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## 2,4-Bis(2-bromophenyl)-7-tert-pentyl-3azabicyclo[3.3.1]nonan-9-one

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Key indicators: single-crystal X-ray study; T = 298 K; mean  $\sigma$ (C–C) = 0.008 Å; R factor = 0.062; wR factor = 0.212; data-to-parameter ratio = 23.2.

The title compound, C<sub>25</sub>H<sub>29</sub>Br<sub>2</sub>NO, is a *tert*-pentyl analog of 2,4-bis(2-bromophenyl)-3-azabicyclo[3.3.1]nonan-9-one [Parthiban et al. (2008). Acta Cryst. E64, o2385]. Similar to its analog, the title compound exists in a twin-chair conformation with an equatorial orientation of the 2-bromophenyl groups. The benzene rings are inclined to each other at a dihedral angle of 29.6  $(3)^{\circ}$ . The *tert*-pentyl group on the cyclohexanone ring also adopts an exocyclic equatorial disposition.

### **Related literature**

For the synthesis, stereochemistry and biological activity of 3azabicyclo[3.3.1]nonan-9-ones, see: Park et al. (2011, 2012a). For the crystal structure of closely related compound, see: Parthiban et al. (2008). For examples of azabicycles with different conformations, see: Parthiban et al. (2010); Park et al. (2012b); Padegimas & Kovacic (1972).



## **Experimental**

#### Crystal data

| $C_{25}H_{29}Br_2NO$             | $\gamma = 97.112 \ (4)^{\circ}$           |
|----------------------------------|---|
| $M_r = 519.31$                   | V = 1151.08 (18) Å <sup>3</sup>           |
| Triclinic, P1                    | Z = 2                                     |
| a = 7.7342 (7) Å                 | Mo $K\alpha$ radiation                    |
| b = 10.6409 (10)  Å              | $\mu = 3.54 \text{ mm}^{-1}$              |
| c = 15.0924 (12) Å               | $T = 298  { m K}$                         |
| $\alpha = 105.856 \ (4)^{\circ}$ | $0.18 \times 0.15 \times 0.10 \text{ mm}$ |
| $\beta = 101.242 \ (4)^{\circ}$  |   |

#### Data collection

Bruker APEXII CCD area-detector diffractometer Absorption correction: multi-scan (SADABS: Bruker, 2004)  $T_{\min} = 0.569, T_{\max} = 0.719$ 

## Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.062$  $wR(F^2) = 0.212$ S = 1.026006 reflections 259 parameters

16189 measured reflections 6006 independent reflections 3081 reflections with  $I > 2\sigma(I)$  $R_{\rm int} = 0.047$ 

1 restraint H-atom parameters constrained  $\Delta \rho_{\rm max} = 1.24 \text{ e} \text{ Å}^{-1}$  $\Delta \rho_{\rm min} = -1.26$  e Å<sup>-3</sup>

Data collection: APEX2 (Bruker, 2004); cell refinement: APEX2 and SAINT-Plus (Bruker, 2004); data reduction: SAINT-Plus and XPREP (Bruker, 2004); program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: ORTEP-3 (Farrugia, 1997); software used to prepare material for publication: SHELXL97.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: CV5341).

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## S1. Comment

The bycyclic compounds posses three major conformations, *viz.*, chair-chair (Parthiban *et al.*, 2010), chair-boat (Park *et al.*, 2012*b*) and boat-boat (Padegimas & Kovacic, 1972), depending upon the nature and position of the substituents on the bicycle. The aim of the present study was to explore the stereochemistry as well as the impact of *tert*-pentyl on the twin-chair conformation of the 2,4-*bis*(2-bromophenyl)-3-azabicyclo[3.3.1]nonan-9-one (Parthiban *et al.*, 2008).

