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# 7-Iodo-3,3-diphenyloctahydrobenzofuran

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Key indicators: single-crystal X-ray study: T = 153 K: mean  $\sigma$ (C–C) = 0.004 Å: R factor = 0.039; wR factor = 0.091; data-to-parameter ratio = 24.2.

The title compound, C<sub>20</sub>H<sub>21</sub>IO, was synthesized by cyclohaloetherification of 2-(cyclohex-2-enyl)-2,2-diphenylethanol in CH<sub>2</sub>Cl<sub>2</sub>, and crystallized with two independent molecules in the asymmetric unit. The six-membered cyclohexane ring adopts a chair conformation, while the five-membered ring adopts an envelope conformation with the fused C atom opposite the O atom as the flap in each case [displacements of the flap atoms = 0.6813 (3) and 0.6679 (3) Å]. In the crystal, molecules are linked via pairs of  $C-H\cdots\pi$  interactions, forming inversion dimers.

## **Related literature**

For the title compound as a core structure of many drugs and natural products, see: Huang & Chen (2007); Trost et al. (2003). For the synthesis of 2-(cyclohex-2-enyl)-2,2-diphenylethanol, see: Brooner & Widenhoefer (2011).



# organic compounds

19455 measured reflections

 $R_{\rm int} = 0.034$ 

397 parameters

 $\Delta \rho_{\text{max}} = 1.05 \text{ e } \text{\AA}^ \Delta \rho_{\rm min} = -0.75$  e Å<sup>-3</sup>

9610 independent reflections

7599 reflections with  $I > 2\sigma(I)$ 

H-atom parameters constrained

### **Experimental**

#### Crystal data

| $C_{20}H_{21}IO$                | $\gamma = 64.945 \ (7)^{\circ}$           |
|---------------------------------|---|
| $M_r = 404.27$                  | V = 1692.8 (5) Å <sup>3</sup>             |
| Triclinic, P1                   | Z = 4                                     |
| a = 11.4082 (18)  Å             | Mo $K\alpha$ radiation                    |
| b = 12.523 (2) Å                | $\mu = 1.89 \text{ mm}^{-1}$              |
| c = 14.007 (3) Å                | T = 153  K                                |
| $\alpha = 73.306 \ (8)^{\circ}$ | $0.33 \times 0.27 \times 0.10 \text{ mm}$ |
| $\beta = 71.646 \ (8)^{\circ}$  |   |
|                                 |   |

#### Data collection

Rigaku AFC10/Saturn724+ diffractometer Absorption correction: multi-scan (CrystalClear; Rigaku, 2008)  $T_{\min} = 0.572, T_{\max} = 0.833$ 

### Refinement

 $R[F^2 > 2\sigma(F^2)] = 0.039$  $wR(F^2) = 0.091$ S = 1.009610 reflections

#### Table 1

Hydrogen-bond geometry (Å, °).

Cg1 and Cg2 are the centroids of the C9-C14 and C15'-C20' rings, respectively.

| $D - H \cdots A$                               | D-H  | $H \cdot \cdot \cdot A$ | $D \cdots A$           | $D - \mathbf{H} \cdot \cdot \cdot A$ |
|--|--|-------------------------|------------------------|--------------------------------------|
| $C2-H2\cdots Cg1^{i}$ $C2'-H2'\cdots Cg2^{ii}$ | $\begin{array}{c} 1.00\\ 1.00 \end{array}$ | 2.53<br>2.54            | 3.519 (3)<br>3.533 (3) | 171<br>171                           |

Symmetry codes: (i) -x + 1, -y + 1, -z + 1; (ii) -x + 2, -y + 2, -z.

Data collection: CrystalClear (Rigaku, 2008); cell refinement: CrystalClear; data reduction: CrystalClear; program(s) used to solve structure: SHELXS97 (Sheldrick, 2008); program(s) used to refine structure: SHELXL97 (Sheldrick, 2008); molecular graphics: SHELXTL (Sheldrick, 2008); software used to prepare material for publication: SHELXTL.

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Supplementary data and figures for this paper are available from the IUCr electronic archives (Reference: HG5298).

#### References

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# supporting information

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# 7-Iodo-3,3-diphenyloctahydrobenzofuran

## Muhammad Sohail, Wang Yao-Feng, Wang Qi and Fu-Xue Chen

## S1. Comment

The title compound (I, Fig. 1), is an important core structure of many organic drugs and natural products (Huang *et al.* 2007, Trost *et al.*, 2003) and is useful to introduce functionality at C7. The asymmetric unit of title compound consists of two independent molecules in which the iodo-cyclohexane rings adopt chair conformations. In the crystal lattice, two molecules in asymmetric unit are linked by C—H… $\pi$  interactions with phenyl ring.

## **S2. Experimental**

N-Iodosuccinimide (13.5 mg, 0.06 mmole, 1.2 eq) was added to the solution of 2-(cyclohex-2-enyl)-2,2-diphenylethanol (13.9 mg, 0.05 mmole, 1 eq) in CH<sub>2</sub>Cl<sub>2</sub> (0.5 ml) at -78°C. The reaction mixture was stirred at -78°C for 2.5 h, after reaction completion, as monitored by TLC the crude was directly loaded on column and purified by flash column chromatography (silica gel, Et<sub>2</sub>O-Petrolium ether, 1:40), redissolving of crude in *n*-hexane afforded pure crystals (99%) of (I) (Brooner *et al.* 2011).

## **S3. Refinement**

Carbon protons were included in the riding model approximation with C—H distances 0.95-1.00 Å, and with  $U_{iso}(H)=1.2U_{eq}(C)$ .



## Figure 1

The molecular structure of the two molecules of (I), with atom labels and 30% probability displacement ellipsoids for non-H atoms.



## Figure 2

A view of C—H··· $\pi$  interactions are indicated by dotted lines in the crystal structure of the title compound.

