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5"-Benzylidene-1"-methyl-1'-phenyl-1',2',3',5',6',7',8',8a'-octahydrodispiro-[acenaphthylene-1,3'-indolizine-2',3"piperidine]-2,4"(1*H*)-dione

J. Suresh,^a R. A. Nagalakshmi,^a R. Ranjith Kumar,^b S. Sivakumar^b and P. L. Nilantha Lakshman^c*

^aDepartment of Physics, The Madura College, Madurai 625 011, India, ^bDepartment of Organic Chemistry, School of Chemistry, Madurai Kamaraj University, Madurai 625 021, India, and ^cDepartment of Food Science and Technology, University of Ruhuna, Mapalana, Kamburupitiya 81100, Sri Lanka Correspondence e-mail: plakshmannilantha@ymail.com

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Key indicators: single-crystal X-ray study; T = 293 K; mean σ (C–C) = 0.002 Å; R factor = 0.053; wR factor = 0.157; data-to-parameter ratio = 25.2.

In the title compound, $C_{37}H_{34}N_2O_2$, the pyridinone ring adopts a half-chair conformation. In the octahydroindolizine fused-ring system, the piperidine ring is in a chair conformation and the pyrrole ring is twisted about the N-C(piperidine) bond. The molecular structure features a weak intramolecular C-H···O interaction.

Related literature

For the importance of spiro compounds, see: Gubin *et al.* (1992); Liu *et al.* (2007); Molyneux & James (1982); Nash *et al.* (1988); Pearson & Guo (2001); Smith *et al.* (2007). For related acenaphthylene structures, see: Sundar *et al.* (2002). For additional conformational analysis, see: Cremer & Pople (1975).



Experimental

Crystal data

Crystal data	
$C_{37}H_{34}N_2O_2$ $M_r = 538.66$ Monoclinic, $P2_1/c$ $a = 8.4913 (3) Å$ $b = 16.6782 (6) Å$ $c = 20.5435 (7) Å$ $\beta = 100.028 (2)^{\circ}$	$V = 2864.92 (17) Å^{3}$ Z = 4 Mo K\alpha radiation $\mu = 0.08 \text{ mm}^{-1}$ T = 293 K $0.21 \times 0.19 \times 0.18 \text{ mm}$
Data collection	
Bruker Kappa APEXII diffractometer Absorption correction: multi-scan (SADABS; Sheldrick, 1996) $T_{min} = 0.967, T_{max} = 0.974$	43034 measured reflections 9332 independent reflections 5857 reflections with $I > 2\sigma(I)$ $R_{int} = 0.035$
Refinement	
$R[F^2 > 2\sigma(F^2)] = 0.053$ wR(F ²) = 0.157 S = 1.03 9332 reflections	371 parameters H-atom parameters constrained $\Delta \rho_{\text{max}} = 0.29 \text{ e } \text{\AA}^{-3}$ $\Delta \rho_{\text{min}} = -0.23 \text{ e } \text{\AA}^{-3}$

Table 1

Hydrogen-bond	geometry (Å,	, °).

$D - H \cdots A$	D-H	$H \cdot \cdot \cdot A$	$D \cdots A$	$D - \mathbf{H} \cdot \cdot \cdot A$
$C2-H2B\cdots O2$	0.97	2.35	2.9329 (18)	118

Data collection: *APEX2* (Bruker, 2004); cell refinement: *SAINT* (Bruker, 2004); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *PLATON* (Spek, 2009); software used to prepare material for publication: *SHELXL97*.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: TK5152).

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5''-Benzylidene-1''-methyl-1'-phenyl-1',2',3',5',6',7',8',8a'-octahydrodispiro-[acenaphthylene-1,3'-indolizine-2',3''-piperidine]-2,4''(1*H*)-dione

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S1. Comment

Spiro indolizine derivatives have been found to possess a variety of biological activities such as antibacterial, antiinflammatory, antiviral, (Nash *et al.*, 1988; Molyneux & James, 1982), anticancer (Liu *et al.*, 2007; Smith *et al.*, 2007) and antitumor (Pearson & Guo, 2001). They are also important synthetic targets in view of developing new pharmaceuticals for the treatment of cardiovascular diseases (Gubin *et al.*, 1992). In view of the high medicinal value of these compounds in conjunction with our research interests, prompted us to synthesize and report the X-ray studies of the title compound. Related acenaphthylene structures are known (Sundar *et al.*, 2002).

In the title compound (Fig. 1), the pyridinone ring adopts twisted chair conformation with atoms N2 and C3 deviating by -0.6237 (1) and -0.4716 (1) Å, respectively, from the least-squares plane defined by other atoms (C2/C4/C5/C6). Within the octahydroindolizine, the six membered piperidine ring adopts chair conformation as evident from the puckering parameters (Cremer & Pople, 1975): Q = 0.551 (2) Å, θ = 145.92 (2)° and Φ = 223.5 (3)°. The dihedral angle between the two benzene rings and the acenapthalene rings are 70.74 (1) and 34.81 (1) Å. The molecular structure also features a weak intramolecular C—H···O interaction (Table 1).

S2. Experimental

A mixture of 1-methyl-3,5-bis[(E)-arylmethylidene]tetrahydro-4(1H)-pyridinone (1 mmol), acenaphthenequinone (1 mmol) and piperidine-2-carboxylic acid (1 mmol) was dissolved in isopropyl alcohol (15 ml), and heated to reflux for 60 min. After completion of the reaction, as evident from TLC, the mixture was poured into water (50 ml), the precipitated solid was filtered and washed with water (100 ml) to obtain pure yellow solid. Melting point: 479 K, Yield: 89%

S3. Refinement

H atoms were placed at calculated positions and allowed to ride on their carrier atoms with C—H = 0.93–0.98 Å and U_{iso} = 1.2–1.5 U_{eq} (C).





The molecular structure of (I), showing 20% probability displacement ellipsoids and the atom-numbering scheme. Hatoms are omitted for clarity.