Examination of the asymmery parameters and torsion angles of the title compound (Fig. 1) reveals that the values are very similar to those in its analog. In detail, the torsion angles of the title compound C2—C8—C6—C7, C1—C2—C8—C6, C5—C6—C8—C2 and C3—C2—C8—C6 are -61.2 (5), 61.9 (5), 63.4 (5) and -63.8 (5)°, respectively. These clearly assign slightly distorted chair conformation to both six-membered rings, and the cyclohexanone ring is compratively flattened. Furthermore, the orientation of the bromophenyl groups on both sides of the secondary amino group is identified by their torsion angles. The torsion angle of C9—C1—C2—C8 and C8—C6—C7—C15 are 178.0 (4) and -178.6 (4)°, respectively. This clearly conform their euatorial orientations, and it is similar to its non-*tert*-pentyl analog [C9—C1—C2—C8 and C8—C6—C7—C15 are 177.8 (4) and -179.4 (6)°, respectively]. Also the orientation of *tert*-pentyl group on the cyclohexanone ring is identified by its torsion angles [C21—C4—C5—C6 and C2—C3—C4—C21 are 171.4 (4) and -172.2 (4)°, respectively]. In addition to the above similarities, the title compound and its analog's benzene rings orientations are very similar. In title compound, C<sub>25</sub>H<sub>29</sub>Br<sub>2</sub>NO, exists in a twin-chair conformation with an euatorial orientation of the *ortho*-bromophenyl groups as its non-*tert*-pentyl analog. The *tert*-pentyl group on the cyclohexnone also adopts an exocyclic equtorial disposition.

### **S2. Experimental**

The 2,4-bis(2-bromophenyl)-7-(*tert*-pentyl) -3-azabicyclo[3.3.1]nonan-9-one was synthesized by a modified and an optimized Mannich condensation in one-pot, using 2-bromobenzaldehyde (0.1 mol, 18.50 g/11.58 ml), 4-*tert*-pentylcyclo-hexanone (0.05 mol, 8.41 g/9.15 ml) and ammonium acetate (0.075 mol, 5.78 g) in a 50 ml of absolute ethanol (Park *et al.*, 2011). The mixture was gently warmed on a hot plate at 303–308 K (30–35° C) with moderate stirring till the complete consumption of the starting materials, which was monitored by TLC. At the end, the crude azabicyclic ketone was separated by filtration and gently washed with 1:5 cold ethanol-ether mixture. X-ray diffraction quality crystals of the title compound were obtained by slow evaporation from ethanol.

## **S3. Refinement**

All hydrogen atoms were fixed geometrically and allowed to ride on the parent carbon atoms with aromatic C—H = 0.93 Å, aliphatic C—H = 0.98 Å, methylene C—H = 0.97 Å. The displacement parameters were set for phenyl, methylene and aliphatic H atoms at  $U_{iso}(H) = 1.2U_{eq}(C)$ , methyl H atoms at  $U_{iso}(H) = 1.5U_{eq}(C)$  and the hydrogen atoms were fixed

geometrically and allowed to ride on the parent nitrogen atom with N—H = 0.86 Å and the displacement parameter was set at  $U_{iso}(H)=1.2U_{eq}(N)$ .



Figure 1

The molecular structure of the title compound showing the atomic numbering and displacement ellipsoids drawn at the 30% probability level.

2,4-Bis(2-bromophenyl)-7-tert-pentyl-3-azabicyclo[3.3.1]nonan-9-one

Crystal data

Z = 2 $C_{25}H_{29}Br_2NO$  $M_r = 519.31$ F(000) = 528Triclinic,  $P\overline{1}$  $D_{\rm x} = 1.498 {\rm Mg m^{-3}}$ Hall symbol: -P 1 Mo *K* $\alpha$  radiation,  $\lambda = 0.71073$  Å a = 7.7342 (7) ÅCell parameters from 4160 reflections b = 10.6409 (10) Å $\theta = 2.7 - 22.8^{\circ}$ c = 15.0924 (12) Å $\mu = 3.54 \text{ mm}^{-1}$ T = 298 K $\alpha = 105.856 (4)^{\circ}$  $\beta = 101.242 \ (4)^{\circ}$ Prism, colourless  $\gamma = 97.112 \ (4)^{\circ}$  $0.18 \times 0.15 \times 0.10 \text{ mm}$  $V = 1151.08 (18) Å^3$ Data collection Bruker APEXII CCD area-detector 16189 measured reflections diffractometer 6006 independent reflections Radiation source: fine-focus sealed tube 3081 reflections with  $I > 2\sigma(I)$  $R_{\rm int} = 0.047$ Graphite monochromator phi and  $\omega$  scans  $\theta_{\rm max} = 29.5^{\circ}, \ \theta_{\rm min} = 1.4^{\circ}$  $h = -10 \rightarrow 10$ Absorption correction: multi-scan (SADABS; Bruker, 2004)  $k = -14 \rightarrow 14$  $T_{\min} = 0.569, T_{\max} = 0.719$  $l = -20 \rightarrow 19$ 

