—С7    | 1.397 (3)   | C21—C22  | 1.461 (2)   |
| С6—Н6А   | 0.9300      | C23—H23A | 0.9600      |
| C7—C8    | 1.469 (2)   | C23—H23B | 0.9600      |
| C8—C9    | 1.455 (2)   | C23—H23C | 0.9600      |
| C9—C10   | 1.520 (2)   | C24—H24A | 0.9600      |
| C10-C22  | 1.509 (2)   | C24—H24B | 0.9600      |
| C10-C11  | 1.510(2)    | C24—H24C | 0.9600      |
| C10—H10A | 0.9800      | C25—H25A | 0.9600      |
| C11—C16  | 1.3402 (18) | C25—H25B | 0.9600      |
| C11—C12  | 1.471 (2)   | C25—H25C | 0.9600      |
| C12—C13  | 1.503 (3)   | C26—H26A | 0.9600      |
| C13—C14  | 1.534 (2)   | C26—H26B | 0.9600      |
| С13—Н13А | 0.9700      | C26—H26C | 0.9600      |
| C13—H13B | 0.9700      |          |             |

| C1—O1—C2      | 118.51 (12) | C14—C15—H15B  | 109.0       |
|---------------|-------------|---------------|-------------|
| C17—O2—C16    | 117.92 (10) | H15A—C15—H15B | 107.8       |
| C9—C1—O1      | 125.01 (16) | C11—C16—O2    | 122.77 (14) |
| C9—C1—H1A     | 117.5       | C11—C16—C15   | 125.73 (14) |
| O1—C1—H1A     | 117.5       | O2-C16-C15    | 111.49 (11) |
| O1—C2—C7      | 121.73 (15) | C22—C17—O2    | 122.97 (13) |
| O1—C2—C3      | 116.91 (16) | C22—C17—C18   | 125.75 (14) |
| C7—C2—C3      | 121.36 (18) | O2—C17—C18    | 111.29 (11) |
| C4—C3—C2      | 117.71 (19) | C17—C18—C19   | 112.21 (12) |
| C4—C3—H3A     | 121.1       | C17—C18—H18A  | 109.2       |
| С2—С3—НЗА     | 121.1       | C19—C18—H18A  | 109.2       |
| F1—C4—C3      | 118.7 (2)   | C17—C18—H18B  | 109.2       |
| F1—C4—C5      | 117.8 (2)   | C19—C18—H18B  | 109.2       |
| C3—C4—C5      | 123.53 (19) | H18A—C18—H18B | 107.9       |
| C6—C5—C4      | 118.2 (2)   | C20—C19—C25   | 110.06 (13) |
| C6—C5—H5A     | 120.9       | C20—C19—C26   | 110.59 (15) |
| C4—C5—H5A     | 120.9       | C25—C19—C26   | 109.19 (15) |
| C5—C6—C7      | 121.02 (19) | C20-C19-C18   | 108.20 (13) |
| С5—С6—Н6А     | 119.5       | C25—C19—C18   | 109.84 (14) |
| С7—С6—Н6А     | 119.5       | C26—C19—C18   | 108.95 (13) |
| C2—C7—C6      | 118.21 (16) | C21—C20—C19   | 113.78 (13) |
| C2—C7—C8      | 120.19 (15) | C21—C20—H20A  | 108.8       |
| C6—C7—C8      | 121.60 (15) | C19—C20—H20A  | 108.8       |
| O3—C8—C9      | 123.44 (15) | C21—C20—H20B  | 108.8       |
| O3—C8—C7      | 121.67 (15) | C19—C20—H20B  | 108.8       |
| C9—C8—C7      | 114.89 (13) | H20A—C20—H20B | 107.7       |
| C1—C9—C8      | 119.57 (15) | O5—C21—C22    | 120.65 (14) |
| C1—C9—C10     | 119.69 (14) | O5—C21—C20    | 121.30 (15) |
| C8—C9—C10     | 120.73 (12) | C22—C21—C20   | 118.03 (13) |
| C22—C10—C11   | 108.70 (11) | C17—C22—C21   | 118.57 (13) |
| C22—C10—C9    | 111.76 (13) | C17—C22—C10   | 121.92 (13) |
| C11—C10—C9    | 111.17 (13) | C21—C22—C10   | 119.48 (12) |
| C22-C10-H10A  | 108.4       | C14—C23—H23A  | 109.5       |
| C11—C10—H10A  | 108.4       | С14—С23—Н23В  | 109.5       |
| С9—С10—Н10А   | 108.4       | H23A—C23—H23B | 109.5       |
| C16—C11—C12   | 118.48 (14) | C14—C23—H23C  | 109.5       |
| C16—C11—C10   | 122.12 (13) | H23A—C23—H23C | 109.5       |
| C12—C11—C10   | 119.40 (12) | H23B—C23—H23C | 109.5       |
| O4—C12—C11    | 120.52 (15) | C14—C24—H24A  | 109.5       |
| O4—C12—C13    | 121.74 (15) | C14—C24—H24B  | 109.5       |
| C11—C12—C13   | 117.66 (13) | H24A—C24—H24B | 109.5       |
| C12—C13—C14   | 113.74 (14) | C14—C24—H24C  | 109.5       |
| С12—С13—Н13А  | 108.8       | H24A—C24—H24C | 109.5       |
| C14—C13—H13A  | 108.8       | H24B—C24—H24C | 109.5       |
| C12—C13—H13B  | 108.8       | C19—C25—H25A  | 109.5       |
| C14—C13—H13B  | 108.8       | C19—C25—H25B  | 109.5       |
| H13A—C13—H13B | 107.7       | H25A—C25—H25B | 109.5       |
| C23—C14—C15   | 108.81 (14) | C19—C25—H25C  | 109.5       |
|               |             |               |             |

