data reports



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Crystal structure of 2-acetyl-5-(3methoxyphenyl)-3,7-dimethyl-5*H*-1,3thiazolo[3,2-a]pyrimidine-6-carboxylate

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Received 17 September 2014; accepted 21 October 2014

Edited by A. J. Lough, University of Toronto, Canada

In the title molecule, $C_{20}H_{22}N_2O_4S$, the pyrimidine ring is in a flattened half-chair conformation and the 3-methoxyphenyl substituent is in an axial arrangement. The thiazole ring forms a dihedral angle of 81.3 (1)° with the benzene ring. In the crystal, weak C-H···S interactions link molecules into chains along [001]. In addition, there are π - π interactions between inversion-related thiazole rings with a centroid–centroid distance of 3.529 (2) Å. The ethyl group was refined as disordered over two sets of sites with an occupancy ratio of 0.52 (3):0.48 (2).

Keywords: crystal structure; thiazolopyrimidine derivative; C—H···S interactions; π – π interactions.

CCDC reference: 1030239

1. Related literature

For pharmacological and biological properties of pyrimidine derivatives, see: Alam *et al.* (2010*a,b*). For the therapeutic potential of thiazolopyrimidine derivatives, see: Zhi *et al.* (2008). For related crystal structures, see: Jotani *et al.* (2010); Nagarajaiah *et al.* (2012).



Experimental
 Crystal data
 C₂₀H₂₂N₂O₄S

 $M_r = 386.46$

Triclinic, $P\overline{1}$ a = 8.281 (3) Å b = 9.680 (4) Å c = 12.821 (5) Å $\alpha = 76.423$ (10)° $\beta = 86.308$ (10)° $\gamma = 74.641$ (11)°

2.2. Data collection

Bruker SMART APEX CCDdetector diffractometer Absorption correction: multi-scan (*SADABS*; Bruker, 1998) *T*_{min} = 0.966, *T*_{max} = 0.969

2.3. Refinement

$R[F^2 > 2\sigma(F^2)] = 0.066$	263 parameters
$vR(F^2) = 0.173$	H-atom parameters constrained
S = 0.93	$\Delta \rho_{\rm max} = 0.34 \text{ e } \text{\AA}^{-3}$
170 reflections	$\Delta \rho_{\rm min} = -0.39 \text{ e } \text{\AA}^{-3}$

 Table 1

 Hydrogen-bond geometry (Å, °).

$D - H \cdot \cdot \cdot A$	D-H	$H \cdot \cdot \cdot A$	$D \cdot \cdot \cdot A$	$D - \mathbf{H} \cdots A$
$C18-H18B\cdots S1^{i}$	0.98	2.87	3.822 (3)	162
Symmetry code: (i) x y	1			

Symmetry code: (i) x, y, z - 1.

Data collection: *SMART* (Bruker, 1998); cell refinement: *SAINT* (Bruker, 1998); data reduction: *SAINT*; program(s) used to solve structure: *SHELXS97* (Sheldrick, 2008); program(s) used to refine structure: *SHELXL97* (Sheldrick, 2008); molecular graphics: *ORTEP-3 for Windows* (Farrugia, 2012) and *PLATON* (Spek, 2009); software used to prepare material for publication: *WinGX* (Farrugia, 2012).

Acknowledgements

NLP thanks for the UGC for the CSIR–NET fellowship and MSK thanks the UGC for the UGC–BSR Meritorious fellowship.

Supporting information for this paper is available from the IUCr electronic archives (Reference: LH5730).

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V = 963.3 (7) Å³

Mo $K\alpha$ radiation

 $0.18 \times 0.16 \times 0.16 \; \mathrm{mm}$

7744 measured reflections

4170 independent reflections

2529 reflections with $I > 2\sigma(I)$

 $\mu = 0.20 \text{ mm}^{-1}$

T = 100 K

 $R_{\rm int} = 0.040$

Z = 2

supporting information

Acta Cryst. (2014). E70, o1204 [doi:10.1107/S1600536814023162]

Crystal structure of 2-acetyl-5-(3-methoxyphenyl)-3,7-dimethyl-5*H*-1,3-thia-zolo[3,2-*a*]pyrimidine-6-carboxylate