5''-Benzylidene-1''-methyl-1'-phenyl-1',2',3',5',6',7',8',8a'- octahydrodispiro[acenaphthylene-1,3'indolizine-2',3''-piperidine]- 2,4''(1*H*)-dione

Crystal data

$C_{37}H_{34}N_2O_2$ $M_r = 538.66$ Monoclinic, $P2_1/c$ Hall symbol: -P 2ybc a = 8.4913 (3) Å b = 16.6782 (6) Å c = 20.5435 (7) Å $\beta = 100.028$ (2)° V = 2864.92 (17) Å ³ Z = 4	F(000) = 1144 $D_x = 1.249 \text{ Mg m}^{-3}$ Mo $K\alpha$ radiation, $\lambda = 0.71073 \text{ Å}$ Cell parameters from 2000 reflections $\theta = 2-31^{\circ}$ $\mu = 0.08 \text{ mm}^{-1}$ T = 293 K Block, yellow $0.21 \times 0.19 \times 0.18 \text{ mm}$
Data collectionBruker Kappa APEXII diffractometerRadiation source: fine-focus sealed tubeGraphite monochromatorDetector resolution: 0 pixels mm ⁻¹ ω and φ scansAbsorption correction: multi-scan $(SADABS; Sheldrick, 1996)$ $T_{min} = 0.967, T_{max} = 0.974$	43034 measured reflections 9332 independent reflections 5857 reflections with $I > 2\sigma(I)$ $R_{int} = 0.035$ $\theta_{max} = 31.3^\circ, \ \theta_{min} = 1.6^\circ$ $h = -12 \rightarrow 12$ $k = -22 \rightarrow 24$ $l = -25 \rightarrow 30$

Refinement

Hydrogen site location: inferred from
neighbouring sites
H-atom parameters constrained
$w = 1/[\sigma^2(F_o^2) + (0.0678P)^2 + 0.5825P]$
where $P = (F_o^2 + 2F_c^2)/3$
$(\Delta/\sigma)_{ m max} < 0.001$
$\Delta ho_{ m max} = 0.29 \ { m e} \ { m \AA}^{-3}$
$\Delta ho_{ m min} = -0.23 \ m e \ m \AA^{-3}$
Extinction correction: <i>SHELXL97</i> (Sheldrick, 2008), $Fc^*=kFc[1+0.001xFc^2\lambda^3/sin(2\theta)]^{-1/4}$
Extinction coefficient: 0.0030 (7)

Special details

Geometry. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on F^2 , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative F^2 . The threshold expression of $F^2 > \sigma(F^2)$ is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on F^2 are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

x	у	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	
0.02236 (11)	0.45746 (6)	0.21716 (5)	0.0463 (3)	
0.18434 (14)	0.27311 (6)	0.30171 (5)	0.0354 (2)	
0.29204 (15)	0.32105 (7)	0.26884 (6)	0.0316 (2)	
0.14839 (15)	0.39871 (7)	0.34350 (6)	0.0311 (2)	
0.0373	0.4034	0.3208	0.037*	
0.50761 (13)	0.45681 (7)	0.26318 (6)	0.0386 (3)	
0.16715 (15)	0.45441 (7)	0.22914 (6)	0.0320 (3)	
0.16991 (16)	0.45865 (8)	0.39942 (7)	0.0370 (3)	
0.54309 (13)	0.29695 (7)	0.34803 (6)	0.0555 (3)	
0.40959 (15)	0.45688 (8)	0.31454 (6)	0.0342 (3)	
0.3840	0.5115	0.3250	0.041*	
0.4676	0.4321	0.3543	0.041*	
0.26458 (17)	0.29985 (8)	0.19575 (6)	0.0364 (3)	
0.19570 (16)	0.50244 (8)	0.12120 (7)	0.0383 (3)	
0.0901	0.4852	0.1108	0.046*	
0.25581 (14)	0.41018 (7)	0.28993 (6)	0.0291 (2)	
0.26203 (17)	0.53783 (8)	0.06646 (7)	0.0406 (3)	
0.1305 (2)	0.30038 (9)	0.14857 (7)	0.0452 (3)	
0.0337	0.3186	0.1582	0.054*	
0.47326 (17)	0.29755 (8)	0.29136 (7)	0.0415 (3)	
0.17403 (16)	0.31133 (7)	0.36444 (6)	0.0341 (3)	
0.2759	0.3056	0.3949	0.041*	
0.26617 (15)	0.49163 (8)	0.18385 (7)	0.0342 (3)	
	x 0.02236 (11) 0.18434 (14) 0.29204 (15) 0.14839 (15) 0.0373 0.50761 (13) 0.16715 (15) 0.16991 (16) 0.54309 (13) 0.40959 (15) 0.3840 0.4676 0.26458 (17) 0.19570 (16) 0.0901 0.25581 (14) 0.26203 (17) 0.1305 (2) 0.0337 0.47326 (17) 0.17403 (16) 0.2759 0.26617 (15)	x y $0.02236 (11)$ $0.45746 (6)$ $0.18434 (14)$ $0.27311 (6)$ $0.29204 (15)$ $0.32105 (7)$ $0.14839 (15)$ $0.39871 (7)$ 0.0373 0.4034 $0.50761 (13)$ $0.45681 (7)$ $0.16715 (15)$ $0.45441 (7)$ $0.16991 (16)$ $0.45865 (8)$ $0.54309 (13)$ $0.29695 (7)$ $0.40959 (15)$ $0.45688 (8)$ 0.3840 0.5115 0.4676 0.4321 $0.26458 (17)$ $0.29985 (8)$ $0.19570 (16)$ $0.50244 (8)$ 0.0901 0.4852 $0.25581 (14)$ $0.41018 (7)$ $0.26203 (17)$ $0.30038 (9)$ 0.0337 0.3186 $0.47326 (17)$ $0.29755 (8)$ $0.17403 (16)$ $0.31133 (7)$ $0.26617 (15)$ $0.49163 (8)$	xyz $0.02236 (11)$ $0.45746 (6)$ $0.21716 (5)$ $0.18434 (14)$ $0.27311 (6)$ $0.30171 (5)$ $0.29204 (15)$ $0.32105 (7)$ $0.26884 (6)$ $0.14839 (15)$ $0.39871 (7)$ $0.34350 (6)$ 0.0373 0.4034 0.3208 $0.50761 (13)$ $0.45681 (7)$ $0.26318 (6)$ $0.16715 (15)$ $0.45441 (7)$ $0.22914 (6)$ $0.16991 (16)$ $0.45865 (8)$ $0.39942 (7)$ $0.54309 (13)$ $0.29695 (7)$ $0.34803 (6)$ $0.40959 (15)$ $0.45688 (8)$ $0.31454 (6)$ 0.3840 0.5115 0.3250 0.4676 0.4321 0.3543 $0.26458 (17)$ $0.29985 (8)$ $0.19575 (6)$ $0.19570 (16)$ $0.50244 (8)$ $0.12120 (7)$ 0.0901 0.4852 0.1108 $0.25581 (14)$ $0.41018 (7)$ $0.28993 (6)$ $0.26203 (17)$ $0.3378 (8)$ $0.06646 (7)$ $0.1305 (2)$ $0.30038 (9)$ $0.14857 (7)$ 0.0337 0.3186 0.1582 $0.47326 (17)$ $0.29755 (8)$ $0.29136 (7)$ $0.17403 (16)$ $0.31133 (7)$ $0.36444 (6)$ 0.2759 0.3056 0.3949 $0.26617 (15)$ $0.49163 (8)$ $0.18385 (7)$	xyz U_{iso}^*/U_{eq} 0.02236 (11)0.45746 (6)0.21716 (5)0.0463 (3)0.18434 (14)0.27311 (6)0.30171 (5)0.0354 (2)0.29204 (15)0.32105 (7)0.26884 (6)0.0316 (2)0.14839 (15)0.39871 (7)0.34350 (6)0.0311 (2)0.03730.40340.32080.037*0.50761 (13)0.45681 (7)0.26318 (6)0.0386 (3)0.16715 (15)0.45441 (7)0.22914 (6)0.0320 (3)0.16715 (15)0.45441 (7)0.22914 (6)0.0370 (3)0.54309 (13)0.29695 (7)0.34803 (6)0.0555 (3)0.40959 (15)0.45688 (8)0.31454 (6)0.0342 (3)0.38400.51150.32500.041*0.46760.43210.35430.041*0.26458 (17)0.29985 (8)0.19575 (6)0.0364 (3)0.19570 (16)0.50244 (8)0.12120 (7)0.0383 (3)0.09010.48520.11080.046*0.25581 (14)0.41018 (7)0.28993 (6)0.0291 (2)0.26203 (17)0.53783 (8)0.06646 (7)0.0406 (3)0.1305 (2)0.30038 (9)0.14857 (7)0.0452 (3)0.03370.31860.15820.054*0.47326 (17)0.29755 (8)0.29136 (7)0.0415 (3)0.17403 (16)0.31133 (7)0.36444 (6)0.0341 (3)0.27590.30560.39490.041*0.26617 (15)0.49163 (8)0.18385 (7)0.0342 (3)