## 7-Iodo-3,3-diphenyloctahydrobenzofuran

Crystal data

C<sub>20</sub>H<sub>21</sub>IO  $M_r = 404.27$ Triclinic, *P*1 Hall symbol: -P 1 a = 11.4082 (18) Å b = 12.523 (2) Å c = 14.007 (3) Å a = 73.306 (8)°  $\beta = 71.646$  (8)°  $\gamma = 64.945$  (7)° V = 1692.8 (5) Å<sup>3</sup>

## Data collection

Rigaku AFC10/Saturn724+ diffractometer Radiation source: Rotating Anode Graphite monochromator Detector resolution: 28.5714 pixels mm<sup>-1</sup> phi and  $\omega$  scans Z = 4 F(000) = 808  $D_x = 1.586 \text{ Mg m}^{-3}$ Mo K $\alpha$  radiation,  $\lambda = 0.71073 \text{ Å}$ Cell parameters from 5864 reflections  $\theta = 2.2-30.0^{\circ}$   $\mu = 1.89 \text{ mm}^{-1}$ T = 153 K Block, colourless  $0.33 \times 0.27 \times 0.10 \text{ mm}$ 

Absorption correction: multi-scan (*CrystalClear*; Rigaku, 2008)  $T_{min} = 0.572$ ,  $T_{max} = 0.833$ 19455 measured reflections 9610 independent reflections 7599 reflections with  $I > 2\sigma(I)$  $R_{int} = 0.034$ 

| $\theta_{\rm max} = 30.0^\circ,  \theta_{\rm min} = 2.2^\circ$ | $k = -17 \rightarrow 16$                                  |
|--|---|
| $h = -16 \rightarrow 13$                                       | $l = -19 \rightarrow 19$                                  |
| Refinement   |   |
| Refinement on $F^2$  | Secondary atom site location: difference Fourier          |
| Least-squares matrix: full                                     | map   |
| $R[F^2 > 2\sigma(F^2)] = 0.039$                                | Hydrogen site location: inferred from                     |
| $wR(F^2) = 0.091$  | neighbouring sites  |
| S = 1.00   | H-atom parameters constrained                             |
| 9610 reflections   | $w = 1/[\sigma^2(F_o^2) + (0.0318P)^2 + 1.060P]$          |
| 397 parameters   | where $P = (F_o^2 + 2F_c^2)/3$                            |
| 0 restraints   | $(\Delta/\sigma)_{\rm max} = 0.002$                       |
| Primary atom site location: structure-invariant                | $\Delta \rho_{\rm max} = 1.05 \text{ e } \text{\AA}^{-3}$ |
| direct methods   | $\Delta \rho_{\rm min} = -0.75 \text{ e} \text{ Å}^{-3}$  |

## Special details

**Geometry**. All e.s.d.'s (except the e.s.d. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell e.s.d.'s are taken into account individually in the estimation of e.s.d.'s in distances, angles and torsion angles; correlations between e.s.d.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell e.s.d.'s is used for estimating e.s.d.'s involving l.s. planes.

**Refinement**. Refinement of  $F^2$  against ALL reflections. The weighted *R*-factor *wR* and goodness of fit *S* are based on  $F^2$ , conventional *R*-factors *R* are based on *F*, with *F* set to zero for negative  $F^2$ . The threshold expression of  $F^2 > \sigma(F^2)$  is used only for calculating *R*-factors(gt) *etc.* and is not relevant to the choice of reflections for refinement. *R*-factors based on  $F^2$  are statistically about twice as large as those based on *F*, and *R*- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters  $(Å^2)$ 

|     | x            | У             | Ζ             | $U_{ m iso}$ */ $U_{ m eq}$ |  |
|-----|--------------|---------------|---------------|-----------------------------|--|
| I1  | 0.65947 (2)  | 0.703016 (18) | 0.295052 (16) | 0.03449 (6)                 |  |
| 01  | 0.53230 (19) | 0.40425 (16)  | 0.40367 (15)  | 0.0228 (4)                  |  |
| C1  | 0.5264 (2)   | 0.5248 (2)    | 0.3578 (2)    | 0.0184 (5)                  |  |
| H1  | 0.4776       | 0.5777        | 0.4103        | 0.022*                      |  |
| C2  | 0.6681 (3)   | 0.5206 (2)    | 0.3193 (2)    | 0.0216 (5)                  |  |
| H2  | 0.7177       | 0.4710        | 0.3743        | 0.026*                      |  |
| C3  | 0.7423 (3)   | 0.4681 (3)    | 0.2228 (2)    | 0.0278 (6)                  |  |
| H3A | 0.7611       | 0.3809        | 0.2388        | 0.033*                      |  |
| H3B | 0.8283       | 0.4796        | 0.1973        | 0.033*                      |  |
| C4  | 0.6631 (3)   | 0.5265 (3)    | 0.1397 (2)    | 0.0285 (6)                  |  |
| H4A | 0.7133       | 0.4889        | 0.0784        | 0.034*                      |  |
| H4B | 0.6493       | 0.6127        | 0.1201        | 0.034*                      |  |
| C5  | 0.5288 (3)   | 0.5116 (3)    | 0.1782 (2)    | 0.0228 (5)                  |  |
| H5A | 0.5438       | 0.4253        | 0.1913        | 0.027*                      |  |
| H5B | 0.4778       | 0.5523        | 0.1240        | 0.027*                      |  |
| C6  | 0.4460 (2)   | 0.5624 (2)    | 0.27622 (19)  | 0.0176 (5)                  |  |
| H6  | 0.4037       | 0.6517        | 0.2601        | 0.021*                      |  |
| C7  | 0.3390 (2)   | 0.5062 (2)    | 0.33450 (19)  | 0.0176 (5)                  |  |
| C8  | 0.4302 (3)   | 0.3834 (2)    | 0.3831 (2)    | 0.0212 (5)                  |  |
| H8A | 0.3792       | 0.3500        | 0.4472        | 0.025*                      |  |
| H8B | 0.4686       | 0.3260        | 0.3355        | 0.025*                      |  |
| C9  | 0.2348 (2)   | 0.5739 (2)    | 0.4198 (2)    | 0.0196 (5)                  |  |
| C10 | 0.1516 (3)   | 0.5193 (3)    | 0.4926 (2)    | 0.0241 (6)                  |  |
|     |              |               |               |                             |  |