N. L. Prasad, M. S. Krishnamurthy, H. Nagarajaiah and Noor Shahina Begum

S1. Comment

Pyrimidine derivatives are of interest because of their pharmacological properties (Alam *et al.*, 2010*a*). A thiazole ring fused to a pyrimidine ring resulting in thiazolopyrimidine is found to possess remarkable biological activities such as antiviral, anticancer, anti-inflammatory and anti-hypertensive properties (Alam *et al.*, 2010*b*). In addition, thiazolopyrimidine derivatives possess therapeutic potential (Zhi *et al.*, 2008). Herein, we report the crystal structure of the title compound. The molecular structure of the title compound is shown in Fig. 1. The mean-plane of the 3-methoxy phenyl group adopts a *syn* periplanar conformation with respect to the C5—H5 bond of the pyrimidine ring. The pyrimidine ring is in a flattened half chair conformation with atoms N1 and C5 displaced by -0.082 (3) and 0.189 (4)Å, respectively from the mean plane of the other four atoms (N2/C6/C7/C9). The 3-methoxy phenyl substituent bonded to atom C5 is in an axial position. The ethyl group was refined as disordered over two sets of sites with an occupancy ratio of 0.52 (3):0.48 (2). The bond lengths and angles in the title compound are in good agreement with the corresponding bond distances and angles reported in closely related structures (Nagarajaiah *et al.*, 2012; Jotani *et al.*, 2010). In the crystal, weak C—H···S interactions link molecules into chains along [001] (Fig. 2). In addition, there are $\pi \cdots \pi$ interactions between inversion related thiazole rings with a centroid–centroid distance of 3.529 (2) Å.

S2. Experimental

A mixture of 4-(3-methoxy-phenyl)-6-methyl-2-thioxo-1,2,3,4-tetrahydro-pyrimidine-5-carboxylic acid ethyl ester (10 mmol) and 3-chloro-2,4-pentanedione (10 mmol) was refluxed in dry ethanol (20 mmol) for 12 h. The excess of solvent was distilled off and the solid hydrochloride salt that separated was collected by filtration, suspended in water and neutralized by aqueous sodium carbonate solution to yield the free base. The solution was filtered, the solid washed with water, dried and recrystallized from ethyl acetate to give the title compound (76% yield, mp 380 K). The compound was recrystallized by slow evaporation from 1:1 mixture of ethyl acetate and methanol , yielding pale-yellow single crystals suitable for X-ray diffraction studies.

S3. Refinement

The H atoms were placed at calculated positions in the riding-model approximation with C—H = 0.95° A, 1.00 Å and 0.96 Å for aromatic, methyne and methyl H-atoms respectively, with $U_{iso}(H) = 1.5U_{eq}(C)$ for methyl H atoms and $U_{iso}(H) = 1.2U_{eq}(C)$ for other hydrogen atoms.



Figure 1

The molecular structure of the title compound with displacement ellipsoids drawn at the 50% probability level. H atoms are presented as small spheres of arbitrary radius. The primed atoms indicate the disorder.



Figure 2

Part of the crystal structure with weak C—H···S interactions shown as dashed lines. H atoms not involved in hydrogen bonding have been excluded.

2-Acetyl-5-(3-methoxy-phenyl)-3,7-dimethyl-5H-thiazolo[3,2-a]pyrimidine-6-carboxylic acid ethyl ester

Z = 2

F(000) = 408

 $\theta = 2.2 - 27.0^{\circ}$ $\mu = 0.20 \text{ mm}^{-1}$

Block, yellow

 $0.18 \times 0.16 \times 0.16$ mm

7744 measured reflections 4170 independent reflections 2529 reflections with $I > 2\sigma(I)$