C9	0.0405 (2)	0.27382 (9)	0.39425 (8)	0.0470 (3)
H9A	-0.0615	0.2847	0.3662	0.056*
H9B	0.0385	0.2972	0.4373	0.056*
C6	0.43879 (16)	0.51107 (10)	0.21008 (7)	0.0432 (3)
H6A	0.4997	0.5074	0.1744	0.052*
H6B	0.4466	0.5657	0.2264	0.052*
C15	0.53287 (19)	0.26629 (9)	0.23289 (8)	0.0485 (4)
C21	0.4175 (2)	0.23699 (10)	0.11699 (9)	0.0558 (4)
C16	0.40641(19)	0.26788 (8)	0 17969 (7)	0.0428(3)
C12	0.2153(2)	0.18695 (8)	0.30668 (8)	0.0488(4)
H12A	0.3173	0.1771	0.3350	0.059*
H12R	0.2199	0.1652	0.2633	0.059*
C72	0.2177 0.2823(2)	0.44916 (10)	0.45633 (7)	0.059 0.0521(4)
U72 H72	0.2625 (2)	0.44910 (10)	0.45035 (7)	0.0521 (4)
C11	0.0826(2)	0.4047 (0)	0.33507 (0)	0.005
	0.0820 (2)	0.14047 (9)	0.33307 (3)	0.0571 (4)
	0.1039	0.0697	0.3409	0.008*
	-0.01/4	0.1320	0.3044	0.068
	0.0659 (2)	0.18347 (10)	0.40116 (9)	0.0592 (4)
HIUA	0.1616	0.1727	0.4333	0.071*
HI0B	-0.0242	0.1593	0.41/1	0.0/1*
CI	0.67269 (18)	0.47886 (13)	0.28887 (9)	0.0613 (5)
HIA	0.7335	0.4781	0.2536	0.092*
HIB	0.7177	0.4413	0.3224	0.092*
H1C	0.6757	0.5317	0.3075	0.092*
C76	0.0721 (2)	0.52561 (9)	0.39544 (9)	0.0537 (4)
H76	-0.0048	0.5340	0.3579	0.064*
C20	0.2790 (3)	0.24183 (11)	0.06903 (9)	0.0658 (5)
H20	0.2808	0.2239	0.0263	0.079*
C53	0.2212 (2)	0.50518 (11)	0.00374 (8)	0.0577 (4)
H53	0.1538	0.4609	-0.0027	0.069*
C57	0.3575 (2)	0.60591 (10)	0.07381 (8)	0.0565 (4)
H57	0.3839	0.6302	0.1150	0.068*
C75	0.0883 (3)	0.58062 (11)	0.44760 (13)	0.0743 (6)
H75	0.0218	0.6253	0.4443	0.089*
C19	0.1418 (3)	0.27253 (11)	0.08442 (8)	0.0600 (5)
H19	0.0517	0.2754	0.0515	0.072*
C74	0.1995 (3)	0.56989 (13)	0.50282 (11)	0.0770 (6)
H74	0.2095	0.6070	0.5371	0.092*
C23	0.6913 (3)	0.20440 (14)	0.16253 (14)	0.0856(7)
H23	0.7891	0.1832	0.1564	0.103*
C22	0.5681 (3)	0.20404 (12)	0.11094 (12)	0.0762 (6)
H22	0.5826	0.1818	0.0709	0.091*
C54	0.2788(3)	0.53737 (14)	-0.04922(9)	0.0760 (6)
H54	0.2510	0.5143	-0.0908	0.091*
C73	0.2965(3)	0.50437(13)	0.50781 (9)	0.0701(5)
H73	0.3724	0.4965	0.5457	0.084*
C56	0.4135(3)	0.63776 (13)	0.02018(10)	0.0766 (6)
H56	0.4772	0.6834	0.0256	0.002*
1120	0.7/14	0.000	0.0230	0.072

C24	0.6777 (2)	0.23534 (12)	0.22476 (12)	0.0723 (6)
H24	0.7643	0.2349	0.2594	0.087*
C55	0.3763 (3)	0.60290 (15)	-0.04099 (10)	0.0802 (6)
H55	0.4172	0.6238	-0.0766	0.096*