Refinement

| Refinement on $F^2$<br>Least-squares matrix: full<br>$R[F^2 > 2\sigma(F^2)] = 0.062$<br>$wR(F^2) = 0.212$ | Secondary atom site location: difference Fourier<br>map<br>Hydrogen site location: inferred from<br>neighbouring sites |
|---|--|
| S = 1.02  | H-atom parameters constrained  |
| 6006 reflections<br>259 parameters  | $w = 1/[\sigma^2(F_o^2) + (0.117P)^2]$<br>where $P = (F_o^2 + 2F_o^2)/3$   |
| 1 restraint   | $(\Delta/\sigma)_{\rm max} = 0.001$  |
| Primary atom site location: structure-invariant direct methods  | $\Delta  ho_{ m max} = 1.24$ e Å <sup>-3</sup><br>$\Delta  ho_{ m min} = -1.26$ e Å <sup>-3</sup>                      |

## Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes. **Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on *F*, and *R*-factors based on ALL data will be even larger.

|     | x           | у           | Ζ           | $U_{ m iso}$ */ $U_{ m eq}$ |  |
|-----|-------------|-------------|-------------|-----------------------------|--|
| Br1 | 0.86819 (8) | 0.90205 (5) | 0.32088 (5) | 0.0717 (3)                  |  |
| Br2 | 0.85323 (8) | 0.28410 (7) | 0.51276 (4) | 0.0732 (3)                  |  |
| C1  | 0.6565 (6)  | 0.6164 (4)  | 0.3068 (3)  | 0.0411 (10)                 |  |
| H1  | 0.7614      | 0.6679      | 0.3573      | 0.049*                      |  |
| C2  | 0.7228 (6)  | 0.5383 (4)  | 0.2223 (3)  | 0.0440 (11)                 |  |
| H2  | 0.8022      | 0.6010      | 0.2042      | 0.053*                      |  |
| C3  | 0.5766 (7)  | 0.4547 (4)  | 0.1333 (3)  | 0.0486 (12)                 |  |
| H3A | 0.4990      | 0.5124      | 0.1143      | 0.058*                      |  |
| H3B | 0.6342      | 0.4219      | 0.0822      | 0.058*                      |  |
| C4  | 0.4601 (7)  | 0.3360 (4)  | 0.1455 (3)  | 0.0456 (11)                 |  |
| H4  | 0.3820      | 0.3730      | 0.1857      | 0.055*                      |  |
| C5  | 0.5749 (7)  | 0.2611 (4)  | 0.1995 (3)  | 0.0474 (12)                 |  |
| H5A | 0.6321      | 0.2059      | 0.1558      | 0.057*                      |  |
| H5B | 0.4959      | 0.2021      | 0.2195      | 0.057*                      |  |
| C6  | 0.7214 (6)  | 0.3469 (4)  | 0.2870 (3)  | 0.0441 (11)                 |  |
| H6  | 0.7977      | 0.2894      | 0.3093      | 0.053*                      |  |
| C7  | 0.6514 (6)  | 0.4244 (4)  | 0.3698 (3)  | 0.0408 (10)                 |  |
| H7  | 0.7552      | 0.4716      | 0.4223      | 0.049*                      |  |
| C8  | 0.8320 (7)  | 0.4438 (4)  | 0.2566 (3)  | 0.0462 (11)                 |  |
| С9  | 0.5400 (6)  | 0.7115 (4)  | 0.2822 (3)  | 0.0405 (10)                 |  |
| C10 | 0.6147 (7)  | 0.8408 (4)  | 0.2862 (3)  | 0.0461 (11)                 |  |