| H10  | 0.1619       | 0.4411        | 0.4891        | 0.029*      |
|------|--------------|---------------|---------------|-------------|
| C11  | 0.0547 (3)   | 0.5757 (3)    | 0.5698 (2)    | 0.0304 (7)  |
| H11  | 0.0001       | 0.5360        | 0.6187        | 0.036*      |
| C12  | 0.0376 (3)   | 0.6890 (3)    | 0.5754 (2)    | 0.0314 (7)  |
| H12  | -0.0294      | 0.7283        | 0.6279        | 0.038*      |
| C13  | 0.1182 (3)   | 0.7460 (3)    | 0.5043 (2)    | 0.0302 (7)  |
| H13  | 0.1067       | 0.8244        | 0.5082        | 0.036*      |
| C14  | 0.2156 (3)   | 0.6888 (3)    | 0.4276 (2)    | 0.0241 (6)  |
| H14  | 0.2704       | 0.7288        | 0.3794        | 0.029*      |
| C15  | 0.2651 (2)   | 0.4991 (2)    | 0.2641 (2)    | 0.0195 (5)  |
| C16  | 0.2684 (3)   | 0.3913 (3)    | 0.2510 (2)    | 0.0250 (6)  |
| H16  | 0.3194       | 0.3175        | 0.2864        | 0.030*      |
| C17  | 0.1972 (3)   | 0.3913 (3)    | 0.1862 (2)    | 0.0300 (7)  |
| H17  | 0.2004       | 0.3174        | 0.1777        | 0.036*      |
| C18  | 0.1223 (3)   | 0.4975 (3)    | 0.1342 (2)    | 0.0296 (6)  |
| H18  | 0.0736       | 0.4969        | 0.0905        | 0.036*      |
| C19  | 0.1185 (3)   | 0.6049 (3)    | 0.1461 (2)    | 0.0311 (7)  |
| H19  | 0.0671       | 0.6783        | 0.1104        | 0.037*      |
| C20  | 0.1893 (3)   | 0.6057 (3)    | 0.2100 (2)    | 0.0260 (6)  |
| H20  | 0.1863       | 0.6800        | 0.2172        | 0.031*      |
| I1′  | 1.19069 (2)  | 1.181469 (19) | 0.013330 (16) | 0.03506 (7) |
| 01′  | 1.02918 (19) | 0.90326 (17)  | 0.12779 (15)  | 0.0251 (4)  |
| C1′  | 1.0347 (3)   | 1.0201 (2)    | 0.1134 (2)    | 0.0203 (5)  |
| H1′  | 0.9883       | 1.0756        | 0.0581        | 0.024*      |
| C2′  | 1.1807 (3)   | 1.0044 (3)    | 0.0810(2)     | 0.0245 (6)  |
| H2′  | 1.2252       | 0.9533        | 0.0270        | 0.029*      |
| C3′  | 1.2537 (3)   | 0.9465 (3)    | 0.1671 (2)    | 0.0305 (7)  |
| H3′1 | 1.3435       | 0.9502        | 0.1426        | 0.037*      |
| H3′2 | 1.2639       | 0.8610        | 0.1875        | 0.037*      |
| C4′  | 1.1806 (3)   | 1.0078 (3)    | 0.2598 (2)    | 0.0301 (6)  |
| H4′1 | 1.1757       | 1.0918        | 0.2411        | 0.036*      |
| H4′2 | 1.2300       | 0.9663        | 0.3150        | 0.036*      |
| C5′  | 1.0407 (3)   | 1.0052 (3)    | 0.2979 (2)    | 0.0256 (6)  |
| H5′1 | 0.9939       | 1.0483        | 0.3563        | 0.031*      |
| H5′2 | 1.0471       | 0.9210        | 0.3230        | 0.031*      |
| C6′  | 0.9582 (3)   | 1.0620 (2)    | 0.21581 (19)  | 0.0187 (5)  |
| H6′  | 0.9238       | 1.1514        | 0.2063        | 0.022*      |
| C7′  | 0.8417 (3)   | 1.0166 (2)    | 0.2427 (2)    | 0.0187 (5)  |
| C8′  | 0.9195 (3)   | 0.8919 (2)    | 0.2105 (2)    | 0.0229 (6)  |
| H8′1 | 0.9521       | 0.8306        | 0.2686        | 0.027*      |
| H8′2 | 0.8617       | 0.8680        | 0.1878        | 0.027*      |
| C9′  | 0.7693 (3)   | 1.0112 (2)    | 0.3550(2)     | 0.0195 (5)  |
| C10′ | 0.7127 (3)   | 1.1150 (2)    | 0.3963 (2)    | 0.0238 (6)  |
| H10′ | 0.7222       | 1.1868        | 0.3546        | 0.029*      |
| C11′ | 0.6425 (3)   | 1.1161 (3)    | 0.4972 (2)    | 0.0273 (6)  |
| H11′ | 0.6047       | 1.1879        | 0.5242        | 0.033*      |
| C12′ | 0.6277 (3)   | 1.0117 (3)    | 0.5583 (2)    | 0.0322 (7)  |
| H12′ | 0.5803       | 1.0116        | 0.6276        | 0.039*      |

| C13′ | 0.6820 (3) | 0.9087 (3) | 0.5183 (2) | 0.0368 (7) |  |
|------|------------|------------|------------|------------|--|
| H13′ | 0.6707     | 0.8376     | 0.5600     | 0.044*     |  |
| C14′ | 0.7535 (3) | 0.9072 (3) | 0.4174 (2) | 0.0295 (6) |  |
| H14′ | 0.7916     | 0.8349     | 0.3911     | 0.035*     |  |
| C15′ | 0.7364 (3) | 1.0920 (2) | 0.1781 (2) | 0.0198 (5) |  |
| C16′ | 0.6360 (3) | 1.0507 (3) | 0.1877 (2) | 0.0271 (6) |  |
| H16′ | 0.6351     | 0.9781     | 0.2331     | 0.032*     |  |
| C17′ | 0.5377 (3) | 1.1134 (3) | 0.1324 (2) | 0.0333 (7) |  |
| H17′ | 0.4708     | 1.0836     | 0.1398     | 0.040*     |  |
| C18′ | 0.5376 (3) | 1.2199 (3) | 0.0662 (2) | 0.0332 (7) |  |
| H18′ | 0.4704     | 1.2634     | 0.0283     | 0.040*     |  |
| C19′ | 0.6352 (3) | 1.2623 (3) | 0.0557 (2) | 0.0288 (6) |  |
| H19′ | 0.6356     | 1.3348     | 0.0100     | 0.035*     |  |
| C20′ | 0.7336 (3) | 1.1995 (2) | 0.1118 (2) | 0.0232 (6) |  |
| H20′ | 0.7995     | 1.2304     | 0.1047     | 0.028*     |  |
|      |            |            |            |            |  |