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	<i>U</i> ³³	U^{12}	<i>U</i> ¹³	U ²³
01	0.0309 (5)	0.0548 (6)	0.0527 (6)	0.0048 (4)	0.0061 (4)	0.0185 (5)
N1	0.0465 (6)	0.0259 (5)	0.0339 (6)	-0.0008 (4)	0.0076 (5)	0.0001 (4)
C13	0.0351 (6)	0.0294 (6)	0.0300 (6)	0.0038 (5)	0.0046 (5)	0.0002 (5)
C7	0.0313 (6)	0.0301 (6)	0.0326 (6)	-0.0001(5)	0.0071 (5)	0.0008 (5)
N2	0.0276 (5)	0.0515 (7)	0.0370 (6)	-0.0019(5)	0.0061 (4)	0.0012 (5)
C4	0.0322 (6)	0.0282 (6)	0.0354 (6)	0.0007 (5)	0.0053 (5)	0.0028 (5)
C71	0.0393 (7)	0.0339 (6)	0.0418 (7)	-0.0039(5)	0.0187 (6)	-0.0039(5)
O2	0.0497 (6)	0.0619 (7)	0.0496 (6)	0.0142 (5)	-0.0059 (5)	0.0064 (5)
C2	0.0321 (6)	0.0369 (6)	0.0334 (6)	-0.0024(5)	0.0053 (5)	-0.0029(5)
C17	0.0480 (8)	0.0294 (6)	0.0323 (6)	0.0001 (5)	0.0084 (6)	-0.0011(5)
C51	0.0381 (7)	0.0348 (6)	0.0419 (7)	-0.0028(5)	0.0067 (6)	0.0050 (5)
C3	0.0294 (6)	0.0282 (6)	0.0296 (6)	0.0012 (4)	0.0052 (4)	0.0013 (4)
C52	0.0433 (7)	0.0400 (7)	0.0381 (7)	-0.0026 (6)	0.0058 (6)	0.0064 (6)
C18	0.0546 (9)	0.0409 (7)	0.0377 (7)	-0.0058 (6)	0.0011 (6)	-0.0028 (6)
C14	0.0409 (7)	0.0368 (7)	0.0452 (8)	0.0097 (6)	0.0029 (6)	0.0011 (6)
C8	0.0413 (7)	0.0306 (6)	0.0303 (6)	-0.0015 (5)	0.0061 (5)	0.0011 (5)
C5	0.0342 (6)	0.0307 (6)	0.0386 (7)	0.0000 (5)	0.0084 (5)	0.0047 (5)
C9	0.0574 (9)	0.0417 (8)	0.0443 (8)	-0.0093 (7)	0.0154 (7)	0.0031 (6)
C6	0.0371 (7)	0.0523 (8)	0.0405 (7)	-0.0079 (6)	0.0081 (6)	0.0061 (6)
C15	0.0483 (8)	0.0409 (8)	0.0582 (9)	0.0112 (6)	0.0149 (7)	-0.0029 (7)
C21	0.0809 (12)	0.0408 (8)	0.0534 (10)	-0.0052 (8)	0.0325 (9)	-0.0091 (7)
C16	0.0557 (9)	0.0323 (7)	0.0441 (8)	0.0006 (6)	0.0193 (7)	-0.0041 (6)
C12	0.0672 (10)	0.0288 (7)	0.0497 (8)	0.0032 (6)	0.0084 (7)	0.0017 (6)
C72	0.0644 (10)	0.0537 (9)	0.0395 (8)	-0.0023 (7)	0.0124 (7)	-0.0090 (7)
C11	0.0745 (11)	0.0309 (7)	0.0644 (11)	-0.0082 (7)	0.0079 (9)	0.0046 (7)
C10	0.0774 (12)	0.0429 (8)	0.0602 (10)	-0.0139 (8)	0.0199 (9)	0.0114 (7)
C1	0.0307 (7)	0.0949 (14)	0.0573 (10)	-0.0090 (8)	0.0047 (7)	0.0078 (9)
C76	0.0509 (9)	0.0394 (8)	0.0754 (11)	0.0024 (6)	0.0239 (8)	-0.0058 (7)
C20	0.1035 (16)	0.0572 (10)	0.0409 (9)	-0.0175 (10)	0.0240 (10)	-0.0153 (7)
C53	0.0724 (11)	0.0551 (10)	0.0472 (9)	-0.0198 (8)	0.0150 (8)	-0.0028 (7)
C57	0.0699 (11)	0.0535 (9)	0.0444 (8)	-0.0209 (8)	0.0047 (8)	0.0056 (7)
C75	0.0807 (14)	0.0449 (9)	0.1095 (18)	0.0002 (9)	0.0502 (13)	-0.0219 (10)
C19	0.0859 (13)	0.0544 (10)	0.0361 (8)	-0.0158 (9)	0.0005 (8)	-0.0064 (7)
C74	0.0941 (15)	0.0696 (13)	0.0778 (14)	-0.0238 (11)	0.0442 (13)	-0.0385 (11)
C23	0.0820 (15)	0.0721 (14)	0.115 (2)	0.0208 (11)	0.0528 (15)	-0.0141 (13)
C22	0.1001 (17)	0.0591 (11)	0.0839 (15)	0.0003 (11)	0.0566 (14)	-0.0189 (10)
C54	0.1030 (16)	0.0851 (15)	0.0436 (10)	-0.0282 (12)	0.0228 (10)	-0.0055 (9)
C73	0.0879 (14)	0.0775 (13)	0.0477 (10)	-0.0191 (11)	0.0194 (9)	-0.0225 (9)
C56	0.0903 (15)	0.0769 (13)	0.0618 (12)	-0.0402 (11)	0.0107 (10)	0.0169 (10)
C24	0.0583 (11)	0.0675 (12)	0.0946 (15)	0.0221 (9)	0.0227 (10)	-0.0086 (11)

<u>C55</u>	0.0961 (16)	0.0948 (16)	0.0544 (11)	-0.0282 (13)	0.0259 (11)	0.0160 (11)
Geome	tric parameters (À	ĺ, °)				
01—C	4	1.2122	(15)	C15—C16		1.393 (2)
N1—C	8	1.4539	(16)	C21—C20		1.399 (3)
N1—C	12	1.4612	(18)	C21—C16		1.406 (2)
N1—C	13	1.4652	(17)	C21—C22		1.418 (3)
C13—0	C17	1.5207	(17)	C12—C11		1.514 (2)
C13—0	C14	1.5772	(18)	C12—H12A		0.9700
C13—0	C3	1.5933	(17)	C12—H12B		0.9700
С7—С	71	1.5097	(18)	С72—С73		1.391 (2)
С7—С	8	1.5243	(17)	С72—Н72		0.9300
С7—С	3	1.5588	(16)	C11—C10		1.520 (3)
С7—Н	7	0.9800		C11—H11A		0.9700
N2—C	2	1.4533	(16)	C11—H11B		0.9700
N2—C	1	1.4564	(18)	C10—H10A		0.9700
N2—C	6	1.4589	(18)	C10—H10B		0.9700
C4—C	5	1.4934	(17)	C1—H1A		0.9600
C4—C	3	1.5306	(17)	C1—H1B		0.9600
C71—0	C72	1.384 (2)	C1—H1C		0.9600
C71—0	C76	1.386 (2)	C76—C75		1.399 (3)
02—C	14	1.2112	(17)	С76—Н76		0.9300
С2—С	3	1.5289	(17)	C20—C19		1.359 (3)
С2—Н	2A	0.9700		C20—H20		0.9300
С2—Н	2B	0.9700		C53—C54		1.377 (2)
C17—0	C18	1.360 (2)	С53—Н53		0.9300
C17—0	C16	1.408 (2)	C57—C56		1.380 (2)
C51—0	C5	1.3337	(19)	С57—Н57		0.9300
C51—0	C52	1.4666	(19)	С75—С74		1.355 (3)
C51—I	H51	0.9300		С75—Н75		0.9300
C52—0	C53	1.386 (2)	C19—H19		0.9300
C52—0	C57	1.388 (2)	C74—C73		1.361 (3)
C18—0	C19	1.416 (2)	С74—Н74		0.9300
C18—I	H18	0.9300		C23—C22		1.353 (3)
C14—0	C15	1.477 (2)	C23—C24		1.402 (3)
С8—С	9	1.5144	(19)	С23—Н23		0.9300
С8—Н	8	0.9800		C22—H22		0.9300
С5—С	6	1.5064	(19)	C54—C55		1.364 (3)
С9—С	10	1.525 (2)	C54—H54		0.9300
С9—Н	9A	0.9700		С73—Н73		0.9300
С9—Н	9B	0.9700		C56—C55		1.371 (3)
С6—Н	6A	0.9700		С56—Н56		0.9300
С6—Н	6B	0.9700		C24—H24		0.9300
C15—0	C24	1.371 (2)	С55—Н55		0.9300
C8—N	1—C12	114.03	(11)	C20—C21—C16		116.24 (16)
C8—N	1—C13	107.94	(10)	C20—C21—C22		128.43 (17)