 $\theta_{\text{max}} = 27.0^{\circ}, \ \theta_{\text{min}} = 2.2^{\circ}$

T = 100 K

 $R_{\rm int} = 0.040$

 $h = -10 \rightarrow 10$ $k = -12 \rightarrow 12$ $l = -11 \rightarrow 16$

 $D_{\rm x} = 1.332 {\rm Mg m^{-3}}$

Mo *K* α radiation, $\lambda = 0.71073$ Å

Cell parameters from 2529 reflections

Crystal data

 $\begin{array}{l} C_{20}H_{22}N_2O_4S\\ M_r = 386.46\\ \text{Triclinic, }P\overline{1}\\ \text{Hall symbol: -P 1}\\ a = 8.281 (3) \text{ Å}\\ b = 9.680 (4) \text{ Å}\\ c = 12.821 (5) \text{ Å}\\ a = 76.423 (10)^{\circ}\\ \beta = 86.308 (10)^{\circ}\\ \gamma = 74.641 (11)^{\circ}\\ V = 963.3 (7) \text{ Å}^3 \end{array}$

Data collection

Bruker SMART APEX CCD-detector
diffractometer
Radiation source: fine-focus sealed tube
Graphite monochromator
ω scans
Absorption correction: multi-scan
(SADABS; Bruker, 1998)
$T_{\min} = 0.966, \ T_{\max} = 0.969$

Refinement

Refinement on F^2	Secondary atom site location: difference Fourier
Least-squares matrix: Iuli $P(E^2 > 2 - (E^2)) = 0.000$	map
$\frac{R[F^2 > 2\sigma(F^2)] = 0.000}{wR(F^2) = 0.173}$	neighbouring sites
<i>S</i> = 0.93	H-atom parameters constrained
4170 reflections	$w = 1/[\sigma^2(F_o^2) + (0.076P)^2 + 0.6885P]$
263 parameters	where $P = (F_o^2 + 2F_c^2)/3$
0 restraints	$(\Delta/\sigma)_{\rm max} < 0.001$
Primary atom site location: structure-invariant	$\Delta \rho_{\rm max} = 0.34 \text{ e} \text{ Å}^{-3}$
direct methods	$\Delta \rho_{\rm min} = -0.39 \text{ e } \text{\AA}^{-3}$

Special details

Geometry. All s.u.'s (except the s.u. in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell s.u.'s are taken into account individually in the estimation of s.u.'s in distances, angles and torsion angles; correlations between s.u.'s in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell s.u.'s is used for estimating s.u.'s involving l.s. planes.

Refinement. Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F, with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R- factors based on ALL data will be even larger.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $(Å^2)$

	X	У	Ζ	$U_{ m iso}$ */ $U_{ m eq}$	Occ. (<1)
S 1	0.30579 (11)	0.36333 (9)	0.10093 (6)	0.0571 (3)	
N1	0.3525 (3)	0.4674 (2)	-0.09649 (16)	0.0408 (5)	
N2	0.1316 (3)	0.6205 (3)	-0.01435 (19)	0.0522 (6)	