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

| C11  | 0.5088 (10) | 0.9304 (5)  | 0.2667 (4)  | 0.0670 (16) |
|------|-------------|-------------|-------------|-------------|
| H11  | 0.5618      | 1.0158      | 0.2708      | 0.080*      |
| C12  | 0.3248 (9)  | 0.8927 (6)  | 0.2414 (5)  | 0.0755 (18) |
| H12  | 0.2527      | 0.9530      | 0.2298      | 0.091*      |
| C13  | 0.2472 (8)  | 0.7627 (6)  | 0.2332 (4)  | 0.0676 (16) |
| H13  | 0.1235      | 0.7341      | 0.2130      | 0.081*      |
| C14  | 0.3574 (7)  | 0.6776 (5)  | 0.2555 (4)  | 0.0531 (13) |
| H14  | 0.3042      | 0.5925      | 0.2521      | 0.064*      |
| C15  | 0.5335 (6)  | 0.3345 (4)  | 0.4043 (3)  | 0.0384 (10) |
| C16  | 0.3459 (6)  | 0.3148 (5)  | 0.3759 (3)  | 0.0483 (11) |
| H16  | 0.2941      | 0.3628      | 0.3382      | 0.058*      |
| C17  | 0.2358 (8)  | 0.2263 (6)  | 0.4020 (4)  | 0.0596 (14) |
| H17  | 0.1119      | 0.2140      | 0.3809      | 0.072*      |
| C18  | 0.3103 (8)  | 0.1554 (5)  | 0.4598 (4)  | 0.0586 (14) |
| H18  | 0.2364      | 0.0954      | 0.4773      | 0.070*      |
| C19  | 0.4926 (8)  | 0.1744 (4)  | 0.4908 (3)  | 0.0509 (12) |
| H19  | 0.5431      | 0.1276      | 0.5298      | 0.061*      |
| C20  | 0.6015 (6)  | 0.2631 (4)  | 0.4641 (3)  | 0.0415 (10) |
| N1   | 0.5541 (5)  | 0.5240 (3)  | 0.3436 (3)  | 0.0413 (9)  |
| H1A  | 0.4463      | 0.5282      | 0.3493      | 0.050*      |
| 01   | 0.9910 (5)  | 0.4487 (4)  | 0.2582 (3)  | 0.0695 (10) |
| C21  | 0.3326 (9)  | 0.2448 (5)  | 0.0486 (4)  | 0.0732 (18) |
| C24  | 0.2293 (15) | 0.1222 (10) | 0.0634 (7)  | 0.155 (4)   |
| H24A | 0.3131      | 0.0784      | 0.0950      | 0.186*      |
| H24B | 0.1656      | 0.0598      | 0.0023      | 0.186*      |
| C22  | 0.1993 (13) | 0.3238 (9)  | 0.0052 (6)  | 0.151 (5)   |
| H22A | 0.1380      | 0.2718      | -0.0585     | 0.226*      |
| H22B | 0.2649      | 0.4062      | 0.0046      | 0.226*      |
| H22C | 0.1133      | 0.3417      | 0.0429      | 0.226*      |
| C25  | 0.0936 (15) | 0.1639 (10) | 0.1242 (7)  | 0.155 (4)   |
| H25A | 0.1470      | 0.2459      | 0.1736      | 0.232*      |
| H25B | 0.0624      | 0.0959      | 0.1521      | 0.232*      |
| H25C | -0.0126     | 0.1758      | 0.0847      | 0.232*      |
| C23  | 0.4459 (12) | 0.1841 (8)  | -0.0222 (5) | 0.113 (3)   |
| H23A | 0.5272      | 0.1372      | 0.0065      | 0.169*      |
| H23B | 0.5130      | 0.2542      | -0.0373     | 0.169*      |
| H23C | 0.3671      | 0.1237      | -0.0792     | 0.169*      |
|      |             |             |             |             |

Atomic displacement parameters  $(Å^2)$ 

|     | $U^{11}$   | $U^{22}$   | $U^{33}$   | $U^{12}$     | $U^{13}$   | $U^{23}$    |
|-----|------------|------------|------------|--------------|------------|-------------|
| Br1 | 0.0725 (4) | 0.0449 (3) | 0.0923 (5) | -0.0143 (3)  | 0.0195 (3) | 0.0238 (3)  |
| Br2 | 0.0604 (4) | 0.0956 (5) | 0.0726 (5) | 0.0205 (3)   | 0.0054 (3) | 0.0452 (4)  |
| C1  | 0.045 (3)  | 0.026 (2)  | 0.051 (3)  | -0.0006 (18) | 0.012 (2)  | 0.0140 (18) |
| C2  | 0.047 (3)  | 0.035 (2)  | 0.056 (3)  | 0.0005 (19)  | 0.024 (2)  | 0.021 (2)   |
| C3  | 0.067 (3)  | 0.035 (2)  | 0.049 (3)  | 0.005 (2)    | 0.021 (2)  | 0.019 (2)   |
| C4  | 0.060 (3)  | 0.034 (2)  | 0.045 (3)  | 0.002 (2)    | 0.015 (2)  | 0.018 (2)   |
| C5  | 0.070 (3)  | 0.028 (2)  | 0.050 (3)  | 0.007 (2)    | 0.021 (2)  | 0.0159 (19) |
|     |            |            |            |              |            |             |