| C23—C14—C24  | 109.51 (15)               | H25A—C25—H25C  | 109.5                    |
|--|---------------------------|--|--------------------------|
| C15—C14—C24  | 110.32 (14)               | H25B—C25—H25C  | 109.5                    |
| C23—C14—C13  | 110.57 (15)               | C19—C26—H26A   | 109.5                    |
| C15—C14—C13  | 107.69 (13)               | C19—C26—H26B   | 109.5                    |
| C24—C14—C13  | 109.92 (14)               | H26A—C26—H26B  | 109.5                    |
| C16—C15—C14  | 113.03 (12)               | C19—C26—H26C   | 109.5                    |
| C16—C15—H15A   | 109.0                     | H26A—C26—H26C  | 109.5                    |
| C14—C15—H15A   | 109.0                     | H26B—C26—H26C  | 109.5                    |
| C16—C15—H15B   | 109.0                     | 11202 020 11200  | 10,10                    |
|  | 10,10                     |  |                          |
| C2-01-C1-C9  | -2.6 (3)                  | C11—C12—C13—C14  | -33.4 (2)                |
| C1—O1—C2—C7  | 2.8 (2)                   | C12—C13—C14—C23  | 173.48 (16)              |
| C1—O1—C2—C3  | -177.91 (16)              | C12—C13—C14—C15  | 54.7 (2)                 |
| O1—C2—C3—C4  | -179.30(18)               | C12—C13—C14—C24  | -65.50 (19)              |
| C7—C2—C3—C4  | 0.0 (3)                   | C23—C14—C15—C16  | -166.89(15)              |
| C2-C3-C4-F1  | 179.54 (19)               | C24—C14—C15—C16  | 72.95 (17)               |
| C2-C3-C4-C5  | 0.2 (3)                   | C13—C14—C15—C16  | -47.01(19)               |
| F1-C4-C5-C6  | -180.0(2)                 | $C_{12}$ $C_{11}$ $C_{16}$ $C_{2}$   | -173.90(13)              |
| $C_3 - C_4 - C_5 - C_6$  | -0.7(4)                   | C10-C11-C16-O2   | 6.7 (2)                  |
| C4-C5-C6-C7  | 0.9(3)                    | $C_{12}$ $C_{11}$ $C_{16}$ $C_{15}$  | 5.1(2)                   |
| 01-C2-C7-C6  | 179 51 (17)               | C10-C11-C16-C15  | -17423(14)               |
| $C_{3}$ $C_{2}$ $C_{7}$ $C_{6}$  | 0.3(3)                    | $C_{17} - O_{2} - C_{16} - C_{11}$   | 87(2)                    |
| $01 - C^2 - C^7 - C^8$   | -0.4(3)                   | $C_{17} = 02 = C_{16} = C_{15}$  | -17042(12)               |
| $C_{3}$ $C_{2}$ $C_{7}$ $C_{8}$  | -17960(17)                | $C_{14}$ $C_{15}$ $C_{16}$ $C_{11}$  | 192(2)                   |
| $C_{5} - C_{6} - C_{7} - C_{2}^{2}$  | -0.7(3)                   | $C_{14}$ $C_{15}$ $C_{16}$ $C$ | -161.68(13)              |
| $C_{5} - C_{6} - C_{7} - C_{8}$  | 179 15 (19)               | $C_{16} = 0^{2} = C_{17} = C_{22}^{2}$   | -94(2)                   |
| $C_{2}^{-}$ $C_{7}^{-}$ $C_{8}^{-}$ $C_{3}^{-}$  | 177.60 (17)               | $C_{16} = 0^{2} = C_{17} = C_{18}$   | 170.45(12)               |
| $C_{6} - C_{7} - C_{8} - O_{3}$  | -22(3)                    | $C_{22}$ $C_{17}$ $C_{18}$ $C_{19}$  | -213(2)                  |
| $C_{2} - C_{7} - C_{8} - C_{9}$  | -2.2(3)                   | 02-C17-C18-C19   | 15887(12)                |
| $C_{2} = C_{1} = C_{3} = C_{3}$  | 2.5(2)                    | $C_{17}$ $C_{18}$ $C_{19}$ $C_{20}$  | 47.87 (17)               |
