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Twinned caesium cerium(IV) pentafluoride

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Key indicators: single-crystal X-ray study; $T = 295$ K; mean $\sigma(\text{Ce}-\text{F}) = 0.006$ Å; R factor = 0.037; wR factor = 0.038; data-to-parameter ratio = 49.6.

Single-crystals of CsCeF_5 were synthesized hydrothermally. The crystal under investigation was twinned by pseudo-merohedry with a twofold rotation around the c axis as an additional twinning operation. The crystal structure is built of layers of distorted edge- and corner-sharing CeF_8 square-antiprisms. The Cs^+ cations are located between the layers and exhibit coordination numbers of nine. Upon compression, CsCeF_5 undergoes an irreversible phase transition at about 1 GPa.

Related literature

For background to the applications of complex cerium(IV) and thorium fluorides, see: Friese *et al.* (2011); Grzechnik *et al.* (2007, 2008, 2013a,b); Rouse & Weller (2009); Underwood (2013); Underwood *et al.* (2012). For related structures, see: Underwood *et al.* (2012). The ruby luminescence method (Mao *et al.*, 1986) was used for pressure calibration. According to a recent review of twinning at high pressures (Friese & Grzechnik, 2014), pseudo-merohedral twinning in general is not significantly affected on compression.

Experimental

Crystal data

CsCeF_5	$V = 968.39$ (9) Å ³
$M_r = 368$	$Z = 8$
Monoclinic, $P2_1/c$	Mo $K\alpha$ radiation
$a = 8.3125$ (5) Å	$\mu = 16.80$ mm ⁻¹
$b = 14.2434$ (6) Å	$T = 295$ K
$c = 8.4507$ (5) Å	$0.10 \times 0.08 \times 0.05$ mm
$\beta = 104.566$ (5)°	

Data collection

STOE IPDS 2 diffractometer	55729 measured reflections
Absorption correction: numerical (X -SHAPE; Stoe & Cie, 2002)	6402 independent reflections
$T_{\min} = 0.207$, $T_{\max} = 0.406$	2543 reflections with $I > 3\sigma(I)$
	$R_{\text{int}} = 0.136$

Refinement

$R[F^2 > 2\sigma(F^2)] = 0.037$	129 parameters
$wR(F^2) = 0.038$	$\Delta\rho_{\text{max}} = 1.85$ e Å ⁻³
$S = 1.04$	$\Delta\rho_{\text{min}} = -1.89$ e Å ⁻³
6402 reflections	

Table 1

Selected bond lengths (Å).

Ce1—F3	2.133 (6)	Cs1—F1 ^{iv}	2.928 (8)
Ce1—F4	2.304 (5)	Cs1—F2	3.152 (6)
Ce1—F5	2.256 (6)	Cs1—F2 ^v	2.982 (6)
Ce1—F5 ⁱ	2.311 (6)	Cs1—F3 ^{vi}	3.222 (7)
Ce1—F6	2.320 (5)	Cs1—F3 ^{vii}	3.229 (7)
Ce1—F7	2.306 (6)	Cs1—F5 ^{vi}	3.099 (6)
Ce1—F8	2.119 (7)	Cs1—F8	3.095 (6)
Ce1—F9	2.487 (6)	Cs1—F8 ^{vii}	3.218 (6)
Ce1—F9 ⁱ	2.882 (7)	Cs1—F9	2.982 (5)
Ce2—F1	2.123 (7)	Cs2—F1 ^{vi}	2.998 (6)
Ce2—F2	2.128 (7)	Cs2—F1 ^{viii}	2.998 (7)
Ce2—F4 ⁱⁱ	2.329 (5)	Cs2—F2 ^{ix}	3.042 (8)
Ce2—F6	2.395 (6)	Cs2—F3 ^{vi}	3.437 (6)
Ce2—F6 ⁱⁱⁱ	3.150 (7)	Cs2—F3 ^{viii}	2.981 (6)
Ce2—F7 ⁱⁱⁱ	2.322 (6)	Cs2—F6 ^{vi}	3.125 (6)
Ce2—F9	2.304 (6)	Cs2—F7 ^{vii}	3.140 (6)
Ce2—F10	2.242 (5)	Cs2—F8	2.980 (7)
Ce2—F10 ⁱ	2.279 (6)	Cs2—F10 ^{viii}	3.162 (6)

Symmetry codes: (i) $x, -y + \frac{3}{2}, z - \frac{1}{2}$; (ii) $x + 1, -y + \frac{3}{2}, z + \frac{1}{2}$; (iii) $x, -y + \frac{3}{2}, z + \frac{1}{2}$; (iv) $-x + 2, y - \frac{1}{2}, -z + \frac{1}{2}$; (v) $-x + 2, -y + 1, -z + 1$; (vi) $-x + 1, y - \frac{1}{2}, -z + \frac{1}{2}$; (vii) $-x + 1, -y + 1, -z$; (viii) $x - 1, -y + \frac{3}{2}, z - \frac{1}{2}$; (ix) $x - 1, y, z$.

Data collection: *X-AREA* (Stoe & Cie, 2002); cell refinement: *X-AREA*; data reduction: *X-AREA*; program(s) used to solve structure: *SIR97* (Altomare *et al.*, 1999); program(s) used to refine structure: *JANA2006* (Petříček *et al.*, 2006); molecular graphics: *DIAMOND* (Brandenburg, 2000); software used to prepare material for publication: *publCIF* (Westrip, 2010).

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Supporting information for this paper is available from the IUCr electronic archives (Reference: FJ2660).

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Twinned caesium cerium(IV) pentafluoride

Andrzej Grzechnik, Christopher C. Underwood and Joseph W. Kolis

S1. Introduction

Most of the work on structural inorganic chemistry of actinide fluorides has been primarily based on the materials that crystallize from molten alkali fluoride salts (Grzechnik *et al.*, 2007; Grzechnik *et al.*, 2008; Friese *et al.*, 2011). Recently, several complex thorium fluorides have been synthesized (Underwood *et al.*, 2012; Grzechnik *et al.*, 2013a) and advances in the synthesis of cerium (IV) fluorides have been made (Rouse *et al.*, 2009; Grzechnik *et al.*, 2013b). The successful use of fluoride mineralizers in the hydrothermal crystal growth of alkali thorium fluorides suggests that additional investigations into inorganic cerium (IV) fluorides may be fruitful. The chemistry of monovalent metal cerium(IV) fluorides in hydrothermal fluids was examined by Underwood (2013) and it was found that it is considerably richer than anticipated.

We are interested in the crystal structures and stabilities of cerium (IV) fluorides as they are thought to be isostructural with the actinide fluorides (Grzechnik *et al.*, 2013b). In the recent study by Underwood *et al.* (2012), three new polymorphs of CsThF₅ have been synthesized hydrothermally. The tetragonal phase (phase I, P4/nmm, Z = 2), consisting of sheets of ThF₉ tricapped trigonal prisms separated by layers of Cs atoms, is a minor product in the hydrothermal conditions. Two monoclinic polymorphs (phases II and III) are synthesized at various conditions. The phase II (P2₁/c, Z = 4) is built of chains of corner-sharing ThF₉ polyhedra, while the phase III (P2₁/c, Z = 8) is built of sheets of edge- and corner-sharing ThF₉ polyhedra. The chain structure of the phase II converts into the sheet structure of the phase III at 500°C. In this study, we examine cesium cerium(IV) pentafluoride, CsCeF₅, to see whether it is indeed isostructural with CsThF₅.

S2. Experimental

A series of crystals mounted on glass pins was tested on a STOE IPDS 2 diffractometer and the best one was selected for the structure determination at ambient conditions and high-pressure single-crystal x-ray studies. High-pressure data were collected in the Ahsbabs-type diamond anvil cell at room temperature at 1.2, 3.1, and 5.0 GPa. A 0.250 mm hole was drilled into a stainless steel gasket preindented to a thickness of about 0.120 mm. A 4:1 mixture of methanol and ethanol was used as a pressure medium. The ruby luminescence method (Mao *et al.*, 1986) was used for pressure calibration.

The intensities were indexed and integrated with the software *X-AREA* (Stoe & Cie, 2002). Due to the pseudomerohedral twinning, some reflections in the lower θ range partly overlap. During the integration the orientation matrices of both twin individuals were used simultaneously. The overlap tolerance was set to 100%, so that all overlapped reflections were included. The faces of the crystal were optimized for each individual with the program *X-SHAPE* (Stoe & Cie, 2002) and an absorption correction was applied with the program *Jana2006* (Petříček *et al.*, 2006). Figures 1-3 were drawn using the program *DIAMOND* (Brandenburg, 2000).

S2.1. Synthesis and crystallization

All reagents for the synthesis of CsCeF₅ were of analytical grade and used as purchased. The compound in this study was prepared hydrothermally as follows: 0.20 g CeF₄ (Strem Chemical, 99.9%) was combined with five molar equivalents (0.703 g) of CsF (Alfa Aesar, 99.9%), placed into a Parr Instruments Teflon-lined autoclave and filled with 10.0 mL water. The autoclave was then heated at 250 °C for 24 h and slowly cooled at a rate of 10 °C/h to room temperature. When the reaction was complete, the content of the autoclave was filtered and the product washed with deionized water to yield a colorless material. Powder X-ray diffraction was used to characterize the bulk solid and single crystal X-ray diffraction was used to structurally characterize the new species.

S2.2. Refinement

Crystal data, data collection and structure refinement details at ambient conditions are summarized in Table 1. The diffraction pattern could be explained assuming a monoclinic lattice with $a = 8.3125$ (5) Å, $b = 14.2434$ (6) Å, $c = 8.4507$ (5) Å, and $\beta = 104.566$ (5)° and a two-fold rotation around the c axis as an additional twinning operation. The twinning matrix corresponds to (-1, 0, -0.4948; 0, -1, 0; 0, 0, 1). The twinning could be classified as pseudomerohedral.