Atomic displacement parameters  $(Å^2)$ 

|     | $U^{11}$     | <i>U</i> <sup>22</sup> | $U^{33}$     | $U^{12}$      | $U^{13}$     | <i>U</i> <sup>23</sup> |
|-----|--------------|------------------------|--------------|---------------|--------------|------------------------|
| I1  | 0.04589 (13) | 0.03359 (11)           | 0.03171 (11) | -0.02655 (10) | -0.00455 (9) | -0.00285 (9)           |
| 01  | 0.0265 (10)  | 0.0197 (9)             | 0.0248 (10)  | -0.0122 (8)   | -0.0108 (8)  | 0.0038 (8)             |
| C1  | 0.0200 (12)  | 0.0202 (12)            | 0.0166 (12)  | -0.0102 (10)  | -0.0033 (9)  | -0.0018 (10)           |
| C2  | 0.0205 (12)  | 0.0250 (13)            | 0.0213 (13)  | -0.0099 (11)  | -0.0060 (10) | -0.0033 (11)           |
| C3  | 0.0201 (13)  | 0.0360 (16)            | 0.0271 (15)  | -0.0110 (12)  | -0.0010 (11) | -0.0089 (13)           |
| C4  | 0.0257 (14)  | 0.0394 (17)            | 0.0210 (14)  | -0.0141 (13)  | 0.0013 (11)  | -0.0102 (12)           |
| C5  | 0.0228 (13)  | 0.0294 (14)            | 0.0161 (12)  | -0.0088 (11)  | -0.0029 (10) | -0.0063 (11)           |
| C6  | 0.0182 (12)  | 0.0199 (12)            | 0.0147 (11)  | -0.0071 (10)  | -0.0038 (9)  | -0.0026 (9)            |
| C7  | 0.0196 (12)  | 0.0174 (12)            | 0.0169 (12)  | -0.0059 (10)  | -0.0055 (9)  | -0.0046 (9)            |
| C8  | 0.0210 (12)  | 0.0212 (13)            | 0.0228 (13)  | -0.0086 (10)  | -0.0065 (10) | -0.0029 (10)           |
| C9  | 0.0153 (11)  | 0.0247 (13)            | 0.0187 (12)  | -0.0040 (10)  | -0.0063 (9)  | -0.0060 (10)           |
| C10 | 0.0191 (12)  | 0.0350 (15)            | 0.0222 (13)  | -0.0129 (11)  | -0.0027 (10) | -0.0083 (12)           |
| C11 | 0.0211 (13)  | 0.054 (2)              | 0.0215 (14)  | -0.0184 (14)  | 0.0009 (11)  | -0.0130 (14)           |
| C12 | 0.0198 (13)  | 0.0466 (18)            | 0.0260 (15)  | -0.0042 (13)  | -0.0041 (11) | -0.0176 (14)           |
| C13 | 0.0314 (15)  | 0.0264 (15)            | 0.0288 (15)  | -0.0011 (12)  | -0.0084 (12) | -0.0124 (12)           |
| C14 | 0.0249 (13)  | 0.0256 (14)            | 0.0211 (13)  | -0.0072 (11)  | -0.0046 (10) | -0.0068 (11)           |
| C15 | 0.0177 (12)  | 0.0240 (13)            | 0.0181 (12)  | -0.0081 (10)  | -0.0014 (9)  | -0.0080 (10)           |
| C16 | 0.0250 (13)  | 0.0317 (15)            | 0.0224 (13)  | -0.0118 (12)  | -0.0052 (11) | -0.0089 (12)           |
| C17 | 0.0334 (16)  | 0.0384 (17)            | 0.0280 (15)  | -0.0209 (14)  | -0.0007 (12) | -0.0146 (13)           |
| C18 | 0.0249 (14)  | 0.0471 (18)            | 0.0237 (14)  | -0.0149 (13)  | -0.0040 (11) | -0.0153 (13)           |
| C19 | 0.0263 (14)  | 0.0367 (17)            | 0.0303 (16)  | -0.0055 (13)  | -0.0131 (12) | -0.0080 (13)           |
| C20 | 0.0242 (14)  | 0.0264 (14)            | 0.0295 (15)  | -0.0054 (11)  | -0.0106 (11) | -0.0089 (12)           |
| I1′ | 0.04789 (13) | 0.04025 (12)           | 0.02762 (11) | -0.02840 (10) | -0.00919 (9) | -0.00140 (9)           |
| O1′ | 0.0276 (10)  | 0.0228 (10)            | 0.0267 (10)  | -0.0111 (8)   | 0.0004 (8)   | -0.0114 (8)            |
| C1′ | 0.0239 (13)  | 0.0226 (13)            | 0.0178 (12)  | -0.0106 (11)  | -0.0045 (10) | -0.0054 (10)           |
| C2′ | 0.0231 (13)  | 0.0277 (14)            | 0.0253 (14)  | -0.0119 (11)  | -0.0034 (11) | -0.0070 (11)           |
| C3′ | 0.0236 (14)  | 0.0333 (16)            | 0.0356 (17)  | -0.0095 (12)  | -0.0092 (12) | -0.0064 (13)           |
| C4′ | 0.0323 (15)  | 0.0389 (17)            | 0.0255 (15)  | -0.0156 (13)  | -0.0140 (12) | -0.0026 (13)           |
| C5′ | 0.0287 (14)  | 0.0316 (15)            | 0.0187 (13)  | -0.0120 (12)  | -0.0084 (11) | -0.0028 (11)           |