| 01 - C1 - C9 - C8  | -0.2(3)                   | $C_{17}$ $C_{18}$ $C_{19}$ $C_{25}$  | -72.29(16)               |
| 01 - C1 - C9 - C10   | -179.64(15)               | C17 - C18 - C19 - C25  | 168 15 (14)              |
| 03 - C8 - C9 - C1  | -177.33(17)               | $C_{25}$ $C_{19}$ $C_{20}$ $C_{21}$  | 65 87 (19)               |
| $C_7 C_8 C_9 C_1$  | 26(2)                     | $C_{25} = C_{15} = C_{20} = C_{21}$  | -173 42 (15)             |
| $C^{2} = C^{2} = C^{2} = C^{2}$  | 2.0(2)<br>2.1(3)          | $C_{20} = C_{10} = C_{20} = C_{21}$  | -54.16(18)               |
| $C_{7} = C_{8} = C_{9} = C_{10}$   | -178 01 (14)              | $C_{10} = C_{10} = C_{20} = C_{21}$  | -140.34(16)              |
| $C_{1} = C_{2} = C_{10}$   | $-121\ 20\ (15)$          | $C_{19} = C_{20} = C_{21} = C_{32}$  | 1+9.5+(10)               |
| $C_1 = C_2 = C_1 = C_2 = C_2$  | 50 36 (18)                | $C_{1}^{-1} = C_{2}^{-1} = C_{2}^{-1} = C_{2}^{-1} = C_{2}^{-1}$   | 52.2(2)                  |
| $C_{3} - C_{3} - C_{10} - C_{22}$  | 117 14 (16)               | $C_{18} = C_{17} = C_{22} = C_{21}$  | -32(2)                   |
| $C_1 = C_2 = C_1 $ | -62.20(18)                | $C_{10} = C_{17} = C_{22} = C_{21}$  | 5.2(2)                   |
| $C_{22} = C_{10} = C_{11} = C_{16}$  | -18.00(10)                | $C_{18} = C_{17} = C_{22} = C_{10}$  | 3.4(2)                   |
| $C_{22} = C_{10} = C_{11} = C_{10}$  | -16.99(19)<br>104 44 (16) | $C_{10} = C_{17} = C_{22} = C_{10}$  | 174.73(14)<br>170.38(15) |
| $C_{22} = C_{10} = C_{11} = C_{10}$  | 104.44(10)<br>161.65(12)  | $C_{21} = C_{22} = C_{17}$   | -22(2)                   |
| $C_{22} = C_{10} = C_{11} = C_{12}$  | 74.02(15)                 | $C_{20} = C_{21} = C_{22} = C_{17}$  | -2.2(2)                  |
| $C_{1} = C_{1} = C_{1$ | -/4.93(10)                | $C_{20} = C_{21} = C_{22} = C_{10}$  | 1.4(2)                   |
| $C_{10} = C_{11} = C_{12} = C_{4}$   | 1/9.18 (10)               | $C_{20} - C_{21} - C_{22} - C_{10}$  | 1/9.80 (13)              |
| C10-C11-C12-O4   | -1.4(2)                   | C11 - C10 - C22 - C17  | 18.33 (19)               |
| C10 - C11 - C12 - C13  | 2.2 (2)                   | $C_{9}$ $C_{10}$ $C_{22}$ $C_{17}$   | -104./4 (16)             |
| C10—C11—C12—C13  | -1/8.44 (15)              | C11—C10—C22—C21  | -163.73 (13)             |

# supporting information

| O4—C12—C13—C14                         | 149.58 (17) | C9—C10—C22—C21 |             | 73.20 (17) |
|--|-------------|----------------|-------------|------------|
| Hydrogen-bond geometry (Å, °)          |             |                |             |            |
| D—H···A                                | <i>D</i> —Н | H···A          | D····A      | D—H…A      |
| C15—H15 <i>B</i> ····O4 <sup>i</sup>   | 0.97        | 2.44           | 3.3487 (19) | 156        |
| C18—H18A…O5 <sup>i</sup>               | 0.97        | 2.45           | 3.3821 (19) | 162        |
| Symmetry code: (i) $x+1$ , $y$ , $z$ . |             |                |             |            |

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