01	0.6747 (4)	0.0390 (3)	0.0353 (3)	0.0991 (9)	
02	0.0460 (5)	0.9217 (3)	-0.3230 (3)	0.1344 (14)	
03	0.2781 (4)	0.7833 (3)	-0.37460 (18)	0.0887 (9)	
04	0.2791 (3)	0.3934 (3)	-0.53399(17)	0.0815 (7)	
C1	-0.0158(5)	0.8666 (4)	-0.0993 (3)	0.0738 (10)	
H1A	0.0392	0.9470	-0.1201	0.111*	
H1B	-0.0530	0.8581	-0.0244	0.111*	
H1C	-0.1128	0.8870	-0.1457	0.111*	
C2	0 4657 (4)	0.2623(3)	0.0315(2)	0.0505(7)	
C3	0.4737(3)	0.3342(3)	-0.0718(2)	0.0202(7) 0.0448(6)	
C4	0.1737(5) 0.5672(5)	0.1135(4)	0.0710(2) 0.0842(3)	0.0678 (9)	
C5	0.3072(3)	0.1135(4) 0.5520(3)	-0.2070(2)	0.0422 (6)	
С5 Н5	0.3087 (5)	0.5520 (5)	-0.2444	0.051*	
115 C6	0.4132 0.1873 (4)	0.6006 (3)	-0.2021(2)	0.031 0.0474(7)	
C0 C7	0.1075(4)	0.0990(3)	-0.1100(2)	0.0474(7)	
C?	0.1055(4)	0.7230(3)	0.1109(2)	0.0303(7)	
	0.3262 (0)	0.0389 (3)	0.1991 (3)	0.0938 (14)	
HðA	0.4158	0.0385	0.2040	0.144*	
H8B	0.5249	0.1339	0.2392	0.144*	
H&C	0.6109	-0.0315	0.2296	0.144*	
C9	0.2502 (3)	0.5029(3)	-0.0135 (2)	0.0435 (6)	
C10	0.314 (4)	0.886 (2)	-0.4/36 (17)	0.116 (7)	0.48 (3)
H10A	0.4280	0.8999	-0.4711	0.139*	0.48 (3)
H10B	0.2317	0.9832	-0.4829	0.139*	0.48 (3)
C10′	0.224 (2)	0.8853 (18)	-0.4809 (13)	0.085 (4)	0.52 (3)
H10C	0.1119	0.8797	-0.5001	0.102*	0.52 (3)
H10D	0.2164	0.9880	-0.4777	0.102*	0.52 (3)
C11	0.300 (2)	0.8136 (19)	-0.5624 (8)	0.102 (6)	0.48 (3)
H11A	0.4102	0.7506	-0.5754	0.152*	0.48 (3)
H11B	0.2622	0.8889	-0.6279	0.152*	0.48 (3)
H11C	0.2199	0.7537	-0.5422	0.152*	0.48 (3)
C11′	0.339 (2)	0.8426 (2)	-0.5548 (10)	0.182 (14)	0.52 (3)
H11D	0.4517	0.8313	-0.5285	0.273*	0.52 (3)
H11E	0.3191	0.9172	-0.6223	0.273*	0.52 (3)
H11F	0.3308	0.7485	-0.5669	0.273*	0.52 (3)
C12	0.2372 (2)	0.4638 (2)	-0.26787(15)	0.0422 (6)	
C13	0.2885 (2)	0.4605 (3)	-0.37231 (16)	0.0495 (7)	
H13	0.3699	0.5105	-0.4044	0.059*	
C14	0.2219(4)	0.3846(3)	-0.4306(2)	0.0561 (8)	
C15	0.1116 (4)	0.3055 (4)	-0.3822(3)	0.0669 (9)	
H15	0.0690	0.2502	-0.4208	0.080*	
C16	0.0622 (4)	0.3063 (4)	-0.2764(3)	0.0648 (9)	
H16	-0.0144	0.2515	-0.2432	0.078*	
C17	0 1232 (4)	0.3860 (3)	-0.2192(2)	0.070	
H17	0.0876	0.3875	-0.1474	0.060*	
C18	0.0070	0.3075	-0.6001(3)	0.000	
U10	0.2005 (0)	0.3271 (3)	-0.5711	0.0995 (15)	
	0.2330	0.2200	-0.6721	0.142	
	0.2317	0.3475	-0.6010	0.147	
11100	0.004/	0.3070	-0.0019	0.149	

supporting information

0.1592 (5)	0.8125 (4)	-0.3027 (3)	0.0715 (10)
0.5962 (4)	0.2884 (4)	-0.1555 (3)	0.0626 (8)
0.6810	0.1991	-0.1230	0.094*
0.6506	0.3673	-0.1864	0.094*
0.5375	0.2686	-0.2122	0.094*
	0.1592 (5) 0.5962 (4) 0.6810 0.6506 0.5375	0.1592 (5)0.8125 (4)0.5962 (4)0.2884 (4)0.68100.19910.65060.36730.53750.2686	$\begin{array}{cccccccccccccccccccccccccccccccccccc$