| C6′  | 0.0228 (12) | 0.0205 (12) | 0.0164 (12) | -0.0098 (10) | -0.0043 (10) | -0.0054 (10) |  |
|------|-------------|-------------|-------------|--------------|--------------|--------------|--|
| C7′  | 0.0220 (12) | 0.0170 (12) | 0.0178 (12) | -0.0071 (10) | -0.0050 (10) | -0.0038 (10) |  |
| C8′  | 0.0238 (13) | 0.0207 (13) | 0.0243 (13) | -0.0077 (11) | -0.0044 (11) | -0.0059 (11) |  |
| C9′  | 0.0204 (12) | 0.0217 (13) | 0.0168 (12) | -0.0080 (10) | -0.0079 (10) | 0.0003 (10)  |  |
| C10′ | 0.0272 (14) | 0.0217 (13) | 0.0193 (13) | -0.0082 (11) | -0.0047 (10) | -0.0008 (10) |  |
| C11′ | 0.0246 (14) | 0.0322 (15) | 0.0232 (14) | -0.0079 (12) | -0.0044 (11) | -0.0069 (12) |  |
| C12′ | 0.0301 (15) | 0.0488 (19) | 0.0180 (13) | -0.0184 (14) | -0.0041 (11) | -0.0018 (13) |  |
| C13′ | 0.0483 (19) | 0.0392 (18) | 0.0256 (16) | -0.0266 (16) | -0.0056 (14) | 0.0037 (13)  |  |
| C14′ | 0.0421 (17) | 0.0270 (15) | 0.0247 (15) | -0.0193 (13) | -0.0089 (13) | -0.0004 (12) |  |
| C15′ | 0.0212 (12) | 0.0192 (12) | 0.0183 (12) | -0.0051 (10) | -0.0035 (10) | -0.0069 (10) |  |
| C16′ | 0.0264 (14) | 0.0330 (15) | 0.0233 (14) | -0.0133 (12) | -0.0041 (11) | -0.0048 (12) |  |
| C17′ | 0.0239 (14) | 0.0474 (19) | 0.0316 (16) | -0.0135 (14) | -0.0066 (12) | -0.0103 (14) |  |
| C18′ | 0.0244 (14) | 0.0414 (18) | 0.0288 (16) | -0.0018 (13) | -0.0119 (12) | -0.0084 (14) |  |
| C19′ | 0.0318 (15) | 0.0249 (14) | 0.0243 (14) | -0.0032 (12) | -0.0114 (12) | -0.0023 (11) |  |
| C20′ | 0.0259 (13) | 0.0242 (13) | 0.0199 (13) | -0.0081 (11) | -0.0073 (10) | -0.0038 (11) |  |
|      |             |             |             |              |              |              |  |

Geometric parameters (Å, °)

| IIC2 $2.175 (3)$ II'C2' $2.1$ O1C8 $1.421 (3)$ O1'C8' $1.4$ O1C1 $1.442 (3)$ O1'C1' $1.4$ C1C2 $1.518 (4)$ C1'C2' $1.5$ C1C6 $1.534 (4)$ C1'C6' $1.5$ C1H1 $1.0000$ C1'H1' $1.000$ C2C3 $1.514 (4)$ C2'C3' $1.5$ C2H2 $1.0000$ C2'-H2' $1.000$ C3C4 $1.524 (4)$ C3'C4' $1.5$ |         |
|--|---------|
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 183 (3) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 439 (3) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 444 (3) |
| $\begin{array}{cccccccccccccccccccccccccccccccccccc$   | 522 (4) |
| C1—H11.0000C1'—H1'1.0C2—C31.514 (4)C2'—C3'1.5C2—H21.0000C2'—H2'1.0C3—C41.524 (4)C3'—C4'1.5   | 534 (3) |
| C2-C31.514 (4)C2'-C3'1.5C2-H21.0000C2'-H2'1.0C3-C41.524 (4)C3'-C4'1.5  | 0000    |
| C2—H2       1.0000       C2'—H2'       1.0         C3—C4       1.524 (4)       C3'—C4'       1.5   | 515 (4) |
| C3—C4 1.524 (4) C3'—C4' 1.5  | 0000    |
|  | 523 (4) |
| C3—H3A 0.9900 C3'—H3'1 0.9   | 9900    |
| C3—H3B 0.9900 C3'—H3'2 0.9   | 9900    |
| C4—C5 1.528 (4) C4′—C5′ 1.5  | 526 (4) |
| C4—H4A 0.9900 C4'—H4'1 0.9   | 9900    |
| C4—H4B 0.9900 C4'—H4'2 0.9   | 9900    |
| C5—C6 1.536 (3) C5'—C6' 1.5  | 535 (4) |
| C5—H5A 0.9900 C5'—H5'1 0.9   | 9900    |
| C5—H5B 0.9900 C5'—H5'2 0.9   | 9900    |
| C6—C7 1.556 (3) C6'—C7' 1.5  | 560 (4) |
| С6—Н6 1.0000 С6'—Н6' 1.0   | 0000    |
| C7—C15 1.526 (4) C7′—C9′ 1.5   | 527 (4) |
| C7—C9 1.547 (3) C7′—C15′ 1.5   | 545 (4) |
| C7—C8 1.550 (4) C7′—C8′ 1.5  | 553 (4) |
| C8—H8A 0.9900 C8'—H8'1 0.9   | 9900    |
| C8—H8B 0.9900 C8'—H8'2 0.9   | 9900    |
| C9—C14 1.393 (4) C9′—C10′ 1.3  | 388 (4) |
| C9—C10 1.396 (4) C9′—C14′ 1.3  | 392 (4) |
| C10—C11 1.384 (4) C10′—C11′ 1.3  | 389 (4) |
| C10—H10 0.9500 C10'—H10' 0.9   | 9500    |
| C11—C12 1.370 (5) C11′—C12′ 1.3  | 386 (4) |
| C11—H11 0.9500 C11'—H11' 0.9   |         |