| C6  | 0.049 (3) | 0.039 (2)   | 0.054 (3) | 0.013 (2)   | 0.017 (2)   | 0.023 (2)   |
|-----|-----------|-------------|-----------|-------------|-------------|-------------|
| C7  | 0.050 (3) | 0.034 (2)   | 0.040 (3) | 0.0032 (19) | 0.011 (2)   | 0.0167 (19) |
| C8  | 0.047 (3) | 0.041 (3)   | 0.053 (3) | 0.009 (2)   | 0.020 (2)   | 0.014 (2)   |
| C9  | 0.054 (3) | 0.028 (2)   | 0.044 (3) | 0.0075 (19) | 0.020(2)    | 0.0130 (18) |
| C10 | 0.068 (3) | 0.031 (2)   | 0.045 (3) | 0.008 (2)   | 0.024 (2)   | 0.0141 (19) |
| C11 | 0.111 (5) | 0.039 (3)   | 0.066 (4) | 0.019 (3)   | 0.037 (3)   | 0.027 (3)   |
| C12 | 0.080 (4) | 0.077 (4)   | 0.103 (5) | 0.043 (4)   | 0.042 (4)   | 0.055 (4)   |
| C13 | 0.061 (4) | 0.079 (4)   | 0.080 (4) | 0.027 (3)   | 0.028 (3)   | 0.040 (3)   |
| C14 | 0.053 (3) | 0.041 (3)   | 0.072 (4) | 0.007 (2)   | 0.021 (3)   | 0.025 (2)   |
| C15 | 0.045 (3) | 0.031 (2)   | 0.040 (3) | 0.0051 (18) | 0.013 (2)   | 0.0095 (18) |
| C16 | 0.043 (3) | 0.044 (3)   | 0.063 (3) | 0.007 (2)   | 0.015 (2)   | 0.024 (2)   |
| C17 | 0.050 (3) | 0.064 (3)   | 0.064 (3) | -0.003 (3)  | 0.014 (3)   | 0.025 (3)   |
| C18 | 0.075 (4) | 0.046 (3)   | 0.055 (3) | -0.007 (3)  | 0.025 (3)   | 0.018 (2)   |
| C19 | 0.076 (4) | 0.039 (3)   | 0.043 (3) | 0.008 (2)   | 0.018 (2)   | 0.019 (2)   |
| C20 | 0.053 (3) | 0.036 (2)   | 0.041 (3) | 0.014 (2)   | 0.016 (2)   | 0.0135 (19) |
| N1  | 0.046 (2) | 0.0310 (18) | 0.057 (2) | 0.0084 (16) | 0.0239 (18) | 0.0205 (17) |
| 01  | 0.050 (2) | 0.078 (3)   | 0.096 (3) | 0.019 (2)   | 0.033 (2)   | 0.039 (2)   |
| C21 | 0.095 (5) | 0.049 (3)   | 0.062 (4) | -0.017 (3)  | 0.001 (3)   | 0.021 (3)   |
| C24 | 0.197 (9) | 0.131 (6)   | 0.100 (5) | -0.054 (6)  | 0.005 (4)   | 0.034 (5)   |
| C22 | 0.179 (9) | 0.106 (6)   | 0.120 (7) | -0.064 (6)  | -0.080 (6)  | 0.078 (5)   |
| C25 | 0.197 (9) | 0.131 (6)   | 0.100 (5) | -0.054 (6)  | 0.005 (4)   | 0.034 (5)   |
| C23 | 0.160 (8) | 0.107 (6)   | 0.041 (4) | -0.016 (5)  | 0.017 (4)   | -0.004 (3)  |
|     |           |             |           |             |             |             |