The structure was solved with the program SIR97 (Altomare *et al.*, 1999) and it was refined with the program Jana2006 (Petříček *et al.*, 2006). The reflections from both individuals and the twinning operation were taken into account during the refinement process. The refined twin volumes of the two individuals are 0.8830 (7) and 0.1170 (7).

S3. Results and discussion

All the examined crystals of CsCeF₅ are pseudomerohedrally twinned and have their lattice parameters close to those for the high-temperature polymorph of CsThF₅ (phase III) (Underwood *et al.*, 2012). We do not find any material whose single-crystal or powder x-ray intensities could be indexed with the lattices analogous to those in the phases I and II of CsThF₅. It indicates that CsCeF₅ does not exhibit any temperature-induced polymorphism within the synthesis conditions.

The analysis of the structural data in Table 2 shows that, unlike the Th atoms in the phase III of CsThF₅, the Ce atoms are eight-fold coordinated to the fluorine atoms in the distorted square antiprismatic geometry (Figure 1): the distances Ce1—F and Ce2—F are in the ranges 2.12–2.49 Å and 2.12–2.40 Å, respectively. The average Ce1—F and Ce2—F distances are the same: 2.3 (1) Å. The doublets of edge-sharing CeF₈ polyhedra share their corners to form sheets perpendicular to the b axis (Figures 2 and 3). The Cs atoms are between the sheets and are coordinated to nine fluorine atoms. The average distances Cs1—F and Cs2—F are identical: 3.1 (1) Å. Altogether, it is clear from our data that, unlike LiCeF₅ and LiThF₅ (Grzechnik *et al.*, 2013b), CsCeF₅ and CsThF₅ are not isostructural at ambient conditions. This suggests that inorganic structural chemistries of actinide and lanthanide (IV) fluorides are not exactly analogous.

Above about 1 GPa, the single-crystal x-ray reflections in CsCeF₅ lose their intensities, become broadened and smeared, while the crystal itself is cracked into tiny pieces. The reflections can no longer be indexed with any lattice and integrated. These changes in the diffraction pattern are irreversible on decompression to atmospheric conditions. Such a behaviour suggests a pressure-induced first-order phase transition in CsCeF₅. According to a recent review of twinned structures at high pressures (Friesse *et al.*, 2014), pseudomerohedral twinning in general is not significantly affected on compression. The broadening and smearing of the reflections could thus rather be due to the collapse of the layer structure. However, the structure of the pressure-induced form of this material cannot be determined from the current single-crystal x-ray data.

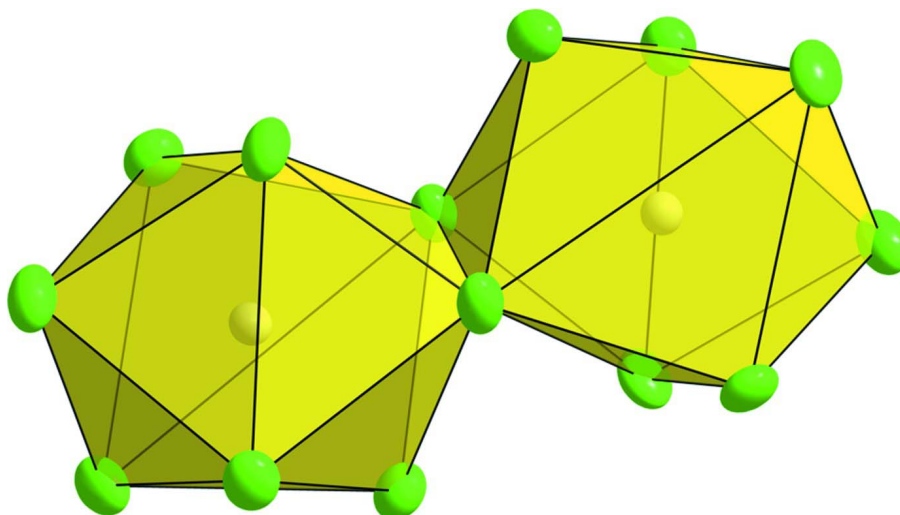


Figure 1
An edge-sharing doublet of distorted square antiprisms CeF_8 .

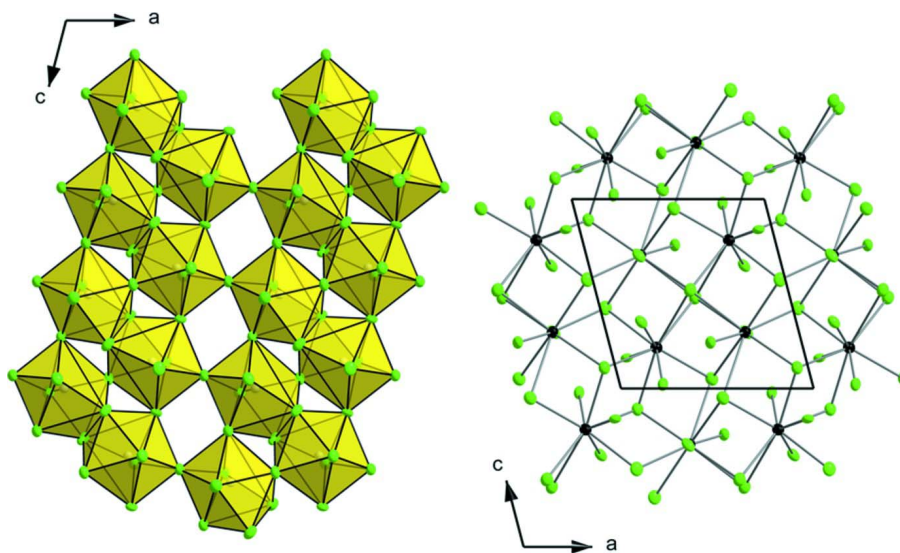


Figure 2
Layers of CeF_8 (left) and CsF_9 (right) polyhedra viewed along the b axis.

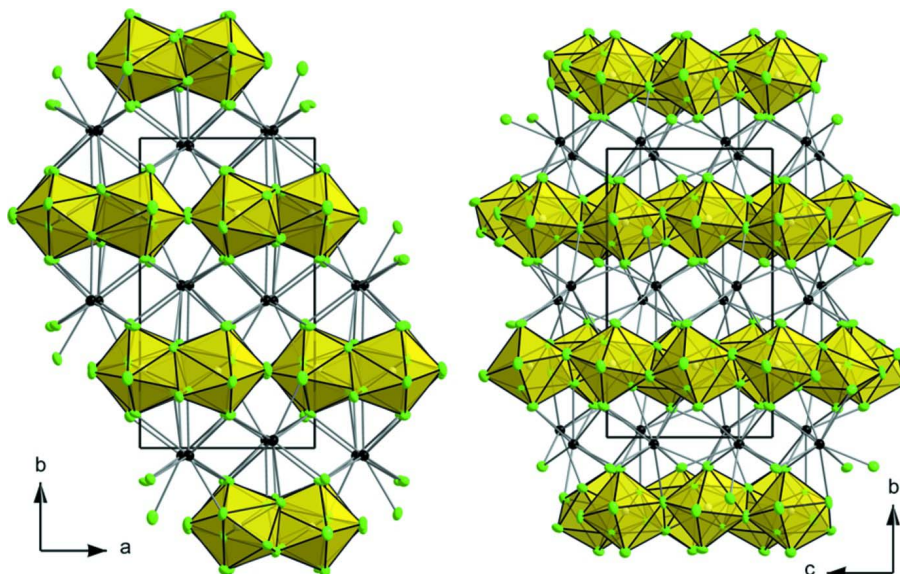


Figure 3

Crystal structure in different projections. The polyhedra around the Ce atoms are drawn.

Caesium cerium(IV) pentafluoride

Crystal data

CsCeF_5

$M_r = 368$

Monoclinic, $P2_1/c$

Hall symbol: -P 2ybc

$a = 8.3125 (5) \text{ \AA}$

$b = 14.2434 (6) \text{ \AA}$

$c = 8.4507 (5) \text{ \AA}$

$\beta = 104.566 (5)^\circ$

$V = 968.39 (9) \text{ \AA}^3$

$Z = 8$

$F(000) = 1264$

$D_x = 5.047 \text{ Mg m}^{-3}$

Mo $K\alpha$ radiation, $\lambda = 0.71069 \text{ \AA}$

Cell parameters from 10057 reflections

$\theta = 5.0\text{--}32.1^\circ$

$\mu = 16.80 \text{ mm}^{-1}$

$T = 295 \text{ K}$

Irregular shape, colourless

$0.10 \times 0.08 \times 0.05 \text{ mm}$

Data collection

STOE IPDS 2

diffractometer

Radiation source: X-ray tube

Plane graphite monochromator

Detector resolution: $6.67 \text{ pixels mm}^{-1}$

rotation method scans

Absorption correction: numerical

(*X-SHAPE*; Stoe & Cie, 2002)

$T_{\min} = 0.207$, $T_{\max} = 0.406$

55729 measured reflections

6402 independent reflections

2543 reflections with $I > 3\sigma(I)$

$R_{\text{int}} = 0.136$

$\theta_{\max} = 32.0^\circ$, $\theta_{\min} = 4.9^\circ$

$h = -12 \rightarrow 12$

$k = -21 \rightarrow 21$

$l = -12 \rightarrow 12$

Refinement

Refinement on F

$R[F^2 > 2\sigma(F^2)] = 0.037$

$wR(F^2) = 0.038$

$S = 1.04$

6402 reflections

129 parameters

0 restraints

0 constraints

Weighting scheme based on measured s.u.'s $w =$

$1/(\sigma^2(F) + 0.0001F^2)$

$(\Delta/\sigma)_{\max} = 0.010$

$\Delta\rho_{\max} = 1.85 \text{ e \AA}^{-3}$

$$\Delta\rho_{\min} = -1.89 \text{ e } \text{\AA}^{-3}$$

Extinction correction: B-C type 1 Gaussian
isotropic (Becker & Coppens, 1974)
Extinction coefficient: 320 (20)