| C12—C13                         | 1.385 (4)          | C12′—C13′  | 1.372 (5)              |
|---------------------------------|--------------------|--|------------------------|
| C12—H12                         | 0.9500             | C12'—H12'  | 0.9500                 |
| C13—C14                         | 1.385 (4)          | C13′—C14′  | 1.392 (4)              |
| C13—H13                         | 0.9500             | C13'—H13'  | 0.9500                 |
| C14—H14                         | 0.9500             | C14′—H14′  | 0.9500                 |
| C15—C16                         | 1.398 (4)          | C15′—C20′  | 1.393 (4)              |
| $C_{15}$ $C_{20}$               | 1 399 (4)          | C15' - C16'  | 1 401 (4)              |
| $C_{16}$ $C_{17}$               | 1 395 (4)          | C16' - C17'  | 1 388 (4)              |
| C16—H16                         | 0.9500             | C16' - H16'  | 0.9500                 |
| C17-C18                         | 1.380(5)           | C10 - 110<br>C17' - C18'   | 1 388 (5)              |
| C17 H17                         | 0.9500             | C17' H17'  | 0.9500                 |
| $C_{1}^{18}$ $C_{10}^{10}$      | 1.383(4)           | C18' - C19'  | 1.378(4)               |
| $C_{10}$                        | 1.363 (4)          | $C_{10} - C_{19}$  | 1.578 (4)              |
|                                 | 0.9300             |  | 0.9300                 |
| C19—C20                         | 1.380 (4)          | C19 - C20  | 1.396 (4)              |
| C19—H19                         | 0.9500             | C19'—H19'  | 0.9500                 |
| C20—H20                         | 0.9500             | C20'—H20'  | 0.9500                 |
| C8 01 C1                        | 110.04 (10)        | $C^{0}$ $O^{1}$ $C^{1}$  | 100 76 (10)            |
| $C_0 = C_1 = C_1$               | 110.04(19)         | $C_{8} = 01 = C_{1}$   | 109.70(19)<br>107.0(2) |
| 01-C1-C2                        | 107.4 (2)          | 01 - 01 - 02   | 107.0 (2)              |
| OI - CI - C6                    | 104.0(2)           | $01^{-}$   | 104.5 (2)              |
| C2-CI-C6                        | 116.3 (2)          | C2' = C1' = C6'  | 116.3 (2)              |
| OI—CI—HI                        | 109.6              |  | 109.6                  |
| C2—C1—H1                        | 109.6              | C2'—C1'—H1'  | 109.6                  |
| C6—C1—H1                        | 109.6              | C6'—C1'—H1'  | 109.6                  |
| C3—C2—C1                        | 114.5 (2)          | C3'—C2'—C1'  | 114.1 (2)              |
| C3—C2—I1                        | 110.48 (19)        | C3'—C2'—I1'  | 110.34 (19)            |
| C1—C2—I1                        | 107.01 (17)        | C1'—C2'—I1'  | 107.33 (18)            |
| С3—С2—Н2                        | 108.2              | C3'—C2'—H2'  | 108.3                  |
| C1—C2—H2                        | 108.2              | C1'—C2'—H2'  | 108.3                  |
| I1—C2—H2                        | 108.2              | I1′—C2′—H2′  | 108.3                  |
| C2—C3—C4                        | 111.7 (2)          | C2'—C3'—C4'  | 112.0 (2)              |
| С2—С3—НЗА                       | 109.3              | C2'—C3'—H3'1   | 109.2                  |
| C4—C3—H3A                       | 109.3              | C4′—C3′—H3′1   | 109.2                  |
| С2—С3—Н3В                       | 109.3              | C2'—C3'—H3'2   | 109.2                  |
| С4—С3—Н3В                       | 109.3              | C4′—C3′—H3′2   | 109.2                  |
| НЗА—СЗ—НЗВ                      | 108.0              | H3'1—C3'—H3'2  | 107.9                  |
| C3—C4—C5                        | 110.1 (2)          | C3'—C4'—C5'  | 110.2 (2)              |
| C3-C4-H4A                       | 109.6              | C3'-C4'-H4'1   | 109.6                  |
| $C_{5}$ $C_{4}$ $H_{4A}$        | 109.6              | C5' - C4' - H4'1   | 109.6                  |
| $C_3 - C_4 - H_4B$              | 109.6              | C3' - C4' - H4'2   | 109.0                  |
| $C_5 C_4 H_{4B}$                | 109.6              | C5' C4' H4'2   | 109.0                  |
|                                 | 109.0              | $H_{11} = C_{11} + C$ | 109.0                  |
| $H_{A} = C_{4} = H_{4} = H_{4}$ | 100.2<br>112 5 (2) | H4 I - C4 - H4 2   | 100.1<br>112.6(2)      |
| $C_{1} = C_{2} = C_{0}$         | 113.3(2)           | $C_4 = C_3 = C_0$  | 115.0 (2)              |
| $C_4 - C_5 - \Pi 5 A$           | 100.9              | C4 - C3 - H5'I   | 108.8                  |
| CO-CS-HSD                       | 108.9              | $C_0 - C_3 - H_3 I$  | 108.8                  |
| C4-C5-H5B                       | 108.9              | $C4^{-}$ $C5^{-}$ $H5^{\prime}2$   | 108.8                  |
| CO-CO-HSB                       | 108.9              | C6'-C5'-H5'2   | 108.8                  |
| нэд—Сэ—Нэв                      | 107.7              | H5'I-C5'-H5'2  | 107.7                  |