## Geometric parameters (Å, °)

| Br1—C10 | 1.908 (5) | C12—H12  | 0.9300     |
|---------|-----------|----------|------------|
| Br2-C20 | 1.904 (5) | C13—C14  | 1.380 (7)  |
| C1—N1   | 1.476 (5) | C13—H13  | 0.9300     |
| C1—C9   | 1.507 (6) | C14—H14  | 0.9300     |
| C1—C2   | 1.537 (7) | C15—C20  | 1.400 (6)  |
| C1—H1   | 0.9800    | C15—C16  | 1.402 (6)  |
| C2—C8   | 1.521 (6) | C16—C17  | 1.379 (7)  |
| C2—C3   | 1.542 (7) | C16—H16  | 0.9300     |
| С2—Н2   | 0.9800    | C17—C18  | 1.390 (8)  |
| C3—C4   | 1.534 (6) | C17—H17  | 0.9300     |
| С3—НЗА  | 0.9700    | C18—C19  | 1.367 (7)  |
| С3—Н3В  | 0.9700    | C18—H18  | 0.9300     |
| C4—C5   | 1.528 (6) | C19—C20  | 1.381 (6)  |
| C4—C21  | 1.574 (7) | C19—H19  | 0.9300     |
| C4—H4   | 0.9800    | N1—H1A   | 0.8600     |
| C5—C6   | 1.538 (6) | C21—C24  | 1.537 (10) |
| С5—Н5А  | 0.9700    | C21—C22  | 1.565 (11) |
| С5—Н5В  | 0.9700    | C21—C23  | 1.567 (10) |
| C6—C8   | 1.483 (6) | C24—C25  | 1.553 (12) |
| C6—C7   | 1.531 (6) | C24—H24A | 0.9700     |
| С6—Н6   | 0.9800    | C24—H24B | 0.9700     |
| C7—N1   | 1.468 (6) | C22—H22A | 0.9600     |
| C7—C15  | 1.503 (6) | C22—H22B | 0.9600     |
|         |           |          |            |

| С7—Н7                           | 0.9800               | C22—H22C   | 0.9600             |
|---------------------------------|----------------------|--|--------------------|
| C8—O1                           | 1.220 (6)            | C25—H25A   | 0.9600             |
| C9—C14                          | 1.364 (7)            | С25—Н25В   | 0.9600             |
| C9—C10                          | 1.406 (6)            | C25—H25C   | 0.9600             |
| C10—C11                         | 1 385 (7)            | C23—H23A   | 0 9600             |
|                                 | 1.305(7)<br>1.376(8) | C23 H23B   | 0.9600             |
| C11_U11                         | 0.0200               | C23—1125B  | 0.9000             |
|                                 | 0.9300               | C23—n23C   | 0.9000             |
| C12—C13                         | 1.401 (8)            |  |                    |
| N1                              | 108 6 (4)            | C14 - C13 - C12  | 119.0 (6)          |
| N1 = C1 = C2                    | 100.0(4)             | $C_{14} = C_{13} = C_{12}$   | 120.5              |
| NI = CI = C2                    | 110.2(3)             | $C_{14} - C_{13} - H_{13}$   | 120.5              |
| C9—C1—C2                        | 113.0 (4)            |  | 120.5              |
| NI—CI—HI                        | 108.3                | C9—C14—C13   | 123.5 (5)          |
| С9—С1—Н1                        | 108.3                | C9—C14—H14   | 118.2              |
| C2—C1—H1                        | 108.3                | C13—C14—H14  | 118.2              |
| C8—C2—C1                        | 107.1 (4)            | C20-C15-C16  | 115.7 (4)          |
| C8—C2—C3                        | 107.6 (4)            | C20—C15—C7   | 123.0 (4)          |
| C1—C2—C3                        | 116.3 (4)            | C16—C15—C7   | 121.3 (4)          |