C12—N1—C13	116.74 (11)	C16—C21—C22	115.33 (19)
N1—C13—C17	109.12 (10)	C15—C16—C21	123.14 (15)
N1-C13-C14	112.62 (10)	C15—C16—C17	113.43 (13)
C17—C13—C14	101.88 (10)	C21—C16—C17	123.37 (15)
N1—C13—C3	102.61 (9)	N1—C12—C11	109.19 (13)
C17—C13—C3	118.80 (10)	N1—C12—H12A	109.8
C14—C13—C3	112.14 (10)	C11—C12—H12A	109.8
C71 - C7 - C8	115 21 (11)	N1-C12-H12B	109.8
C71 - C7 - C3	116.61 (10)	$C_{11} - C_{12} - H_{12B}$	109.8
$C_{8} - C_{7} - C_{3}$	104 13 (10)	H12A - C12 - H12B	108.3
$C_{1} = C_{1} = C_{2} = H_{2}$	106.7	C71 - C72 - C73	121.46(17)
C8-C7-H7	106.7	C71 - C72 - H72	110.3
C_{0}	106.7	$C_{1}^{2} = C_{12}^{2} = H_{12}^{2}$	119.5
$C_{2} = C_{1} = C_{1}$	100.7	$C_{12} = C_{12} = C$	119.5
$C_2 = N_2 = C_1$	111.92(12)	C_{12} C_{11} U_{11A}	100.5
$C_2 = N_2 = C_0$	109.09 (11)		109.5
CI = N2 = C6	110.45 (12)	CIO-CII-HIIA	109.5
01C3	121.15 (11)	CI2—CII—HIIB	109.5
01	121.55 (11)	Cl0—Cl1—HIIB	109.5
C3—C4—C3	117.28 (10)	HIIA—CII—HIIB	108.1
C72—C71—C76	117.41 (14)	C11—C10—C9	110.58 (13)
C72—C71—C7	122.78 (12)	C11—C10—H10A	109.5
C76—C71—C7	119.79 (14)	C9—C10—H10A	109.5
N2—C2—C3	108.88 (10)	C11—C10—H10B	109.5
N2—C2—H2A	109.9	C9—C10—H10B	109.5
C3—C2—H2A	109.9	H10A—C10—H10B	108.1
N2—C2—H2B	109.9	N2—C1—H1A	109.5
С3—С2—Н2В	109.9	N2—C1—H1B	109.5
H2A—C2—H2B	108.3	H1A—C1—H1B	109.5
C18—C17—C16	118.64 (13)	N2—C1—H1C	109.5
C18—C17—C13	131.87 (13)	H1A—C1—H1C	109.5
C16—C17—C13	109.21 (12)	H1B—C1—H1C	109.5
C5—C51—C52	128.80 (13)	C71—C76—C75	120.34 (18)
С5—С51—Н51	115.6	С71—С76—Н76	119.8
С52—С51—Н51	115.6	С75—С76—Н76	119.8
C2—C3—C4	107.15 (10)	C19—C20—C21	120.48 (15)
$C^2 - C^3 - C^7$	113 58 (10)	C19—C20—H20	119.8
C4—C3—C7	111.72 (10)	$C_{21} - C_{20} - H_{20}$	119.8
$C^2 - C^3 - C^{13}$	111.72 (10)	$C_{54} C_{53} C_{52}$	121.02 (16)
C_{4} C_{3} C_{13}	108 58 (10)	$C_{54} - C_{53} - H_{53}$	119.5
C7 - C3 - C13	104.00 (9)	C_{52} C_{53} H_{53}	119.5
C_{7}^{53} C_{57}^{52} C_{57}^{57}	117.00(1)	C56 C57 C52	120.26 (16)
$C_{53} = C_{52} = C_{51}$	110 16 (13)	C56 C57 H57	110.0
$C_{55} = C_{52} = C_{51}$	122.75(13)	$C_{50} = C_{57} = H_{57}$	110.0
$C_{17} = C_{12} = C_{11}$	122.73(14) 118 50 (16)	$C_{32} - C_{37} - H_{37}$	117.7
C17 - C10 - C17 C17 - C19 - U19	120.8	C74 C75 H75	121.05 (10)
$C_{1} - C_{10} - C_{10} - C_{10}$	120.0	$C_{14} - C_{13} - \Pi_{13}$	119.5
$C_{12} = C_{10} = \Pi_{10}$	120.0 126.70(12)	$C_{10} - C_{13} - \Pi_{13}$	117.3
02 - 014 - 013	120.79(13) 124.08(12)	$C_{20} = C_{10} = U_{10}$	122.00 (17)
02-014-013	124.98 (13)	U2U-UI9-HI9	110./