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters (\AA^2)

	x	y	z	$U_{\text{iso}}^*/U_{\text{eq}}$
Ce1	0.55769 (5)	0.74670 (6)	0.03297 (5)	0.01796 (12)
Ce2	0.98279 (5)	0.75627 (6)	0.38963 (5)	0.01810 (12)
Cs1	0.72055 (8)	0.47560 (6)	0.29747 (8)	0.0279 (2)
Cs2	0.23935 (7)	0.52409 (6)	0.21659 (8)	0.0285 (2)
F1	1.0580 (7)	0.8988 (5)	0.3904 (9)	0.031 (2)
F2	1.0275 (8)	0.6097 (5)	0.4251 (9)	0.030 (2)
F3	0.5084 (7)	0.8919 (4)	-0.0200 (8)	0.0306 (19)
F4	0.2716 (6)	0.7548 (6)	-0.0383 (6)	0.0332 (13)
F5	0.4735 (6)	0.7877 (4)	0.2572 (7)	0.0309 (17)
F6	0.8051 (7)	0.8239 (4)	0.1490 (7)	0.0286 (17)
F7	0.7769 (7)	0.6649 (4)	-0.0219 (7)	0.0280 (16)
F8	0.4839 (7)	0.6055 (5)	0.0505 (8)	0.0311 (19)
F9	0.7275 (7)	0.6849 (4)	0.2977 (8)	0.0309 (15)
F10	1.0714 (7)	0.7753 (4)	0.6611 (6)	0.032 (2)

Atomic displacement parameters (\AA^2)

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U^{23}
Ce1	0.01799 (17)	0.0192 (2)	0.01669 (18)	-0.0006 (3)	0.00442 (13)	-0.0005 (3)
Ce2	0.01748 (17)	0.0193 (3)	0.01749 (18)	0.0000 (2)	0.00426 (13)	-0.0001 (3)
Cs1	0.0277 (2)	0.0267 (4)	0.0302 (3)	0.0012 (3)	0.0091 (2)	0.0004 (3)
Cs2	0.0279 (3)	0.0285 (4)	0.0285 (3)	-0.0021 (3)	0.0060 (2)	-0.0004 (2)
F1	0.026 (3)	0.031 (4)	0.035 (3)	-0.003 (2)	0.008 (2)	0.001 (3)
F2	0.033 (3)	0.016 (3)	0.041 (4)	0.006 (2)	0.010 (3)	0.001 (3)
F3	0.031 (3)	0.025 (3)	0.037 (3)	0.000 (2)	0.012 (3)	0.005 (3)
F4	0.0222 (16)	0.049 (3)	0.0287 (17)	0.006 (4)	0.0073 (15)	0.004 (5)
F5	0.022 (2)	0.040 (3)	0.031 (3)	0.007 (2)	0.008 (2)	0.005 (3)
F6	0.025 (2)	0.025 (3)	0.032 (3)	-0.003 (2)	-0.001 (2)	0.004 (2)
F7	0.022 (2)	0.029 (3)	0.034 (3)	0.003 (2)	0.010 (2)	0.003 (2)
F8	0.031 (3)	0.025 (3)	0.036 (3)	-0.004 (2)	0.006 (2)	0.005 (3)
F9	0.028 (2)	0.022 (2)	0.036 (3)	-0.002 (2)	-0.004 (2)	0.008 (3)
F10	0.030 (2)	0.050 (5)	0.016 (2)	0.001 (2)	0.0065 (18)	0.005 (2)

Geometric parameters (\AA , $^\circ$)

Ce1—F3	2.133 (6)	F1—F8 ⁱⁱ	3.458 (8)
Ce1—F4	2.304 (5)	F1—F10	2.865 (9)
Ce1—F5	2.256 (6)	F1—F10 ⁱ	3.166 (10)
Ce1—F5 ⁱ	2.311 (6)	F2—F2 ^v	3.445 (10)
Ce1—F6	2.320 (5)	F2—F4 ⁱⁱ	2.761 (10)
Ce1—F7	2.306 (6)	F2—F6 ⁱⁱⁱ	3.107 (10)

Ce1—F8	2.119 (7)	F2—F9	2.679 (8)
Ce1—F9	2.487 (6)	F2—F10	3.051 (9)
Ce1—F9 ⁱ	2.882 (7)	F2—F10 ⁱ	2.864 (9)
Ce2—F1	2.123 (7)	F3—F3 ^x	3.106 (9)
Ce2—F2	2.128 (7)	F3—F4	2.749 (10)
Ce2—F4 ⁱⁱ	2.329 (5)	F3—F5	2.848 (9)
Ce2—F6	2.395 (6)	F3—F5 ⁱ	3.146 (9)
Ce2—F6 ⁱⁱⁱ	3.150 (7)	F3—F6	2.700 (8)
Ce2—F7 ⁱⁱⁱ	2.322 (6)	F3—F9 ⁱ	2.881 (10)
Ce2—F9	2.304 (6)	F4—F5	2.676 (7)
Ce2—F10	2.242 (5)	F4—F5 ⁱ	2.762 (9)
Ce2—F10 ⁱ	2.279 (6)	F4—F8	2.745 (10)
Cs1—F1 ^{iv}	2.928 (8)	F4—F10 ^{xi}	2.680 (6)
Cs1—F2	3.152 (6)	F4—F10 ^{viii}	2.684 (8)
Cs1—F2 ^v	2.982 (6)	F5—F6	3.157 (9)
Cs1—F3 ^{vi}	3.222 (7)	F5—F7 ⁱⁱⁱ	2.817 (7)
Cs1—F3 ⁱⁱⁱ	3.229 (7)	F5—F8	3.142 (9)
Cs1—F5 ^{vi}	3.099 (6)	F5—F8 ⁱⁱⁱ	2.891 (9)
Cs1—F8	3.095 (6)	F5—F9	2.521 (8)
Cs1—F8 ^{vii}	3.218 (6)	F5—F10 ^{viii}	3.357 (8)
Cs1—F9	2.982 (5)	F6—F7	2.664 (8)
Cs2—F1 ^{vi}	2.998 (6)	F6—F7 ⁱⁱⁱ	2.853 (9)
Cs2—F1 ^{viii}	2.998 (7)	F6—F9	2.514 (9)
Cs2—F2 ^{ix}	3.042 (8)	F6—F9 ⁱ	2.878 (9)
Cs2—F3 ^{vi}	3.437 (6)	F6—F10 ⁱ	2.607 (8)
Cs2—F3 ⁱⁱⁱ	2.981 (6)	F7—F8	2.788 (9)
Cs2—F6 ^{vi}	3.125 (6)	F7—F9	2.847 (9)
Cs2—F7 ^{vii}	3.140 (6)	F7—F9 ⁱ	2.598 (8)
Cs2—F8	2.980 (7)	F7—F10 ⁱ	2.684 (7)
Cs2—F10 ^{viii}	3.162 (6)	F8—F8 ^{vii}	3.153 (9)
F1—F4 ⁱⁱ	2.786 (10)	F8—F9	2.760 (8)
F1—F6	2.750 (8)	F9—F10 ⁱ	3.390 (9)
F1—F7 ⁱⁱⁱ	2.776 (9)		
F3—Ce1—F4	76.4 (3)	F3 ⁱⁱⁱ —F5—F6	110.5 (2)
F3—Ce1—F5	80.9 (2)	F3 ⁱⁱⁱ —F5—F7 ⁱⁱⁱ	82.3 (2)
F3—Ce1—F5 ⁱ	90.0 (2)	F3 ⁱⁱⁱ —F5—F8	69.5 (2)
F3—Ce1—F6	74.5 (2)	F3 ⁱⁱⁱ —F5—F8 ⁱⁱⁱ	86.3 (2)
F3—Ce1—F7	124.6 (2)	F3 ⁱⁱⁱ —F5—F9	59.9 (2)
F3—Ce1—F8	153.0 (2)	F3 ⁱⁱⁱ —F5—F10 ^{viii}	82.2 (2)
F3—Ce1—F9	124.6 (2)	F4—F5—F4 ⁱⁱⁱ	102.0 (2)
F3—Ce1—F9 ⁱ	68.3 (2)	F4—F5—F6	98.4 (2)
F4—Ce1—F5	71.86 (18)	F4—F5—F7 ⁱⁱⁱ	155.1 (3)
F4—Ce1—F5 ⁱ	73.51 (19)	F4—F5—F8	55.6 (2)
F4—Ce1—F6	146.4 (3)	F4—F5—F8 ⁱⁱⁱ	140.2 (3)
F4—Ce1—F7	142.0 (2)	F4—F5—F9	109.4 (3)
F4—Ce1—F8	76.6 (3)	F4—F5—F10 ^{viii}	51.32 (17)
F4—Ce1—F9	124.6 (2)	F4 ⁱⁱⁱ —F5—F6	158.3 (2)