| C8—C2—H2                        | 108.5                | C17—C16—C15  | 122.0 (4)          |
| C1—C2—H2                        | 108.5                | C17—C16—H16  | 119.0              |
| C3—C2—H2                        | 108.5                | C15—C16—H16  | 119.0              |
| $C_4 - C_3 - C_2$               | 115.2(4)             | $C_{16}$ $C_{17}$ $C_{18}$   | 120.0(5)           |
| $C_4 = C_3 = C_2$               | 108.5                | $C_{10} = C_{17} = C_{10}$   | 120.0 (3)          |
| $C_{4}$                         | 100.5                | $C_{10} = C_{17} = H_{17}$   | 120.0              |
| C2—C3—H3A                       | 108.5                |  | 120.0              |
| С4—С3—Н3В                       | 108.5                | C19—C18—C17  | 119.7 (5)          |
| С2—С3—Н3В                       | 108.5                | C19—C18—H18  | 120.1              |
| НЗА—СЗ—НЗВ                      | 107.5                | C17—C18—H18  | 120.1              |
| C5—C4—C3                        | 111.0 (4)            | C18—C19—C20  | 119.8 (5)          |
| C5-C4-C21                       | 114.0 (4)            | C18—C19—H19  | 120.1              |
| C3—C4—C21                       | 112.0 (4)            | С20—С19—Н19  | 120.1              |
| C5—C4—H4                        | 106.4                | C19—C20—C15  | 122.7 (5)          |
| C3—C4—H4                        | 106.4                | C19—C20—Br2  | 116.5 (3)          |
| C21—C4—H4                       | 106.4                | C15—C20—Br2  | 120.8(3)           |
| C4-C5-C6                        | 1163(4)              | C7—N1—C1   | 1145(4)            |
| C4 - C5 - H5A                   | 108.2                | C7—N1—H1A  | 122.7              |
| C6 C5 H5A                       | 108.2                | $C_1 $ N1 H1A  | 122.7              |
| $C_{0}$ $C_{5}$ $H_{5}$ $H_{5}$ | 108.2                | $C_1 = N_1 = M_1 $ | 122.7<br>110 5 (7) |
|                                 | 108.2                | $C_{24} = C_{21} = C_{22}$   | 110.3(7)           |
|                                 | 108.2                | $C_{24} = C_{21} = C_{23}$   | 103.0 (0)          |
| H5A—C5—H5B                      | 107.4                | C22—C21—C23  | 111.4 (/)          |
| C8-C6-C7                        | 108.2 (4)            | C24—C21—C4   | 109.9 (5)          |
| C8—C6—C5                        | 107.5 (4)            | C22—C21—C4   | 110.9 (5)          |
| C7—C6—C5                        | 114.9 (4)            | C23—C21—C4   | 110.3 (5)          |
| С8—С6—Н6                        | 108.7                | C21—C24—C25  | 110.3 (8)          |
| С7—С6—Н6                        | 108.7                | C21—C24—H24A   | 109.6              |
| С5—С6—Н6                        | 108.7                | C25—C24—H24A   | 109.6              |
| N1—C7—C15                       | 109.9 (4)            | C21—C24—H24B   | 109.6              |
| N1—C7—C6                        | 111.0 (3)            | C25—C24—H24B   | 109.6              |
| C15—C7—C6                       | 112.2 (3)            | H24A—C24—H24B  | 108.1              |