~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~ ~		Q10 Q10 TT10	
C15—C14—C13	107.71 (12)	C18—C19—H19	118.7
N1—C8—C9	110.01 (11)	C75—C74—C73	119.54 (17)
N1—C8—C7	101.35 (10)	С75—С74—Н74	120.2
C9—C8—C7	115.39 (11)	С73—С74—Н74	120.2
N1—C8—H8	109.9	C22—C23—C24	122.73 (19)
С9—С8—Н8	109.9	С22—С23—Н23	118.6
С7—С8—Н8	109.9	С24—С23—Н23	118.6
C51—C5—C4	116.79 (12)	C23—C22—C21	121.06 (18)
C51—C5—C6	124.14 (12)	C23—C22—H22	119.5
C4—C5—C6	119.01 (11)	C21—C22—H22	119.5
C8—C9—C10	110.01 (13)	C55—C54—C53	120.40 (18)
С8—С9—Н9А	109.7	С55—С54—Н54	119.8
С10—С9—Н9А	109.7	С53—С54—Н54	119.8
С8—С9—Н9В	109.7	C74—C73—C72	120.2 (2)
C10—C9—H9B	109.7	С74—С73—Н73	119.9
H9A—C9—H9B	108.2	С72—С73—Н73	119.9
N_{2} C_{6} C_{5}	111 84 (11)	$C_{55} - C_{56} - C_{57}$	120.82 (18)
N2C6H6A	100.2	$C_{55} = C_{56} = H_{56}$	119.6
C_{5} C_{6} H_{6A}	109.2	C57 C56 H56	119.0
N2 C6 H6P	109.2	$C_{15} = C_{24} = C_{23}$	117.0(2)
$N_2 = C_0 = H_0 B$	109.2	C15 - C24 - C25	117.9(2)
	109.2	C13 - C24 - H24	121.1
H0A - C0 - H0B	107.9	C23—C24—H24	121.1
$C_{24} = C_{15} = C_{16}$	119.82 (17)	C54—C55—C56	119.44 (17)
C24—C15—C14	132.36 (17)	С54—С55—Н55	120.3
C16—C15—C14	107.74 (12)	С56—С55—Н55	120.3
C8—N1—C13—C17	-161.77 (10)	C52—C51—C5—C4	179.34 (13)
C8—N1—C13—C17 C12—N1—C13—C17	-161.77 (10) 68.27 (14)	C52—C51—C5—C4 C52—C51—C5—C6	179.34 (13) -3.5 (2)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14	-161.77 (10) 68.27 (14) 85.87 (12)	C52—C51—C5—C4 C52—C51—C5—C6 O1—C4—C5—C51	179.34 (13) -3.5 (2) -22.96 (19)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15)	C52—C51—C5—C4 C52—C51—C5—C6 O1—C4—C5—C51 C3—C4—C5—C51	179.34 (13) -3.5 (2) -22.96 (19) 155.19 (12)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C14 C8—N1—C13—C3	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12)	C52—C51—C5—C4 C52—C51—C5—C6 O1—C4—C5—C51 C3—C4—C5—C51 O1—C4—C5—C6	179.34 (13) -3.5 (2) -22.96 (19) 155.19 (12) 159.74 (13)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12) -164.86 (11)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	179.34 (13) -3.5 (2) -22.96 (19) 155.19 (12) 159.74 (13) -22.11 (17)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12) -164.86 (11) 35.14 (18)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	179.34 (13) -3.5 (2) -22.96 (19) 155.19 (12) 159.74 (13) -22.11 (17) 55.74 (16)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72 C3—C7—C71—C72	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12) -164.86 (11) 35.14 (18) -87.39 (16)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	179.34 (13) -3.5 (2) -22.96 (19) 155.19 (12) 159.74 (13) -22.11 (17) 55.74 (16) 169.61 (12)
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72 C3—C7—C71—C72 C8—C7—C71—C76	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12) -164.86 (11) 35.14 (18) -87.39 (16) -143.38 (13)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15) \end{array}$
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72 C3—C7—C71—C72 C8—C7—C71—C76 C3—C7—C71—C76	-161.77 (10) 68.27 (14) 85.87 (12) -44.09 (15) -34.89 (12) -164.86 (11) 35.14 (18) -87.39 (16) -143.38 (13) 94.09 (15)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13) \end{array}$
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72 C3—C7—C71—C72 C8—C7—C71—C76 C3—C7—C71—C76 C1—N2—C2—C3	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13) \end{array}$
C8—N1—C13—C17 C12—N1—C13—C17 C8—N1—C13—C14 C12—N1—C13—C14 C8—N1—C13—C3 C12—N1—C13—C3 C8—C7—C71—C72 C3—C7—C71—C72 C8—C7—C71—C76 C3—C7—C71—C76 C1—N2—C2—C3 C6—N2—C2—C3	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18) \end{array}$
$\begin{array}{c} C8 = N1 = C13 = C17 \\ C12 = N1 = C13 = C17 \\ C8 = N1 = C13 = C14 \\ C12 = N1 = C13 = C14 \\ C8 = N1 = C13 = C3 \\ C12 = N1 = C13 = C3 \\ C12 = N1 = C13 = C3 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C4 = C7 = C71 = C76 \\ C1 = N2 = C2 = C3 \\ C6 = N2 = C2 = C3 \\ N1 = C13 = C17 = C18 \end{array}$	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \\ 55.50 (18) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34 (13) \\ -3.5 (2) \\ -22.96 (19) \\ 155.19 (12) \\ 159.74 (13) \\ -22.11 (17) \\ 55.74 (16) \\ 169.61 (12) \\ -54.29 (15) \\ -178.11 (13) \\ -147.88 (13) \\ 29.22 (18) \\ -5.5 (3) \end{array}$
$\begin{array}{c} C8 = N1 = C13 = C17 \\ C12 = N1 = C13 = C17 \\ C8 = N1 = C13 = C14 \\ C12 = N1 = C13 = C14 \\ C8 = N1 = C13 = C3 \\ C12 = N1 = C13 = C3 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C4 = C7 = C71 = C76 \\ C1 = N2 = C2 = C3 \\ C6 = N2 = C2 = C3 \\ N1 = C13 = C17 = C18 \\ C14 = C13 = C17 = C18 \\ \end{array}$	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \\ 55.50 (18) \\ 174.76 (14) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177\ 54\ (19) \end{array}$
$\begin{array}{c} C8 = N1 = C13 = C17 \\ C12 = N1 = C13 = C17 \\ C8 = N1 = C13 = C14 \\ C12 = N1 = C13 = C14 \\ C8 = N1 = C13 = C3 \\ C12 = N1 = C13 = C3 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C4 = C7 = C71 = C76 \\ C1 = N2 = C2 = C3 \\ C6 = N2 = C2 = C3 \\ N1 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C14 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C14 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C14 = C13 = C17 = C18 \\ C3 = C13 = C17 = C18 \\ C14 = C18 \\ C14 = C17 = C18 \\ C14 = C18 \\ C14 = C17 \\ C14 = C18 \\ C14 = C18$	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \\ 55.50 (18) \\ 174.76 (14) \\ -61 52 (19) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171\ 13\ (15)\\ \end{array}$