F4—Ce1—F9 ⁱ	117.07 (18)	F4 ⁱⁱⁱ —F5—F7 ⁱⁱⁱ	102.8 (2)
F5—Ce1—F5 ⁱ	145.35 (18)	F4 ⁱⁱⁱ —F5—F8	105.8 (3)
F5—Ce1—F6	87.2 (2)	F4 ⁱⁱⁱ —F5—F8 ⁱⁱⁱ	58.0 (2)
F5—Ce1—F7	136.69 (19)	F4 ⁱⁱⁱ —F5—F9	114.1 (3)
F5—Ce1—F8	91.8 (2)	F4 ⁱⁱⁱ —F5—F10 ^{viii}	50.83 (16)
F5—Ce1—F9	64.0 (2)	F6—F5—F7 ⁱⁱⁱ	56.7 (2)
F5—Ce1—F9 ⁱ	143.25 (19)	F6—F5—F8	80.0 (2)
F5 ⁱ —Ce1—F6	122.6 (2)	F6—F5—F8 ⁱⁱⁱ	108.8 (2)
F5 ⁱ —Ce1—F7	75.19 (19)	F6—F5—F9	51.1 (2)
F5 ⁱ —Ce1—F8	81.4 (2)	F6—F5—F10 ^{viii}	149.6 (2)
F5 ⁱ —Ce1—F9	142.4 (2)	F7 ⁱⁱⁱ —F5—F8	114.9 (2)
F5 ⁱ —Ce1—F9 ⁱ	56.81 (18)	F7 ⁱⁱⁱ —F5—F8 ⁱⁱⁱ	58.5 (2)
F6—Ce1—F7	70.3 (2)	F7 ⁱⁱⁱ —F5—F9	57.9 (2)
F6—Ce1—F8	131.4 (2)	F7 ⁱⁱⁱ —F5—F10 ^{viii}	153.6 (3)
F6—Ce1—F9	62.9 (2)	F8—F5—F8 ⁱⁱⁱ	155.8 (3)
F6—Ce1—F9 ⁱ	66.2 (2)	F8—F5—F9	57.1 (2)
F7—Ce1—F8	78.0 (2)	F8—F5—F10 ^{viii}	79.02 (19)
F7—Ce1—F9	72.8 (2)	F8 ⁱⁱⁱ —F5—F9	110.2 (3)
F7—Ce1—F9 ⁱ	58.87 (18)	F8 ⁱⁱⁱ —F5—F10 ^{viii}	99.3 (2)
F8—Ce1—F9	73.1 (2)	F9—F5—F10 ^{viii}	128.8 (3)
F8—Ce1—F9 ⁱ	124.7 (2)	Ce1—F6—Ce2 ⁱ	117.4 (3)
F9—Ce1—F9 ⁱ	118.33 (19)	Ce1—F6—Cs2 ^{xiii}	93.16 (19)
F1—Ce2—F2	153.7 (2)	Ce1—F6—F1	114.4 (2)
F1—Ce2—F4 ⁱⁱ	77.3 (3)	Ce1—F6—F2 ⁱ	158.2 (3)
F1—Ce2—F6	74.7 (2)	Ce1—F6—F3	119.1 (3)
F1—Ce2—F6 ⁱⁱⁱ	122.3 (2)	Ce1—F6—F5	49.59 (17)
F1—Ce2—F7 ⁱⁱⁱ	77.1 (2)	Ce1—F6—F7	45.54 (15)
F1—Ce2—F9	131.9 (2)	Ce1—F6—F7	54.58 (17)
F1—Ce2—F10	82.0 (3)	Ce1—F6—F7 ⁱⁱⁱ	99.0 (3)
F1—Ce2—F10 ⁱ	91.9 (3)	Ce1—F6—F9	61.76 (19)
F2—Ce2—F4 ⁱⁱ	76.4 (3)	Ce1—F6—F9 ⁱ	66.33 (18)
F2—Ce2—F6	124.2 (2)	Ce1—F6—F10 ⁱ	114.4 (3)
F2—Ce2—F6 ⁱⁱⁱ	69.0 (2)	Ce2—F6—Ce2 ⁱ	98.51 (19)
F2—Ce2—F7 ⁱⁱⁱ	123.1 (3)	Ce2—F6—Cs2 ^{xiii}	99.35 (19)
F2—Ce2—F9	74.2 (2)	Ce2—F6—F1	48.14 (18)
F2—Ce2—F10	88.5 (2)	Ce2—F6—F2 ⁱ	107.8 (2)
F2—Ce2—F10 ⁱ	81.0 (3)	Ce2—F6—F3	151.6 (3)
F4 ⁱⁱ —Ce2—F6	128.6 (2)	Ce2—F6—F5	94.9 (2)
F4 ⁱⁱ —Ce2—F6 ⁱⁱⁱ	115.26 (18)	Ce2—F6—F7	94.0 (2)
F4 ⁱⁱ —Ce2—F7 ⁱⁱⁱ	138.0 (2)	Ce2—F6—F7 ⁱⁱⁱ	51.62 (16)
F4 ⁱⁱ —Ce2—F9	149.3 (3)	Ce2—F6—F9	55.94 (18)
F4 ⁱⁱ —Ce2—F10	71.9 (2)	Ce2—F6—F9 ⁱ	142.1 (3)
F4 ⁱⁱ —Ce2—F10 ⁱ	71.13 (18)	Ce2—F6—F10 ⁱ	54.00 (16)
F6—Ce2—F6 ⁱⁱⁱ	116.07 (18)	Ce2 ⁱ —F6—Cs2 ^{xiii}	134.6 (2)
F6—Ce2—F7 ⁱⁱⁱ	74.4 (2)	Ce2 ⁱ —F6—F1	104.6 (2)
F6—Ce2—F9	64.7 (2)	Ce2 ⁱ —F6—F2 ⁱ	39.77 (15)
F6—Ce2—F10	142.5 (2)	Ce2 ⁱ —F6—F3	106.7 (2)
F6—Ce2—F10 ⁱ	67.8 (2)	Ce2 ⁱ —F6—F5	137.6 (2)

F6 ⁱⁱⁱ —Ce2—F7 ⁱⁱⁱ	55.83 (18)	Ce2 ⁱ —F6—F7	46.15 (17)
F6 ⁱⁱⁱ —Ce2—F9	61.40 (19)	Ce2 ⁱ —F6—F7 ⁱⁱⁱ	150.0 (2)
F6 ⁱⁱⁱ —Ce2—F10	54.76 (18)	Ce2 ⁱ —F6—F9	106.7 (2)
F6 ⁱⁱⁱ —Ce2—F10 ⁱ	145.75 (19)	Ce2 ⁱ —F6—F9 ⁱ	44.67 (15)
F7 ⁱⁱⁱ —Ce2—F9	68.3 (2)	Ce2 ⁱ —F6—F10 ⁱ	44.62 (15)
F7 ⁱⁱⁱ —Ce2—F10	72.0 (2)	Cs2 ^{xiii} —F6—F1	60.97 (19)
F7 ⁱⁱⁱ —Ce2—F10 ⁱ	142.19 (19)	Cs2 ^{xiii} —F6—F2 ⁱ	94.9 (2)
F9—Ce2—F10	115.9 (2)	Cs2 ^{xiii} —F6—F3	71.90 (19)
F9—Ce2—F10 ⁱ	95.4 (2)	Cs2 ^{xiii} —F6—F5	81.50 (19)
F10—Ce2—F10 ⁱ	142.9 (2)	Cs2 ^{xiii} —F6—F7	166.0 (2)
F1 ^{iv} —Cs1—F2	81.20 (19)	Cs2 ^{xiii} —F6—F7 ⁱⁱⁱ	63.18 (17)
F1 ^{iv} —Cs1—F2 ^v	82.0 (2)	Cs2 ^{xiii} —F6—F9	117.9 (3)
F1 ^{iv} —Cs1—F3 ^{vi}	136.22 (19)	Cs2 ^{xiii} —F6—F9 ⁱ	113.5 (2)
F1 ^{iv} —Cs1—F3 ⁱⁱⁱ	166.16 (19)	Cs2 ^{xiii} —F6—F10 ⁱ	131.1 (2)
F1 ^{iv} —Cs1—F5 ^{vi}	88.34 (18)	F1—F6—F2 ⁱ	82.7 (2)
F1 ^{iv} —Cs1—F8	103.73 (19)	F1—F6—F3	132.8 (3)
F1 ^{iv} —Cs1—F8 ^{vii}	68.29 (17)	F1—F6—F5	114.1 (3)
F1 ^{iv} —Cs1—F9	111.1 (2)	F1—F6—F7	132.7 (3)
F2—Cs1—F2 ^v	68.27 (17)	F1—F6—F7 ⁱⁱⁱ	59.4 (2)
F2—Cs1—F3 ^{vi}	124.79 (18)	F1—F6—F9	100.3 (3)
F2—Cs1—F3 ⁱⁱⁱ	88.55 (17)	F1—F6—F9 ⁱ	135.5 (3)
F2—Cs1—F5 ^{vi}	156.99 (15)	F1—F6—F10 ⁱ	72.4 (2)
F2—Cs1—F8	101.01 (16)	F2 ⁱ —F6—F3	100.0 (3)
F2—Cs1—F8 ^{vii}	136.56 (19)	F2 ⁱ —F6—F5	157.3 (2)
F2—Cs1—F9	51.69 (16)	F2 ⁱ —F6—F7	85.0 (3)
F2 ^v —Cs1—F3 ^{vi}	77.96 (18)	F2 ⁱ —F6—F7 ⁱⁱⁱ	141.6 (3)
F2 ^v —Cs1—F3 ⁱⁱⁱ	102.87 (18)	F2 ⁱ —F6—F9	144.2 (3)
F2 ^v —Cs1—F5 ^{vi}	90.09 (16)	F2 ⁱ —F6—F9 ⁱ	53.0 (2)
F2 ^v —Cs1—F8	167.23 (17)	F2 ⁱ —F6—F10 ⁱ	63.8 (2)
F2 ^v —Cs1—F8 ^{vii}	132.64 (17)	F3—F6—F5	57.6 (2)
F2 ^v —Cs1—F9	113.41 (16)	F3—F6—F7	94.2 (2)
F3 ^{vi} —Cs1—F3 ⁱⁱⁱ	57.57 (16)	F3—F6—F7 ⁱⁱⁱ	102.0 (3)
F3 ^{vi} —Cs1—F5 ^{vi}	53.52 (16)	F3—F6—F9	103.4 (3)
F3 ^{vi} —Cs1—F8	104.26 (16)	F3—F6—F9 ⁱ	62.1 (2)
F3 ^{vi} —Cs1—F8 ^{vii}	98.44 (16)	F3—F6—F10 ⁱ	150.3 (3)
F3 ^{vi} —Cs1—F9	112.58 (18)	F5—F6—F7	93.1 (2)
F3 ⁱⁱⁱ —Cs1—F5 ^{vi}	104.46 (16)	F5—F6—F7 ⁱⁱⁱ	55.62 (19)
F3 ⁱⁱⁱ —Cs1—F8	69.01 (17)	F5—F6—F9	51.3 (2)
F3 ⁱⁱⁱ —Cs1—F8 ^{vii}	114.83 (15)	F5—F6—F9 ⁱ	107.8 (2)
F3 ⁱⁱⁱ —Cs1—F9	55.10 (18)	F5—F6—F10 ⁱ	134.0 (3)
F5 ^{vi} —Cs1—F8	101.36 (15)	F7—F6—F7 ⁱⁱⁱ	123.9 (3)
F5 ^{vi} —Cs1—F8 ^{vii}	54.44 (16)	F7—F6—F9	66.6 (2)
F5 ^{vi} —Cs1—F9	150.79 (15)	F7—F6—F9 ⁱ	55.8 (2)
F8—Cs1—F8 ^{vii}	59.89 (16)	F7—F6—F10 ⁱ	61.2 (2)
F8—Cs1—F9	53.97 (16)	F7 ⁱⁱⁱ —F6—F9	57.5 (2)
F8 ^{vii} —Cs1—F9	111.41 (16)	F7 ⁱⁱⁱ —F6—F9 ⁱ	162.9 (3)
F1 ^{vi} —Cs2—F1 ^{viii}	75.84 (19)	F7 ⁱⁱⁱ —F6—F10 ⁱ	105.6 (2)
F1 ^{vi} —Cs2—F2 ^{ix}	81.94 (19)	F9—F6—F9 ⁱ	117.5 (3)