| C1—C6—C5                   | 112.9 (2)            | C1'—C6'—C5'                  | 112.9 (2)            |
|----------------------------|----------------------|------------------------------|----------------------|
| C1—C6—C7                   | 100.37 (19)          | C1'—C6'—C7'                  | 100.5 (2)            |
| C5—C6—C7                   | 111.6 (2)            | C5'—C6'—C7'                  | 111.4 (2)            |
| С1—С6—Н6                   | 110.5                | C1'—C6'—H6'                  | 110.6                |
| С5—С6—Н6                   | 110.5                | С5'—С6'—Н6'                  | 110.6                |
| С7—С6—Н6                   | 110.5                | С7'—С6'—Н6'                  | 110.6                |
| C15—C7—C9                  | 108.0 (2)            | C9'—C7'—C15'                 | 107.4 (2)            |
| C15—C7—C8                  | 114.7 (2)            | C9'—C7'—C8'                  | 113.8 (2)            |
| <u>C9–C7–C8</u>            | 109.6 (2)            | C15'-C7'-C8'                 | 109.0(2)             |
| $C_{15} - C_{7} - C_{6}$   | 112.9(2)             | C9'-C7'-C6'                  | 103.0(2)<br>113.4(2) |
| C9-C7-C6                   | 112.9(2)<br>113.0(2) | $C_{15'} - C_{7'} - C_{6'}$  | 113.1(2)             |
| $C_{8}$ $C_{7}$ $C_{6}$    | 98 61 (19)           | C8' - C7' - C6'              | 99.6(2)              |
| $C_{0} = C_{1} = C_{0}$    | 106.6(2)             | $C_{0} = C_{1} = C_{0}$      | 106.6(2)             |
| O1 C8 H8A                  | 110.0 (2)            | 01 - 03 - 07                 | 100.0(2)             |
| $C_{1}$                    | 110.4                | $C_1 - C_0 - H_0 I$          | 110.4                |
| $C = C = H \delta A$       | 110.4                | $C/-C_{0}$ H8 1              | 110.4                |
| 01—C8—H8B                  | 110.4                | $O1^{-}$ $C8^{-}$ $H8^{2}$   | 110.4                |
| C/—C8—H8B                  | 110.4                | C//                          | 110.4                |
| H8A—C8—H8B                 | 108.6                | H8'1—C8'—H8'2                | 108.6                |
| C14—C9—C10                 | 117.0 (2)            | C10'—C9'—C14'                | 118.3 (3)            |
| C14—C9—C7                  | 124.0 (2)            | C10'—C9'—C7'                 | 118.9 (2)            |
| C10—C9—C7                  | 118.9 (2)            | C14'—C9'—C7'                 | 122.8 (2)            |
| C11—C10—C9                 | 121.9 (3)            | C9'—C10'—C11'                | 121.4 (3)            |
| C11—C10—H10                | 119.0                | C9'—C10'—H10'                | 119.3                |
| С9—С10—Н10                 | 119.0                | C11'—C10'—H10'               | 119.3                |
| C12—C11—C10                | 119.9 (3)            | C12'—C11'—C10'               | 119.6 (3)            |
| C12—C11—H11                | 120.1                | C12'—C11'—H11'               | 120.2                |
| C10—C11—H11                | 120.1                | C10′—C11′—H11′               | 120.2                |
| C11—C12—C13                | 119.8 (3)            | C13'—C12'—C11'               | 119.6 (3)            |
| C11—C12—H12                | 120.1                | C13'—C12'—H12'               | 120.2                |
| C13—C12—H12                | 120.1                | C11′—C12′—H12′               | 120.2                |
| C14-C13-C12                | 120.2 (3)            | C12'—C13'—C14'               | 120.8 (3)            |
| C14—C13—H13                | 119.9                | C12'-C13'-H13'               | 119.6                |
| C12—C13—H13                | 119.9                | C14'-C13'-H13'               | 119.6                |
| C12 - C13 - C14 - C9       | 121.3 (3)            | $C_{0'} - C_{14'} - C_{13'}$ | 120.2(3)             |
| $C_{13}$ $C_{14}$ $H_{14}$ | 110 /                | $C_{0}$ $C_{14}$ $H_{14}$    | 110.0                |
| $C_{13}$ $C_{14}$ $H_{14}$ | 119.4                | $C_{3} - C_{14} - H_{14}$    | 119.9                |
| $C_{16} = C_{15} = C_{20}$ | 117.7                | $C_{13} = C_{14} = 1114$     | 117.7 (2)            |
| C10 - C15 - C20            | 117.9(3)             | $C_{20} = C_{15} = C_{10}$   | 117.7(3)             |
| C10 - C15 - C7             | 123.3 (2)            | $C_{20} = C_{13} = C_{7}$    | 124.2 (2)            |
| $C_{20} = C_{15} = C_{7}$  | 118.7 (2)            |                              | 118.1 (2)            |
| C17—C16—C15                | 120.5 (3)            | C17' - C16' - C15'           | 121.5 (3)            |
| С17—С16—Н16                | 119.7                | C17′—C16′—H16′               | 119.2                |
| C15—C16—H16                | 119.7                | C15'—C16'—H16'               | 119.2                |
| C18—C17—C16                | 120.6 (3)            | C18'—C17'—C16'               | 119.7 (3)            |
| C18—C17—H17                | 119.7                | C18'—C17'—H17'               | 120.1                |
| C16—C17—H17                | 119.7                | C16'—C17'—H17'               | 120.1                |
| C17—C18—C19                | 119.5 (3)            | C19'—C18'—C17'               | 119.7 (3)            |
| C17—C18—H18                | 120.2                | C19'—C18'—H18'               | 120.1                |
| C19—C18—H18                | 120.2                | C17'—C18'—H18'               | 120.1                |