$\begin{array}{c} C8 = N1 = C13 = C17 \\ C12 = N1 = C13 = C17 \\ C8 = N1 = C13 = C14 \\ C12 = N1 = C13 = C14 \\ C8 = N1 = C13 = C3 \\ C12 = N1 = C13 = C3 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C72 \\ C3 = C7 = C71 = C76 \\ C1 = N2 = C2 = C3 \\ N1 = C13 = C17 = C18 \\ C14 = C13 = C17 = C18 \\ N1 = C13 = C17 = C16 \end{array}$	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \\ 55.50 (18) \\ 174.76 (14) \\ -61.52 (19) \\ -118.20 (12) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0\ 94\ (16)\\ \end{array}$
$C_{8} = N_{1} = C_{13} = C_{17}$ $C_{12} = N_{1} = C_{13} = C_{17}$ $C_{8} = N_{1} = C_{13} = C_{14}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{1} = N_{1} = C_{13} = C_{3}$ $C_{1} = C_{13} = C_{3}$ $C_{1} = C_{13} = C_{17} = C_{16}$ $C_{1} = C_{13} = C_{17} = C_{16}$ $C_{1} = C_{13} = C_{17} = C_{16}$ $C_{14} = C_{13} = C_{17} = C_{16}$	$\begin{array}{c} -161.77 (10) \\ 68.27 (14) \\ 85.87 (12) \\ -44.09 (15) \\ -34.89 (12) \\ -164.86 (11) \\ 35.14 (18) \\ -87.39 (16) \\ -143.38 (13) \\ 94.09 (15) \\ -163.22 (13) \\ 73.82 (13) \\ 55.50 (18) \\ 174.76 (14) \\ -61.52 (19) \\ -118.20 (12) \\ 1.06 (14) \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1\ 7\ (2)\\ \end{array}$
$C_{8} = N_{1} = C_{13} = C_{17}$ $C_{12} = N_{1} = C_{13} = C_{17}$ $C_{8} = N_{1} = C_{13} = C_{14}$ $C_{12} = N_{1} = C_{13} = C_{14}$ $C_{8} = N_{1} = C_{13} = C_{3}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{8} = C_{7} = C_{71} = C_{72}$ $C_{3} = C_{7} = C_{71} = C_{72}$ $C_{8} = C_{7} = C_{73}$ $C_{8} = C_{7} = C_{73}$ $C_{8} = C_{7} = C_{73}$ $C_{8} = C_{73} = C_{73}$ $C_{7} = $	$\begin{array}{c} -161.77\ (10)\\ 68.27\ (14)\\ 85.87\ (12)\\ -44.09\ (15)\\ -34.89\ (12)\\ -164.86\ (11)\\ 35.14\ (18)\\ -87.39\ (16)\\ -143.38\ (13)\\ 94.09\ (15)\\ -163.22\ (13)\\ 73.82\ (13)\\ 55.50\ (18)\\ 174.76\ (14)\\ -61.52\ (19)\\ -118.20\ (12)\\ 1.06\ (14)\\ 124\ 78\ (12)\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1.7\ (2)\\ -175\ 37\ (14) \end{array}$
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} -161.77\ (10)\\ 68.27\ (14)\\ 85.87\ (12)\\ -44.09\ (15)\\ -34.89\ (12)\\ -164.86\ (11)\\ 35.14\ (18)\\ -87.39\ (16)\\ -143.38\ (13)\\ 94.09\ (15)\\ -163.22\ (13)\\ 73.82\ (13)\\ 55.50\ (18)\\ 174.76\ (14)\\ -61.52\ (19)\\ -118.20\ (12)\\ 1.06\ (14)\\ 124.78\ (12)\\ -61.97\ (13)\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1.7\ (2)\\ -175.37\ (14)\\ 178\ 83\ (16)\\ \end{array}$
$C_{8} = N_{1} = C_{13} = C_{17}$ $C_{12} = N_{1} = C_{13} = C_{17}$ $C_{8} = N_{1} = C_{13} = C_{14}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{1} = C_{13} = C_{3}$ $C_{3} = C_{7} = C_{71} = C_{72}$ $C_{3} = C_{7} = C_{71} = C_{76}$ $C_{3} = C_{73} = C_{77} = C_{76}$ $C_{1} = N_{2} = C_{2} = C_{3}$ $N_{1} = C_{13} = C_{17} = C_{18}$ $C_{3} = C_{13} = C_{17} = C_{16}$ $C_{3} = C_{13} = C_{17} = C_{16}$ $N_{2} = C_{2} = C_{3} = C_{7}$	$\begin{array}{c} -161.77\ (10)\\ 68.27\ (14)\\ 85.87\ (12)\\ -44.09\ (15)\\ -34.89\ (12)\\ -164.86\ (11)\\ 35.14\ (18)\\ -87.39\ (16)\\ -143.38\ (13)\\ 94.09\ (15)\\ -163.22\ (13)\\ 73.82\ (13)\\ 55.50\ (18)\\ 174.76\ (14)\\ -61.52\ (19)\\ -118.20\ (12)\\ 1.06\ (14)\\ 124.78\ (12)\\ -61.97\ (13)\\ 174.16\ (10)\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1.7\ (2)\\ -175.37\ (14)\\ 178.83\ (16)\\ 1.72\ (18)\\ \end{array}$
$C_{8} = N_{1} = C_{13} = C_{17}$ $C_{12} = N_{1} = C_{13} = C_{17}$ $C_{8} = N_{1} = C_{13} = C_{14}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{1} = N_{1} = C_{13} = C_{3}$ $C_{8} = C_{7} = C_{71} = C_{72}$ $C_{3} = C_{7} = C_{71} = C_{72}$ $C_{8} = C_{7} = C_{71} = C_{72}$ $C_{8} = C_{7} = C_{71} = C_{72}$ $C_{8} = C_{7} = C_{71} = C_{76}$ $C_{3} = C_{7} = C_{71} = C_{76}$ $C_{3} = C_{7} = C_{71} = C_{76}$ $C_{3} = C_{7} = C_{71} = C_{76}$ $C_{1} = N_{2} = C_{2} = C_{3}$ $N_{1} = C_{13} = C_{17} = C_{18}$ $N_{1} = C_{13} = C_{17} = C_{16}$ $C_{3} = C_{13} = C_{17} = C_{16}$ $N_{2} = C_{2} = C_{3} = C_{7}$ $N_{2} = C_{2} = C_{3} = C_{7}$	$\begin{array}{c} -161.77\ (10)\\ 68.27\ (14)\\ 85.87\ (12)\\ -44.09\ (15)\\ -34.89\ (12)\\ -164.86\ (11)\\ 35.14\ (18)\\ -87.39\ (16)\\ -143.38\ (13)\\ 94.09\ (15)\\ -163.22\ (13)\\ 73.82\ (13)\\ 55.50\ (18)\\ 174.76\ (14)\\ -61.52\ (19)\\ -118.20\ (12)\\ 1.06\ (14)\\ 124.78\ (12)\\ -61.97\ (13)\\ 174.16\ (10)\\ 55.67\ (12)\\ \end{array}$	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1.7\ (2)\\ -175.37\ (14)\\ 178.83\ (16)\\ 1.73\ (18)\\ 179.09\ (15)\\ \end{array}$
$C_{8} = N_{1} = C_{13} = C_{17}$ $C_{12} = N_{1} = C_{13} = C_{17}$ $C_{8} = N_{1} = C_{13} = C_{14}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{12} = N_{1} = C_{13} = C_{3}$ $C_{1} = N_{1} = C_{13} = C_{3}$ $C_{8} = C_{7} = C_{71} = C_{72}$ $C_{8} = C_{7} = C_{71} = C_{76}$ $C_{3} = C_{7} = C_{77} = C_{78}$ $N_{1} = C_{13} = C_{17} = C_{18}$ $N_{1} = C_{13} = C_{17} = C_{16}$ $C_{3} = C_{13} = C_{17} = C_{16}$ $N_{2} = C_{2} = C_{3} = C_{7}$ $N_{2} = C_{2} = C_{3} = C_{7}$	$\begin{array}{c} -161.77\ (10)\\ 68.27\ (14)\\ 85.87\ (12)\\ -44.09\ (15)\\ -34.89\ (12)\\ -164.86\ (11)\\ 35.14\ (18)\\ -87.39\ (16)\\ -143.38\ (13)\\ 94.09\ (15)\\ -163.22\ (13)\\ 73.82\ (13)\\ 55.50\ (18)\\ 174.76\ (14)\\ -61.52\ (19)\\ -118.20\ (12)\\ 1.06\ (14)\\ 124.78\ (12)\\ -61.97\ (13)\\ 174.16\ (10)\\ 56.87\ (13)\\ -1100\ (14)\\ -1100\ (14)\\ -1100\ (14)\\ -1100\ (14)\\ -1100\ (14)\\ -1100\ (14)\ (10)\ (14)\ (10)\\ -1100\ (14)\ (10)\ (14)\ (10)\ (14)\ (11)\\ -1100\ (14)\ (11)\ ($	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} 179.34\ (13)\\ -3.5\ (2)\\ -22.96\ (19)\\ 155.19\ (12)\\ 159.74\ (13)\\ -22.11\ (17)\\ 55.74\ (16)\\ 169.61\ (12)\\ -54.29\ (15)\\ -178.11\ (13)\\ -147.88\ (13)\\ 29.22\ (18)\\ -5.5\ (3)\\ -177.54\ (19)\\ 171.13\ (15)\\ -0.94\ (16)\\ 1.7\ (2)\\ -175.37\ (14)\\ 178.83\ (16)\\ 1.73\ (18)\\ 178.90\ (15)\\ -2.4\ (2)\\ -175.37\ (15)\\ -2.4\ (2)\\ -175.90\ (15)\\ -2.4\ (2)\ (2)\\ -2.4\ (2)\ (2)\ (2)\ (2)\ (2)\ (2)\ (2)\ (2)$