F1 ^{vi} —Cs2—F3 ^{vi}	101.58 (17)	F9—F6—F10 ⁱ	82.9 (3)
F1 ^{vi} —Cs2—F3 ⁱⁱⁱ	150.6 (2)	F9 ⁱ —F6—F10 ⁱ	89.1 (3)
F1 ^{vi} —Cs2—F6 ^{vi}	53.32 (16)	Ce1—F7—Ce2 ⁱ	120.3 (2)
F1 ^{vi} —Cs2—F7 ^{vii}	53.71 (18)	Ce1—F7—Cs2 ^{vii}	127.3 (2)
F1 ^{vi} —Cs2—F8	134.27 (19)	Ce1—F7—F1 ⁱ	168.5 (3)
F1 ^{vi} —Cs2—F10 ^{viii}	101.15 (17)	Ce1—F7—F5 ⁱ	52.49 (17)
F1 ^{viii} —Cs2—F2 ^{ix}	98.94 (19)	Ce1—F7—F6	55.10 (18)
F1 ^{viii} —Cs2—F3 ^{vi}	163.34 (19)	Ce1—F7—F6 ⁱ	115.5 (2)
F1 ^{viii} —Cs2—F3 ⁱⁱⁱ	130.44 (18)	Ce1—F7—F8	48.02 (18)
F1 ^{viii} —Cs2—F6 ^{vi}	126.19 (17)	Ce1—F7—F9	56.55 (18)
F1 ^{viii} —Cs2—F7 ^{vii}	83.52 (17)	Ce1—F7—F9 ⁱ	71.7 (2)
F1 ^{viii} —Cs2—F8	70.68 (17)	Ce1—F7—F10 ⁱ	112.1 (3)
F1 ^{viii} —Cs2—F10 ^{viii}	55.35 (17)	Ce2 ⁱ —F7—Cs2 ^{vii}	100.6 (2)
F2 ^{ix} —Cs2—F3 ^{vi}	96.96 (17)	Ce2 ⁱ —F7—F1 ⁱ	48.22 (19)
F2 ^{ix} —Cs2—F3 ⁱⁱⁱ	80.87 (18)	Ce2 ⁱ —F7—F5 ⁱ	106.3 (2)
F2 ^{ix} —Cs2—F6 ^{vi}	90.96 (18)	Ce2 ⁱ —F7—F6	78.0 (2)
F2 ^{ix} —Cs2—F7 ^{vii}	133.81 (17)	Ce2 ⁱ —F7—F6 ⁱ	53.95 (18)
F2 ^{ix} —Cs2—F8	132.82 (18)	Ce2 ⁱ —F7—F8	166.6 (3)
F2 ^{ix} —Cs2—F10 ^{viii}	54.94 (17)	Ce2 ⁱ —F7—F9	123.4 (2)
F3 ^{vi} —Cs2—F3 ⁱⁱⁱ	57.36 (16)	Ce2 ⁱ —F7—F9 ⁱ	55.52 (19)
F3 ^{vi} —Cs2—F6 ^{vi}	48.29 (14)	Ce2 ⁱ —F7—F10 ⁱ	52.62 (17)
F3 ^{vi} —Cs2—F7 ^{vii}	81.88 (15)	Cs2 ^{vii} —F7—F1 ⁱ	60.53 (18)
F3 ^{vi} —Cs2—F8	101.76 (16)	Cs2 ^{vii} —F7—F5 ⁱ	86.83 (19)
F3 ^{vi} —Cs2—F10 ^{viii}	140.30 (14)	Cs2 ^{vii} —F7—F6	177.4 (2)
F3 ⁱⁱⁱ —Cs2—F6 ^{vi}	103.30 (16)	Cs2 ^{vii} —F7—F6 ⁱ	62.65 (17)
F3 ⁱⁱⁱ —Cs2—F7 ^{vii}	131.37 (16)	Cs2 ^{vii} —F7—F8	86.0 (2)
F3 ⁱⁱⁱ —Cs2—F8	73.91 (18)	Cs2 ^{vii} —F7—F9	125.8 (2)
F3 ⁱⁱⁱ —Cs2—F10 ^{viii}	88.18 (15)	Cs2 ^{vii} —F7—F9 ⁱ	114.8 (2)
F6 ^{vi} —Cs2—F7 ^{vii}	54.18 (16)	Cs2 ^{vii} —F7—F10 ⁱ	119.1 (2)
F6 ^{vi} —Cs2—F8	133.07 (17)	F1 ⁱ —F7—F5 ⁱ	125.1 (3)
F6 ^{vi} —Cs2—F10 ^{viii}	142.19 (16)	F1 ⁱ —F7—F6	117.2 (3)
F7 ^{vii} —Cs2—F8	91.80 (17)	F1 ⁱ —F7—F6 ⁱ	58.5 (2)
F7 ^{vii} —Cs2—F10 ^{viii}	137.52 (13)	F1 ⁱ —F7—F8	143.1 (3)
F8—Cs2—F10 ^{viii}	84.64 (17)	F1 ⁱ —F7—F9	128.2 (3)
Ce2—F1—Cs1 ^{xii}	125.5 (3)	F1 ⁱ —F7—F9 ⁱ	97.6 (3)
Ce2—F1—Cs2 ^{xiii}	110.4 (2)	F1 ⁱ —F7—F10 ⁱ	63.3 (2)
Ce2—F1—Cs2 ⁱⁱ	115.6 (3)	F5 ⁱ —F7—F6	95.6 (2)
Ce2—F1—F4 ⁱⁱ	54.7 (2)	F5 ⁱ —F7—F6 ⁱ	67.7 (2)
Ce2—F1—F6	57.14 (19)	F5 ⁱ —F7—F8	62.1 (2)
Ce2—F1—F7 ⁱⁱⁱ	54.6 (2)	F5 ⁱ —F7—F9	106.6 (3)
Ce2—F1—F8 ⁱⁱ	104.8 (3)	F5 ⁱ —F7—F9 ⁱ	55.3 (2)
Ce2—F1—F10	50.81 (19)	F5 ⁱ —F7—F10 ⁱ	147.2 (3)
Ce2—F1—F10 ⁱ	45.99 (18)	F6—F7—F6 ⁱ	117.6 (3)
Cs1 ^{xii} —F1—Cs2 ^{xiii}	101.4 (2)	F6—F7—F8	95.8 (3)
Cs1 ^{xii} —F1—Cs2 ⁱⁱ	97.03 (18)	F6—F7—F9	54.2 (2)
Cs1 ^{xii} —F1—F4 ⁱⁱ	87.6 (2)	F6—F7—F9 ⁱ	66.3 (2)
Cs1 ^{xii} —F1—F6	102.2 (3)	F6—F7—F10 ⁱ	58.4 (2)
Cs1 ^{xii} —F1—F7 ⁱⁱⁱ	162.4 (3)	F6 ⁱ —F7—F8	121.4 (2)