| C18—C19—C20     | 120.2 (3)    | C18′—C19′—C20′      | 120.5 (3)   |
|-----------------|--------------|---------------------|-------------|
| C18—C19—H19     | 119.9        | C18'—C19'—H19'      | 119.8       |
| С20—С19—Н19     | 119.9        | С20'—С19'—Н19'      | 119.8       |
| C19—C20—C15     | 121.3 (3)    | C15'—C20'—C19'      | 120.8 (3)   |
| C19—C20—H20     | 119.4        | C15'—C20'—H20'      | 119.6       |
| C15—C20—H20     | 119.4        | C19'—C20'—H20'      | 119.6       |
|                 |              |                     |             |
| C8—O1—C1—C2     | -143.3 (2)   | C8'—O1'—C1'—C2'     | 145.4 (2)   |
| C8—O1—C1—C6     | -19.5 (3)    | C8′—O1′—C1′—C6′     | 21.4 (3)    |
| O1—C1—C2—C3     | 74.7 (3)     | O1'—C1'—C2'—C3'     | -74.9 (3)   |
| C6—C1—C2—C3     | -41.2 (3)    | C6'—C1'—C2'—C3'     | 41.4 (3)    |
| O1—C1—C2—I1     | -162.47 (16) | O1'—C1'—C2'—I1'     | 162.51 (16) |
| C6—C1—C2—I1     | 81.6 (2)     | C6'—C1'—C2'—I1'     | -81.2 (2)   |
| C1—C2—C3—C4     | 50.6 (3)     | C1'—C2'—C3'—C4'     | -50.7 (3)   |
| I1—C2—C3—C4     | -70.3 (3)    | I1′—C2′—C3′—C4′     | 70.2 (3)    |
| C2—C3—C4—C5     | -58.0 (3)    | C2'—C3'—C4'—C5'     | 57.8 (3)    |
| C3—C4—C5—C6     | 56.8 (3)     | C3'—C4'—C5'—C6'     | -56.4 (3)   |
| O1—C1—C6—C5     | -79.3 (2)    | O1′—C1′—C6′—C5′     | 79.0 (3)    |
| C2-C1-C6-C5     | 38.5 (3)     | C2'—C1'—C6'—C5'     | -38.7 (3)   |
| O1—C1—C6—C7     | 39.7 (2)     | O1′—C1′—C6′—C7′     | -39.8 (2)   |
| C2-C1-C6-C7     | 157.5 (2)    | C2′—C1′—C6′—C7′     | -157.4 (2)  |
| C4—C5—C6—C1     | -46.6 (3)    | C4′—C5′—C6′—C1′     | 46.5 (3)    |
| C4—C5—C6—C7     | -158.8 (2)   | C4′—C5′—C6′—C7′     | 158.6 (2)   |
| C1—C6—C7—C15    | -164.5 (2)   | C1′—C6′—C7′—C9′     | 162.8 (2)   |
| C5—C6—C7—C15    | -44.6 (3)    | C5'—C6'—C7'—C9'     | 43.0 (3)    |
| C1—C6—C7—C9     | 72.6 (2)     | C1′—C6′—C7′—C15′    | -74.1 (2)   |
| C5—C6—C7—C9     | -167.5 (2)   | C5'—C6'—C7'—C15'    | 166.0 (2)   |
| C1—C6—C7—C8     | -43.0 (2)    | C1′—C6′—C7′—C8′     | 41.6 (2)    |
| C5—C6—C7—C8     | 76.9 (2)     | C5'—C6'—C7'—C8'     | -78.2 (2)   |
| C1—O1—C8—C7     | -9.2 (3)     | C1′—O1′—C8′—C7′     | 6.3 (3)     |
| C15—C7—C8—O1    | 153.3 (2)    | C9′—C7′—C8′—O1′     | -151.4 (2)  |
| C9—C7—C8—O1     | -85.2 (2)    | C15'—C7'—C8'—O1'    | 88.8 (3)    |
| C6-C7-C8-O1     | 33.1 (2)     | C6'—C7'—C8'—O1'     | -30.4 (3)   |
| C15—C7—C9—C14   | -109.6 (3)   | C15'—C7'—C9'—C10'   | -68.6 (3)   |
| C8—C7—C9—C14    | 124.8 (3)    | C8′—C7′—C9′—C10′    | 170.7 (2)   |
| C6-C7-C9-C14    | 16.0 (4)     | C6'—C7'—C9'—C10'    | 57.8 (3)    |
| C15—C7—C9—C10   | 68.7 (3)     | C15'—C7'—C9'—C14'   | 109.2 (3)   |
| C8—C7—C9—C10    | -56.9 (3)    | C8′—C7′—C9′—C14′    | -11.6 (4)   |
| C6-C7-C9-C10    | -165.8 (2)   | C6'—C7'—C9'—C14'    | -124.4 (3)  |
| C14—C9—C10—C11  | -0.4 (4)     | C14′—C9′—C10′—C11′  | 0.3 (4)     |
| C7—C9—C10—C11   | -178.8 (2)   | C7'—C9'—C10'—C11'   | 178.2 (3)   |
| C9—C10—C11—C12  | 0.6 (4)      | C9′—C10′—C11′—C12′  | -0.3 (4)    |
| C10-C11-C12-C13 | -0.5 (5)     | C10'—C11'—C12'—C13' | -0.4 (5)    |
| C11—C12—C13—C14 | 0.2 (5)      | C11'—C12'—C13'—C14' | 0.9 (5)     |
| C12—C13—C14—C9  | 0.1 (5)      | C10'—C9'—C14'—C13'  | 0.3 (4)     |
| C10—C9—C14—C13  | 0.0 (4)      | C7'—C9'—C14'—C13'   | -177.5 (3)  |
| C7—C9—C14—C13   | 178.3 (3)    | C12'—C13'—C14'—C9'  | -0.9 (5)    |
| C9—C7—C15—C16   | -116.8 (3)   | C9'—C7'—C15'—C20'   | 118.0 (3)   |
|                 |              |                     |             |

| $\begin{array}{c} C8 & -C7 & -C15 & -C16\\ C6 & -C7 & -C15 & -C16\\ C9 & -C7 & -C15 & -C20\\ C8 & -C7 & -C15 & -C20\\ C6 & -C7 & -C15 & -C20\\ C20 & -C15 & -C16 & -C17\\ C7 & -C15 & -C16 & -C17\\ C15 & -C16 & -C17 & -C18\\ C16 & -C17 & -C18 & -C19\\ C17 & -C18 & -C19 & -C20\\ C18 & -C19 & -C20 & -C15\\ C16 & -C15 & -C20 & -C19\\ \end{array}$ | 5.7 (4)<br>117.6 (3)<br>62.9 (3)<br>-174.7 (2)<br>-62.7 (3)<br>-0.3 (4)<br>179.3 (2)<br>-0.2 (4)<br>0.4 (4)<br>-0.1 (5)<br>-0.4 (5)<br>0.6 (4) | $\begin{array}{c} C8'-C7'-C15'-C20'\\ C6'-C7'-C15'-C20'\\ C9'-C7'-C15'-C16'\\ C8'-C7'-C15'-C16'\\ C6'-C7'-C15'-C16'\\ C20'-C15'-C16'-C17'\\ C7'-C15'-C16'-C17'\\ C15'-C16'-C17'\\ C15'-C16'-C17'\\ C15'-C16'-C19'\\ C16'-C17'-C18'-C19'\\ C16'-C15'-C20'-C19'\\ C7'-C15'-C20'-C19'\\ C7'-C15'-C20'-C19'\\ \end{array}$ | $\begin{array}{c} -118.3 (3) \\ -8.3 (3) \\ -61.1 (3) \\ 62.6 (3) \\ 172.6 (2) \\ 0.8 (4) \\ 179.9 (3) \\ -0.3 (5) \\ 0.2 (5) \\ -0.6 (5) \\ -1.1 (4) \\ 179.8 (2) \end{array}$ |
|---|--|--|---|
| C16—C15—C20—C19   | 0.6 (4)  | C18'—C19'—C20'—C19'  | 1/9.8 (2)   |
| C7—C15—C20—C19  | -179.0 (3)   | C18'—C19'—C20'—C15'  | 1.0 (4)   |

## Hydrogen-bond geometry (Å, °)

Cg1 and Cg2 are the centroids of the C9–C14 and C15'–C20' rings, respectively.

| D—H···A                       | <i>D</i> —Н | H···A | D····A    | D—H···A |
|-------------------------------|-------------|-------|-----------|---------|
| $C2$ — $H2$ ··· $Cg1^i$       | 1.00        | 2.53  | 3.519 (3) | 171     |
| $C2'$ — $H2'$ ···· $Cg2^{ii}$ | 1.00        | 2.54  | 3.533 (3) | 171     |

Symmetry codes: (i) -*x*+1, -*y*+1, -*z*+1; (ii) -*x*+2, -*y*+2, -*z*.