C5—C4—C3—C2	36.60 (14)	C20-C21-C16-C17	2.1 (2)
O1—C4—C3—C7	-20.26 (17)	C22—C21—C16—C17	-177.24 (15)
C5—C4—C3—C7	161.60 (10)	C18—C17—C16—C15	-176.47 (13)
O1—C4—C3—C13	93.86 (14)	C13—C17—C16—C15	-1.81 (17)
C5—C4—C3—C13	-84.29 (13)	C18—C17—C16—C21	0.6 (2)
C71—C7—C3—C2	23.51 (15)	C13—C17—C16—C21	175.28 (13)
C8—C7—C3—C2	-104.61 (12)	C8—N1—C12—C11	59.07 (16)
C71—C7—C3—C4	-97.83 (13)	C13—N1—C12—C11	-173.91 (12)
C8—C7—C3—C4	134.04 (10)	C76—C71—C72—C73	0.3 (2)
C71—C7—C3—C13	145.25 (11)	C7—C71—C72—C73	-178.25 (15)
C8—C7—C3—C13	17.12 (12)	N1-C12-C11-C10	-55.75 (18)
N1—C13—C3—C2	132.33 (10)	C12—C11—C10—C9	55.3 (2)
C17—C13—C3—C2	-107.27 (13)	C8—C9—C10—C11	-54.83 (19)
C14—C13—C3—C2	11.23 (14)	C72—C71—C76—C75	-0.1 (2)
N1—C13—C3—C4	-109.69 (10)	C7—C71—C76—C75	178.50 (14)
C17—C13—C3—C4	10.71 (15)	C16—C21—C20—C19	-2.1 (2)
C14—C13—C3—C4	129.22 (11)	C22—C21—C20—C19	177.08 (19)
N1—C13—C3—C7	9.40 (12)	C57—C52—C53—C54	2.6 (3)
C17—C13—C3—C7	129.80 (11)	C51—C52—C53—C54	178.97 (18)
C14—C13—C3—C7	-111.69 (11)	C53—C52—C57—C56	-2.1 (3)
C5—C51—C52—C53	141.99 (17)	C51—C52—C57—C56	-178.41 (18)
C5—C51—C52—C57	-41.8 (2)	C71—C76—C75—C74	0.1 (3)
C16—C17—C18—C19	-3.2 (2)	C21—C20—C19—C18	-0.4 (3)
C13—C17—C18—C19	-176.42 (14)	C17—C18—C19—C20	3.2 (2)
N1-C13-C14-O2	-55.56 (18)	C76—C75—C74—C73	-0.3 (3)
C17—C13—C14—O2	-172.32 (14)	C24—C23—C22—C21	1.3 (4)
C3—C13—C14—O2	59.57 (18)	C20—C21—C22—C23	179.7 (2)
N1—C13—C14—C15	116.69 (12)	C16—C21—C22—C23	-1.1 (3)
C17—C13—C14—C15	-0.07 (14)	C52—C53—C54—C55	-0.7 (4)
C3—C13—C14—C15	-128.18 (12)	C75—C74—C73—C72	0.5 (3)
C12—N1—C8—C9	-59.48 (15)	C71—C72—C73—C74	-0.5 (3)
C13—N1—C8—C9	169.06 (11)	C52—C57—C56—C55	-0.1 (3)
C12—N1—C8—C7	177.93 (11)	C16—C15—C24—C23	-1.5 (3)
C13—N1—C8—C7	46.47 (12)	C14—C15—C24—C23	174.78 (19)
C71—C7—C8—N1	-166.60 (10)	C22—C23—C24—C15	0.0 (4)
C3—C7—C8—N1	-37.62 (12)	C53—C54—C55—C56	-1.6 (4)
C71—C7—C8—C9	74.61 (15)	C57—C56—C55—C54	2.0 (4)
C3—C7—C8—C9	-156.41 (11)		

Hydrogen-bond geometry (Å, °)

D—H···A	D—H	Н…А	D····A	<i>D</i> —H··· <i>A</i>
C2—H2 <i>B</i> ···O2	0.97	2.35	2.9329 (18)	118