Cs1 ^{xii} —F1—F8 ⁱⁱ	59.84 (16)	F6 ⁱ —F7—F9	170.4 (3)
Cs1 ^{xii} —F1—F10	139.3 (3)	F6 ⁱ —F7—F9 ⁱ	54.7 (2)
Cs1 ^{xii} —F1—F10 ⁱ	80.6 (2)	F6 ⁱ —F7—F10 ⁱ	104.9 (3)
Cs2 ^{xiii} —F1—Cs2 ⁱⁱ	104.2 (2)	F8—F7—F9	58.6 (2)
Cs2 ^{xiii} —F1—F4 ⁱⁱ	164.8 (3)	F8—F7—F9 ⁱ	111.2 (3)
Cs2 ^{xiii} —F1—F6	65.71 (18)	F8—F7—F10 ⁱ	133.7 (3)
Cs2 ^{xiii} —F1—F7 ⁱⁱⁱ	65.76 (18)	F9—F7—F9 ⁱ	115.8 (3)
Cs2 ^{xiii} —F1—F8 ⁱⁱ	144.5 (3)	F9—F7—F10 ⁱ	75.5 (2)
Cs2 ^{xiii} —F1—F10	118.0 (3)	F9 ⁱ —F7—F10 ⁱ	93.7 (2)
Cs2 ^{xiii} —F1—F10 ⁱ	115.8 (2)	Ce1—F8—Cs1	117.9 (2)
Cs2 ⁱⁱ —F1—F4 ⁱⁱ	86.7 (2)	Ce1—F8—Cs1 ^{vii}	111.9 (2)
Cs2 ⁱⁱ —F1—F6	159.7 (3)	Ce1—F8—Cs2	130.2 (3)
Cs2 ⁱⁱ —F1—F7 ⁱⁱⁱ	97.8 (3)	Ce1—F8—F1 ^{viii}	106.0 (2)
Cs2 ⁱⁱ —F1—F8 ⁱⁱ	54.42 (15)	Ce1—F8—F4	54.7 (2)
Cs2 ⁱⁱ —F1—F10	65.24 (19)	Ce1—F8—F5	45.86 (17)
Cs2 ⁱⁱ —F1—F10 ⁱ	139.7 (2)	Ce1—F8—F5 ⁱ	52.21 (18)
F4 ⁱⁱ —F1—F6	100.5 (3)	Ce1—F8—F7	54.00 (19)
F4 ⁱⁱ —F1—F7 ⁱⁱⁱ	102.7 (3)	Ce1—F8—F8 ^{vii}	147.1 (3)
F4 ⁱⁱ —F1—F8 ⁱⁱ	50.8 (2)	Ce1—F8—F9	59.58 (19)
F4 ⁱⁱ —F1—F10	56.7 (2)	Cs1—F8—Cs1 ^{vii}	120.1 (2)
F4 ⁱⁱ —F1—F10 ⁱ	53.06 (19)	Cs1—F8—Cs2	80.98 (17)
F6—F1—F7 ⁱⁱⁱ	62.2 (2)	Cs1—F8—F1 ^{viii}	131.9 (2)
F6—F1—F8 ⁱⁱ	143.1 (3)	Cs1—F8—F4	154.6 (3)
F6—F1—F10	102.9 (3)	Cs1—F8—F5	102.8 (2)
F6—F1—F10 ⁱ	51.7 (2)	Cs1—F8—F5 ⁱ	140.3 (3)
F7 ⁱⁱⁱ —F1—F8 ⁱⁱ	137.5 (3)	Cs1—F8—F7	83.54 (19)
F7 ⁱⁱⁱ —F1—F10	56.8 (2)	Cs1—F8—F8 ^{vii}	61.99 (16)
F7 ⁱⁱⁱ —F1—F10 ⁱ	94.0 (3)	Cs1—F8—F9	60.92 (16)
F8 ⁱⁱ —F1—F10	81.2 (2)	Cs1 ^{vii} —F8—Cs2	91.41 (16)
F8 ⁱⁱ —F1—F10 ⁱ	92.0 (2)	Cs1 ^{vii} —F8—F1 ^{viii}	51.88 (15)
F10—F1—F10 ⁱ	90.4 (3)	Cs1 ^{vii} —F8—F4	82.68 (19)
Ce2—F2—Cs1	116.7 (2)	Cs1 ^{vii} —F8—F5	136.2 (2)
Ce2—F2—Cs1 ^v	125.0 (3)	Cs1 ^{vii} —F8—F5 ⁱ	60.67 (16)
Ce2—F2—Cs2 ^{xiv}	114.7 (3)	Cs1 ^{vii} —F8—F7	101.4 (2)
Ce2—F2—F2 ^v	155.1 (3)	Cs1 ^{vii} —F8—F8 ^{vii}	58.11 (15)
Ce2—F2—F4 ⁱⁱ	55.1 (2)	Cs1 ^{vii} —F8—F9	163.2 (3)
Ce2—F2—F6 ⁱⁱⁱ	71.2 (2)	Cs2—F8—F1 ^{viii}	54.90 (16)
Ce2—F2—F9	55.89 (18)	Cs2—F8—F4	87.8 (2)
Ce2—F2—F10	47.28 (17)	Cs2—F8—F5	86.7 (2)
Ce2—F2—F10 ⁱ	51.8 (2)	Cs2—F8—F5 ⁱ	137.0 (2)
Cs1—F2—Cs1 ^v	111.7 (2)	Cs2—F8—F7	163.5 (3)
Cs1—F2—Cs2 ^{xiv}	95.48 (19)	Cs2—F8—F8 ^{vii}	82.6 (2)
Cs1—F2—F2 ^v	53.51 (14)	Cs2—F8—F9	105.1 (3)
Cs1—F2—F4 ⁱⁱ	166.1 (3)	F1 ^{viii} —F8—F4	51.8 (2)
Cs1—F2—F6 ⁱⁱⁱ	80.7 (2)	F1 ^{viii} —F8—F5	93.6 (2)
Cs1—F2—F9	60.88 (17)	F1 ^{viii} —F8—F5 ⁱ	82.3 (2)
Cs1—F2—F10	130.2 (3)	F1 ^{viii} —F8—F7	141.6 (3)
Cs1—F2—F10 ⁱ	109.3 (2)	F1 ^{viii} —F8—F8 ^{vii}	91.5 (2)

Cs1 ^v —F2—Cs2 ^{xiv}	84.12 (17)	F1 ^{viii} —F8—F9	141.9 (3)
Cs1 ^v —F2—F2 ^v	58.21 (15)	F4—F8—F5	53.57 (19)
Cs1 ^v —F2—F4 ⁱⁱ	81.1 (2)	F4—F8—F5 ⁱ	58.6 (2)
Cs1 ^v —F2—F6 ⁱⁱⁱ	93.0 (2)	F4—F8—F7	104.0 (3)
Cs1 ^v —F2—F9	151.4 (3)	F4—F8—F8 ^{vii}	139.2 (3)
Cs1 ^v —F2—F10	81.74 (19)	F4—F8—F9	100.8 (3)
Cs1 ^v —F2—F10 ⁱ	130.1 (3)	F5—F8—F5 ⁱ	92.5 (2)
Cs2 ^{xiv} —F2—F2 ^v	89.9 (2)	F5—F8—F7	91.1 (2)
Cs2 ^{xiv} —F2—F4 ⁱⁱ	80.1 (2)	F5—F8—F8 ^{vii}	162.5 (3)
Cs2 ^{xiv} —F2—F6 ⁱⁱⁱ	174.1 (3)	F5—F8—F9	50.06 (18)
Cs2 ^{xiv} —F2—F9	122.9 (3)	F5 ⁱ —F8—F7	59.4 (2)
Cs2 ^{xiv} —F2—F10	134.2 (3)	F5 ⁱ —F8—F8 ^{vii}	104.8 (3)
Cs2 ^{xiv} —F2—F10 ⁱ	64.7 (2)	F5 ⁱ —F8—F9	106.9 (3)
F2 ^v —F2—F4 ⁱⁱ	139.0 (3)	F7—F8—F8 ^{vii}	95.3 (3)
F2 ^v —F2—F6 ⁱⁱⁱ	84.2 (2)	F7—F8—F9	61.7 (2)
F2 ^v —F2—F9	108.3 (3)	F8 ^{vii} —F8—F9	120.0 (2)
F2 ^v —F2—F10	117.8 (3)	Ce1—F9—Ce1 ⁱⁱⁱ	103.6 (2)
F2 ^v —F2—F10 ⁱ	149.3 (3)	Ce1—F9—Ce2	114.4 (3)
F4 ⁱⁱ —F2—F6 ⁱⁱⁱ	104.6 (3)	Ce1—F9—Cs1	110.27 (19)
F4 ⁱⁱ —F2—F9	110.4 (3)	Ce1—F9—F2	139.8 (3)
F4 ⁱⁱ —F2—F10	54.7 (2)	Ce1—F9—F3 ⁱⁱⁱ	108.9 (2)
F4 ⁱⁱ —F2—F10 ⁱ	56.9 (2)	Ce1—F9—F5	53.54 (18)
F6 ⁱⁱⁱ —F2—F9	59.1 (2)	Ce1—F9—F6	55.29 (17)
F6 ⁱⁱⁱ —F2—F10	50.09 (19)	Ce1—F9—F6 ⁱⁱⁱ	150.8 (3)
F6 ⁱⁱⁱ —F2—F10 ⁱ	120.8 (3)	Ce1—F9—F7	50.68 (16)
F9—F2—F10	84.2 (2)	Ce1—F9—F7 ⁱⁱⁱ	101.9 (2)
F9—F2—F10 ⁱ	75.3 (2)	Ce1—F9—F8	47.29 (17)
F10—F2—F10 ⁱ	92.8 (2)	Ce1—F9—F10 ⁱ	88.3 (2)
Ce1—F3—Cs1 ^{xiii}	110.3 (3)	Ce1 ⁱⁱⁱ —F9—Ce2	100.8 (2)
Ce1—F3—Cs1 ⁱ	124.6 (3)	Ce1 ⁱⁱⁱ —F9—Cs1	109.0 (2)
Ce1—F3—Cs2 ^{xiii}	109.0 (2)	Ce1 ⁱⁱⁱ —F9—F2	115.2 (3)
Ce1—F3—Cs2 ⁱ	127.9 (2)	Ce1 ⁱⁱⁱ —F9—F3 ⁱⁱⁱ	43.46 (17)
Ce1—F3—F3 ^x	161.8 (3)	Ce1 ⁱⁱⁱ —F9—F5	50.11 (18)
Ce1—F3—F4	54.6 (2)	Ce1 ⁱⁱⁱ —F9—F6	108.1 (2)
Ce1—F3—F5	51.44 (19)	Ce1 ⁱⁱⁱ —F9—F6 ⁱⁱⁱ	47.52 (16)
Ce1—F3—F5 ⁱ	47.28 (16)	Ce1 ⁱⁱⁱ —F9—F7	154.3 (2)
Ce1—F3—F6	55.92 (18)	Ce1 ⁱⁱⁱ —F9—F7 ⁱⁱⁱ	49.44 (18)
Ce1—F3—F9 ⁱ	68.3 (2)	Ce1 ⁱⁱⁱ —F9—F8	105.5 (2)
Cs1 ^{xiii} —F3—Cs1 ⁱ	122.4 (2)	Ce1 ⁱⁱⁱ —F9—F10 ⁱ	141.3 (2)
Cs1 ^{xiii} —F3—Cs2 ^{xiii}	72.60 (14)	Ce2—F9—Cs1	117.2 (2)
Cs1 ^{xiii} —F3—Cs2 ⁱ	81.08 (15)	Ce2—F9—F2	49.88 (18)
Cs1 ^{xiii} —F3—F3 ^x	61.33 (18)	Ce2—F9—F3 ⁱⁱⁱ	129.8 (3)
Cs1 ^{xiii} —F3—F4	77.1 (2)	Ce2—F9—F5	117.3 (3)
Cs1 ^{xiii} —F3—F5	61.03 (19)	Ce2—F9—F6	59.41 (18)
Cs1 ^{xiii} —F3—F5 ⁱ	132.2 (2)	Ce2—F9—F6 ⁱⁱⁱ	73.93 (19)
Cs1 ^{xiii} —F3—F6	114.8 (3)	Ce2—F9—F7	91.3 (2)
Cs1 ^{xiii} —F3—F9 ⁱ	176.8 (2)	Ce2—F9—F7 ⁱⁱⁱ	56.16 (18)
Cs1 ⁱ —F3—Cs2 ^{xiii}	74.44 (13)	Ce2—F9—F8	150.9 (3)