| N1—C7—H7                           | 107.9     | C21—C22—H22A                      | 109.5      |
|------------------------------------|-----------|-----------------------------------|------------|
| С15—С7—Н7                          | 107.9     | C21—C22—H22B                      | 109.5      |
| С6—С7—Н7                           | 107.9     | H22A—C22—H22B                     | 109.5      |
| O1—C8—C6                           | 125.0 (4) | C21—C22—H22C                      | 109.5      |
| O1—C8—C2                           | 123.3 (4) | H22A—C22—H22C                     | 109.5      |
| C6—C8—C2                           | 111.7 (4) | H22B—C22—H22C                     | 109.5      |
| C14—C9—C10                         | 116.3 (4) | C24—C25—H25A                      | 109.5      |
| C14—C9—C1                          | 122.2 (4) | C24—C25—H25B                      | 109.5      |
| C10-C9-C1                          | 121.5 (4) | H25A—C25—H25B                     | 109.5      |
| C11—C10—C9                         | 122.0 (5) | C24—C25—H25C                      | 109.5      |
| C11—C10—Br1                        | 116.8 (4) | H25A—C25—H25C                     | 109.5      |
| C9—C10—Br1                         | 121.2 (4) | H25B—C25—H25C                     | 109.5      |
| C12—C11—C10                        | 119.8 (5) | C21—C23—H23A                      | 109.5      |
| C12—C11—H11                        | 120.1     | C21—C23—H23B                      | 109.5      |
| C10-C11-H11                        | 120.1     | H23A—C23—H23B                     | 109.5      |
| C11—C12—C13                        | 119.4 (5) | C21—C23—H23C                      | 109.5      |
| C11—C12—H12                        | 120.3     | H23A—C23—H23C                     | 109.5      |
| C13—C12—H12                        | 120.3     | H23B—C23—H23C                     | 109.5      |
|                                    |           |                                   |            |
| N1—C1—C2—C8                        | -56.2(5)  | C10-C11-C12-C13                   | -1.7(9)    |
| C9—C1—C2—C8                        | -178.0(4) | C11—C12—C13—C14                   | 3.2 (9)    |
| N1—C1—C2—C3                        | 64.1 (5)  | C10—C9—C14—C13                    | -0.1 (8)   |
| C9—C1—C2—C3                        | -57.7 (5) | C1—C9—C14—C13                     | 179.5 (5)  |
| C8—C2—C3—C4                        | 52.9 (5)  | C12—C13—C14—C9                    | -2.4 (9)   |
| C1—C2—C3—C4                        | -67.2(5)  | N1—C7—C15—C20                     | -156.6 (4) |
| C2—C3—C4—C5                        | -43.5 (5) | C6—C7—C15—C20                     | 79.4 (5)   |
| C2—C3—C4—C21                       | -172.2(4) | N1—C7—C15—C16                     | 25.0 (6)   |
| C3—C4—C5—C6                        | 43.8 (5)  | C6-C7-C15-C16                     | -99.0(5)   |
| C21—C4—C5—C6                       | 171.4 (4) | C20—C15—C16—C17                   | -2.7(7)    |
| C4—C5—C6—C8                        | -53.5(5)  | C7—C15—C16—C17                    | 175.8 (5)  |
| C4-C5-C6-C7                        | 67.0 (5)  | C15-C16-C17-C18                   | 1.3 (8)    |
| C8—C6—C7—N1                        | 55.2 (5)  | C16—C17—C18—C19                   | 0.3 (8)    |
| $C_{5}$ $C_{6}$ $C_{7}$ $N_{1}$    | -64.8(5)  | C17 - C18 - C19 - C20             | -0.4(8)    |
| C8—C6—C7—C15                       | 178.6 (4) | C18 - C19 - C20 - C15             | -1.1(7)    |
| $C_{5}$ $C_{6}$ $C_{7}$ $C_{15}$   | 58.6 (5)  | C18 - C19 - C20 - Br2             | 179.1 (4)  |
| C7—C6—C8—O1                        | 118.8 (5) | C16-C15-C20-C19                   | 2.6 (6)    |
| C5-C6-C8-O1                        | -116.6(5) | C7-C15-C20-C19                    | -175.9(4)  |
| C7—C6—C8—C2                        | -61.2(5)  | $C16-C15-C20-Br^{2}$              | -177.6(3)  |
| C5-C6-C8-C2                        | 63.4 (5)  | C7-C15-C20-Br2                    | 3.9 (6)    |
| C1 - C2 - C8 - O1                  | -118.1(5) | C15—C7—N1—C1                      | -178.9(3)  |
| $C_{3}$ $C_{2}$ $C_{8}$ $C_{1}$    | 116.2 (5) | C6-C7-N1-C1                       | -542(5)    |
| C1 - C2 - C8 - C6                  | 61.9 (5)  | C9-C1-N1-C7                       | 179.5 (3)  |
| $C_{3}$ $C_{2}$ $C_{8}$ $C_{6}$    | -638(5)   | $C^{2}-C^{1}-N^{1}-C^{7}$         | 55 1 (5)   |
| N1-C1-C9-C14                       | -28.3(6)  | $C_{5}$ $C_{4}$ $C_{21}$ $C_{24}$ | 48.8 (8)   |
| C2-C1-C9-C14                       | 94.4 (5)  | $C_{3}$ $C_{4}$ $C_{21}$ $C_{24}$ | 175 8 (6)  |
| $N_1 - C_1 - C_9 - C_{10}$         | 151.3 (4) | $C_{5}$ $C_{4}$ $C_{21}$ $C_{22}$ | 1714(6)    |
| $C_2 - C_1 - C_9 - C_{10}$         | -86.0(5)  | $C_{3}$ $C_{4}$ $C_{21}$ $C_{22}$ | -61.6(7)   |
| $C_{14}$ $C_{9}$ $C_{10}$ $C_{11}$ | 18(7)     | $C_{5} - C_{4} - C_{21} - C_{23}$ | -64.8(6)   |
|                                    | 1.0 ( / ) |                                   | 07.0(0)    |

| C1—C9—C10—C11   | -177.9 (4) | C3—C4—C21—C23   | 62.3 (6)   |
|-----------------|------------|-----------------|------------|
| C14—C9—C10—Br1  | -179.2 (4) | C22—C21—C24—C25 | -54.6 (10) |
| C1C9C10Br1      | 1.1 (6)    | C23—C21—C24—C25 | -174.0 (8) |
| C9—C10—C11—C12  | -0.9 (8)   | C4—C21—C24—C25  | 68.2 (10)  |
| Br1-C10-C11-C12 | -179.9 (5) |                 |            |