Cs1 ⁱ —F3—Cs2 ⁱ	78.80 (16)	Ce2—F9—F10 ⁱ	42.01 (14)
Cs1 ⁱ —F3—F3 ^x	61.10 (18)	Cs1—F9—F2	67.43 (18)
Cs1 ⁱ —F3—F4	149.1 (3)	Cs1—F9—F3 ⁱⁱⁱ	66.80 (18)
Cs1 ⁱ —F3—F5	151.4 (2)	Cs1—F9—F5	124.4 (3)
Cs1 ⁱ —F3—F5 ⁱ	99.7 (2)	Cs1—F9—F6	142.6 (3)
Cs1 ⁱ —F3—F6	85.8 (2)	Cs1—F9—F6 ⁱⁱⁱ	87.5 (2)
Cs1 ⁱ —F3—F9 ⁱ	58.10 (17)	Cs1—F9—F7	84.64 (19)
Cs2 ^{xiii} —F3—Cs2 ⁱ	122.6 (2)	Cs1—F9—F7 ⁱⁱⁱ	145.4 (3)
Cs2 ^{xiii} —F3—F3 ^x	53.91 (14)	Cs1—F9—F8	65.10 (17)
Cs2 ^{xiii} —F3—F4	136.5 (3)	Cs1—F9—F10 ⁱ	100.6 (2)
Cs2 ^{xiii} —F3—F5	80.86 (19)	F2—F9—F3 ⁱⁱⁱ	106.4 (3)
Cs2 ^{xiii} —F3—F5 ⁱ	147.0 (2)	F2—F9—F5	161.8 (3)
Cs2 ^{xiii} —F3—F6	59.80 (17)	F2—F9—F6	100.7 (3)
Cs2 ^{xiii} —F3—F9 ⁱ	104.9 (2)	F2—F9—F6 ⁱⁱⁱ	67.9 (2)
Cs2 ⁱ —F3—F3 ^x	68.73 (17)	F2—F9—F7	90.0 (3)
Cs2 ⁱ —F3—F4	81.45 (19)	F2—F9—F7 ⁱⁱⁱ	95.7 (3)
Cs2 ⁱ —F3—F5	127.7 (2)	F2—F9—F8	124.9 (3)
Cs2 ⁱ —F3—F5 ⁱ	86.59 (18)	F2—F9—F10 ⁱ	54.8 (2)
Cs2 ⁱ —F3—F6	162.4 (3)	F3 ⁱⁱⁱ —F9—F5	70.9 (2)
Cs2 ⁱ —F3—F9 ⁱ	102.1 (2)	F3 ⁱⁱⁱ —F9—F6	147.4 (3)
F3 ^x —F3—F4	131.3 (3)	F3 ⁱⁱⁱ —F9—F6 ⁱⁱⁱ	55.9 (2)
F3 ^x —F3—F5	114.2 (3)	F3 ⁱⁱⁱ —F9—F7	137.0 (3)
F3 ^x —F3—F5 ⁱ	150.6 (3)	F3 ⁱⁱⁱ —F9—F7 ⁱⁱⁱ	91.5 (3)
F3 ^x —F3—F6	111.0 (2)	F3 ⁱⁱⁱ —F9—F8	78.9 (2)
F3 ^x —F3—F9 ⁱ	119.1 (3)	F3 ⁱⁱⁱ —F9—F10 ⁱ	161.2 (2)
F4—F3—F5	57.1 (2)	F5—F9—F6	77.7 (2)
F4—F3—F5 ⁱ	55.4 (2)	F5—F9—F6 ⁱⁱⁱ	97.4 (3)
F4—F3—F6	108.7 (3)	F5—F9—F7	104.2 (3)
F4—F3—F9 ⁱ	103.9 (3)	F5—F9—F7 ⁱⁱⁱ	66.7 (2)
F5—F3—F5 ⁱ	93.2 (2)	F5—F9—F8	72.9 (2)
F5—F3—F6	69.3 (2)	F5—F9—F10 ⁱ	127.3 (3)
F5—F3—F9 ⁱ	116.8 (3)	F6—F9—F6 ⁱⁱⁱ	122.1 (3)
F5 ⁱ —F3—F6	87.7 (2)	F6—F9—F7	59.2 (2)
F5 ⁱ —F3—F9 ⁱ	49.21 (18)	F6—F9—F7 ⁱⁱⁱ	67.8 (2)
F6—F3—F9 ⁱ	62.0 (2)	F6—F9—F8	100.1 (3)
Ce1—F4—Ce2 ^{viii}	173.3 (4)	F6—F9—F10 ⁱ	49.8 (2)
Ce1—F4—F1 ^{viii}	125.2 (4)	F6 ⁱⁱⁱ —F9—F7	157.8 (3)
Ce1—F4—F2 ^{viii}	138.2 (4)	F6 ⁱⁱⁱ —F9—F7 ⁱⁱⁱ	58.0 (2)
Ce1—F4—F3	48.98 (18)	F6 ⁱⁱⁱ —F9—F8	134.0 (3)
Ce1—F4—F5	53.23 (16)	F6 ⁱⁱⁱ —F9—F10 ⁱ	111.7 (2)
Ce1—F4—F5 ⁱ	53.36 (16)	F7—F9—F7 ⁱⁱⁱ	126.9 (3)
Ce1—F4—F8	48.67 (18)	F7—F9—F8	59.6 (2)
Ce1—F4—F10 ^{xi}	127.4 (3)	F7—F9—F10 ⁱ	50.06 (18)
Ce1—F4—F10 ^{viii}	126.2 (2)	F7 ⁱⁱⁱ —F9—F8	139.4 (3)
Ce2 ^{viii} —F4—F1 ^{viii}	48.04 (19)	F7 ⁱⁱⁱ —F9—F10 ⁱ	92.3 (2)
Ce2 ^{viii} —F4—F2 ^{viii}	48.52 (18)	F8—F9—F10 ⁱ	109.4 (3)
Ce2 ^{viii} —F4—F3	137.6 (4)	Ce2—F10—Ce2 ⁱⁱⁱ	138.6 (3)
Ce2 ^{viii} —F4—F5	128.2 (3)	Ce2—F10—Cs2 ⁱⁱ	106.3 (2)

Ce2 ^{viii} —F4—F5 ⁱ	124.8 (2)	Ce2—F10—F1	47.22 (17)
Ce2 ^{viii} —F4—F8	124.7 (4)	Ce2—F10—F1 ⁱⁱⁱ	118.6 (3)
Ce2 ^{viii} —F4—F10 ^{xi}	53.56 (16)	Ce2—F10—F2	44.21 (16)
Ce2 ^{viii} —F4—F10 ^{viii}	52.57 (15)	Ce2—F10—F2 ⁱⁱⁱ	142.4 (3)
F1 ^{viii} —F4—F2 ^{viii}	96.5 (2)	Ce2—F10—F4 ^{xv}	157.3 (3)
F1 ^{viii} —F4—F3	168.0 (3)	Ce2—F10—F4 ⁱⁱ	55.57 (16)
F1 ^{viii} —F4—F5	123.7 (3)	Ce2—F10—F5 ⁱⁱ	105.4 (2)
F1 ^{viii} —F4—F5 ⁱ	98.5 (3)	Ce2—F10—F6 ⁱⁱⁱ	80.6 (2)
F1 ^{viii} —F4—F8	77.4 (3)	Ce2—F10—F7 ⁱⁱⁱ	55.37 (17)
F1 ^{viii} —F4—F10 ^{xi}	70.8 (2)	Ce2—F10—F9 ⁱⁱⁱ	106.3 (2)
F1 ^{viii} —F4—F10 ^{viii}	63.1 (3)	Ce2 ⁱⁱⁱ —F10—Cs2 ⁱⁱ	106.1 (2)
F2 ^{viii} —F4—F3	90.3 (3)	Ce2 ⁱⁱⁱ —F10—F1	147.4 (3)
F2 ^{viii} —F4—F5	104.6 (3)	Ce2 ⁱⁱⁱ —F10—F1 ⁱⁱⁱ	42.08 (17)
F2 ^{viii} —F4—F5 ⁱ	128.9 (3)	Ce2 ⁱⁱⁱ —F10—F2	113.0 (3)
F2 ^{viii} —F4—F8	167.5 (3)	Ce2 ⁱⁱⁱ —F10—F2 ⁱⁱⁱ	47.22 (18)
F2 ^{viii} —F4—F10 ^{xi}	63.5 (2)	Ce2 ⁱⁱⁱ —F10—F4 ^{xv}	55.32 (16)
F2 ^{viii} —F4—F10 ^{viii}	68.1 (2)	Ce2 ⁱⁱⁱ —F10—F4 ⁱⁱ	152.2 (3)
F3—F4—F5	63.3 (2)	Ce2 ⁱⁱⁱ —F10—F5 ⁱⁱ	104.9 (2)
F3—F4—F5 ⁱ	69.6 (2)	Ce2 ⁱⁱⁱ —F10—F6 ⁱⁱⁱ	58.2 (2)
F3—F4—F8	97.6 (2)	Ce2 ⁱⁱⁱ —F10—F7 ⁱⁱⁱ	96.2 (2)
F3—F4—F10 ^{xi}	103.9 (3)	Ce2 ⁱⁱⁱ —F10—F9 ⁱⁱⁱ	42.60 (14)
F3—F4—F10 ^{viii}	128.8 (3)	Cs2 ⁱⁱ —F10—F1	59.42 (18)
F5—F4—F5 ⁱ	106.6 (2)	Cs2 ⁱⁱ —F10—F1 ⁱⁱⁱ	134.3 (2)
F5—F4—F8	70.8 (2)	Cs2 ⁱⁱ —F10—F2	140.5 (3)
F5—F4—F10 ^{xi}	163.6 (4)	Cs2 ⁱⁱ —F10—F2 ⁱⁱⁱ	60.40 (18)
F5—F4—F10 ^{viii}	77.6 (2)	Cs2 ⁱⁱ —F10—F4 ^{xv}	79.2 (2)
F5 ⁱ —F4—F8	63.3 (2)	Cs2 ⁱⁱ —F10—F4 ⁱⁱ	85.3 (2)
F5 ⁱ —F4—F10 ^{xi}	76.2 (2)	Cs2 ⁱⁱ —F10—F5 ⁱⁱ	80.24 (16)
F5 ⁱ —F4—F10 ^{viii}	158.1 (4)	Cs2 ⁱⁱ —F10—F6 ⁱⁱⁱ	146.5 (3)
F8—F4—F10 ^{xi}	123.2 (3)	Cs2 ⁱⁱ —F10—F7 ⁱⁱⁱ	96.0 (2)
F8—F4—F10 ^{viii}	99.3 (3)	Cs2 ⁱⁱ —F10—F9 ⁱⁱⁱ	100.21 (19)
F10 ^{xi} —F4—F10 ^{viii}	106.1 (2)	F1—F10—F1 ⁱⁱⁱ	165.7 (3)
Ce1—F5—Ce1 ⁱⁱⁱ	135.5 (3)	F1—F10—F2	88.8 (2)
Ce1—F5—Cs1 ^{xiii}	111.0 (2)	F1—F10—F2 ⁱⁱⁱ	106.5 (3)
Ce1—F5—F3	47.69 (18)	F1—F10—F4 ^{xv}	135.6 (3)
Ce1—F5—F3 ⁱⁱⁱ	106.9 (2)	F1—F10—F4 ⁱⁱ	60.2 (2)
Ce1—F5—F4	54.91 (17)	F1—F10—F5 ⁱⁱ	101.2 (2)
Ce1—F5—F4 ⁱⁱⁱ	146.6 (3)	F1—F10—F6 ⁱⁱⁱ	116.1 (2)
Ce1—F5—F6	47.24 (15)	F1—F10—F7 ⁱⁱⁱ	59.9 (2)
Ce1—F5—F7 ⁱⁱⁱ	101.7 (2)	F1—F10—F9 ⁱⁱⁱ	107.6 (2)
Ce1—F5—F8	42.39 (17)	F1 ⁱⁱⁱ —F10—F2	77.1 (2)
Ce1—F5—F8 ⁱⁱⁱ	155.2 (3)	F1 ⁱⁱⁱ —F10—F2 ⁱⁱⁱ	86.6 (2)
Ce1—F5—F9	62.5 (2)	F1 ⁱⁱⁱ —F10—F4 ^{xv}	56.2 (2)
Ce1—F5—F10 ^{viii}	103.2 (2)	F1 ⁱⁱⁱ —F10—F4 ⁱⁱ	112.4 (3)
Ce1 ⁱⁱⁱ —F5—Cs1 ^{xiii}	110.3 (2)	F1 ⁱⁱⁱ —F10—F5 ⁱⁱ	80.1 (2)
Ce1 ⁱⁱⁱ —F5—F3	150.7 (3)	F1 ⁱⁱⁱ —F10—F6 ⁱⁱⁱ	55.9 (2)
Ce1 ⁱⁱⁱ —F5—F3 ⁱⁱⁱ	42.70 (15)	F1 ⁱⁱⁱ —F10—F7 ⁱⁱⁱ	115.7 (3)
Ce1 ⁱⁱⁱ —F5—F4	149.7 (3)	F1 ⁱⁱⁱ —F10—F9 ⁱⁱⁱ	76.1 (2)

Ce1 ⁱⁱⁱ —F5—F4 ⁱⁱⁱ	53.13 (16)	F2—F10—F2 ⁱⁱⁱ	159.0 (3)
Ce1 ⁱⁱⁱ —F5—F6	105.16 (19)	F2—F10—F4 ^{xv}	118.6 (3)
Ce1 ⁱⁱⁱ —F5—F7 ⁱⁱⁱ	52.32 (16)	F2—F10—F4 ⁱⁱ	57.1 (2)
Ce1 ⁱⁱⁱ —F5—F8	110.0 (2)	F2—F10—F5 ⁱⁱ	84.2 (2)
Ce1 ⁱⁱⁱ —F5—F8 ⁱⁱⁱ	46.43 (17)	F2—F10—F6 ⁱⁱⁱ	66.1 (2)
Ce1 ⁱⁱⁱ —F5—F9	73.1 (2)	F2—F10—F7 ⁱⁱⁱ	85.8 (2)
Ce1 ⁱⁱⁱ —F5—F10 ^{viii}	102.6 (2)	F2—F10—F9 ⁱⁱⁱ	112.3 (2)
Cs1 ^{xiii} —F5—F3	65.45 (18)	F2 ⁱⁱⁱ —F10—F4 ^{xv}	59.6 (2)
Cs1 ^{xiii} —F5—F3 ⁱⁱⁱ	139.2 (3)	F2 ⁱⁱⁱ —F10—F4 ⁱⁱ	143.2 (3)
Cs1 ^{xiii} —F5—F4	80.3 (2)	F2 ⁱⁱⁱ —F10—F5 ⁱⁱ	106.2 (2)
Cs1 ^{xiii} —F5—F4 ⁱⁱⁱ	84.7 (2)	F2 ⁱⁱⁱ —F10—F6 ⁱⁱⁱ	93.8 (3)
Cs1 ^{xiii} —F5—F6	106.0 (2)	F2 ⁱⁱⁱ —F10—F7 ⁱⁱⁱ	89.5 (3)
Cs1 ^{xiii} —F5—F7 ⁱⁱⁱ	103.7 (2)	F2 ⁱⁱⁱ —F10—F9 ⁱⁱⁱ	49.86 (18)
Cs1 ^{xiii} —F5—F8	135.8 (2)	F4 ^{xv} —F10—F4 ⁱⁱ	104.0 (2)
Cs1 ^{xiii} —F5—F8 ⁱⁱⁱ	64.89 (17)	F4 ^{xv} —F10—F5 ⁱⁱ	53.02 (19)
Cs1 ^{xiii} —F5—F9	155.3 (3)	F4 ^{xv} —F10—F6 ⁱⁱⁱ	107.2 (3)
Cs1 ^{xiii} —F5—F10 ^{viii}	75.28 (16)	F4 ^{xv} —F10—F7 ⁱⁱⁱ	147.1 (3)
F3—F5—F3 ⁱⁱⁱ	154.5 (3)	F4 ^{xv} —F10—F9 ⁱⁱⁱ	94.1 (2)
F3—F5—F4	59.6 (2)	F4 ⁱⁱ —F10—F5 ⁱⁱ	51.12 (17)
F3—F5—F4 ⁱⁱⁱ	146.3 (3)	F4 ⁱⁱ —F10—F6 ⁱⁱⁱ	122.9 (3)
F3—F5—F6	53.13 (19)	F4 ⁱⁱ —F10—F7 ⁱⁱⁱ	108.0 (2)
F3—F5—F7 ⁱⁱⁱ	99.3 (2)	F4 ⁱⁱ —F10—F9 ⁱⁱⁱ	161.8 (2)
F3—F5—F8	87.2 (2)	F5 ⁱⁱ —F10—F6 ⁱⁱⁱ	130.4 (3)
F3—F5—F8 ⁱⁱⁱ	116.3 (3)	F5 ⁱⁱ —F10—F7 ⁱⁱⁱ	158.8 (3)
F3—F5—F9	99.2 (3)	F5 ⁱⁱ —F10—F9 ⁱⁱⁱ	146.7 (2)
F3—F5—F10 ^{viii}	104.0 (2)	F6 ⁱⁱⁱ —F10—F7 ⁱⁱⁱ	60.4 (2)
F3 ⁱⁱⁱ —F5—F4	111.0 (3)	F6 ⁱⁱⁱ —F10—F9 ⁱⁱⁱ	47.38 (19)
F3 ⁱⁱⁱ —F5—F4 ⁱⁱⁱ	55.0 (2)	F7 ⁱⁱⁱ —F10—F9 ⁱⁱⁱ	54.4 (2)

Symmetry codes: (i) $x, -y+3/2, z-1/2$; (ii) $x+1, -y+3/2, z+1/2$; (iii) $x, -y+3/2, z+1/2$; (iv) $-x+2, y-1/2, -z+1/2$; (v) $-x+2, -y+1, -z+1$; (vi) $-x+1, y-1/2, -z+1/2$; (vii) $-x+1, -y+1, -z$; (viii) $x-1, -y+3/2, z-1/2$; (ix) $x-1, y, z$; (x) $-x+1, -y+2, -z$; (xi) $x-1, y, z-1$; (xii) $-x+2, y+1/2, -z+1/2$; (xiii) $-x+1, y+1/2, -z+1/2$; (xiv) $x+1, y, z$; (xv) $x+1, y, z+1$.