Atomic displacement parameters $(Å^2)$

	U^{11}	U^{22}	U^{33}	U^{12}	U^{13}	U ²³
S 1	0.0654 (5)	0.0657 (5)	0.0413 (4)	-0.0239 (4)	0.0025 (3)	-0.0068 (3)
N1	0.0435 (12)	0.0428 (11)	0.0375 (11)	-0.0094 (10)	0.0013 (9)	-0.0143 (9)
N2	0.0498 (14)	0.0546 (14)	0.0562 (15)	-0.0136 (12)	0.0120 (11)	-0.0231 (12)
01	0.086 (2)	0.0692 (16)	0.123 (2)	0.0134 (15)	-0.0095 (18)	-0.0203 (16)
02	0.163 (3)	0.090 (2)	0.097 (2)	0.038 (2)	-0.022 (2)	0.0100 (17)
03	0.145 (3)	0.0573 (14)	0.0516 (14)	-0.0198 (15)	0.0099 (15)	0.0022 (11)
O4	0.1022 (19)	0.0988 (18)	0.0448 (13)	-0.0126 (15)	-0.0014 (12)	-0.0338 (12)
C1	0.065 (2)	0.0558 (19)	0.103 (3)	-0.0046 (17)	0.004 (2)	-0.0358 (19)
C2	0.0505 (17)	0.0482 (15)	0.0546 (17)	-0.0154 (14)	-0.0096 (13)	-0.0094 (13)
C3	0.0438 (15)	0.0420 (14)	0.0518 (16)	-0.0090 (12)	-0.0074 (12)	-0.0172 (12)
C4	0.063 (2)	0.060 (2)	0.082 (2)	-0.0211 (18)	-0.0222 (19)	-0.0070 (18)
C5	0.0461 (15)	0.0435 (14)	0.0367 (14)	-0.0118 (12)	0.0024 (11)	-0.0088 (11)
C6	0.0532 (17)	0.0395 (14)	0.0509 (16)	-0.0122 (13)	-0.0054 (13)	-0.0114 (12)
C7	0.0480 (17)	0.0445 (15)	0.0637 (19)	-0.0122 (13)	0.0008 (14)	-0.0215 (14)
C8	0.105 (3)	0.091 (3)	0.083 (3)	-0.042 (3)	-0.031 (2)	0.025 (2)
C9	0.0454 (15)	0.0511 (15)	0.0408 (14)	-0.0191 (13)	0.0057 (12)	-0.0176 (12)
C10	0.156 (18)	0.101 (8)	0.068 (9)	-0.029 (14)	0.018 (13)	0.017 (6)
C10′	0.103 (9)	0.066 (5)	0.064 (6)	-0.013 (7)	-0.008 (7)	0.020 (4)
C11	0.139 (12)	0.113 (10)	0.039 (7)	-0.022 (9)	-0.009 (7)	0.001 (6)
C11′	0.185 (19)	0.136 (14)	0.127 (17)	0.035 (13)	0.078 (15)	0.052 (13)
C12	0.0430 (15)	0.0424 (13)	0.0394 (14)	-0.0039 (12)	-0.0023 (11)	-0.0133 (11)
C13	0.0559 (18)	0.0520 (16)	0.0394 (15)	-0.0100 (14)	0.0015 (13)	-0.0126 (12)
C14	0.0628 (19)	0.0617 (18)	0.0406 (16)	-0.0011 (16)	-0.0048 (14)	-0.0211 (14)
C15	0.070 (2)	0.068 (2)	0.072 (2)	-0.0101 (18)	-0.0140 (18)	-0.0388 (18)
C16	0.062 (2)	0.069 (2)	0.075 (2)	-0.0282 (18)	0.0025 (17)	-0.0256 (17)
C17	0.0510 (17)	0.0561 (16)	0.0472 (16)	-0.0147 (14)	0.0023 (13)	-0.0176 (13)
C18	0.150 (4)	0.093 (3)	0.052 (2)	-0.004 (3)	-0.023 (2)	-0.035 (2)
C19	0.100 (3)	0.0505 (19)	0.060 (2)	-0.0115 (19)	-0.015 (2)	-0.0099 (16)
C20	0.0558 (19)	0.0620 (18)	0.067 (2)	0.0026 (15)	-0.0006 (16)	-0.0283 (16)

Geometric parameters (Å, °)

S1—C9	1.736 (3)	C8—H8C	0.9800
S1—C2	1.753 (3)	C10—C11	1.50 (4)
N1—C9	1.368 (3)	C10—H10A	0.9900
N1—C3	1.391 (3)	C10—H10B	0.9900
N1—C5	1.475 (3)	C10'—C11'	1.358 (19)
N2—C9	1.290 (4)	C10'—H10C	0.9900
N2—C7	1.391 (4)	C10'—H10D	0.9900

O1—C4	1.228 (4)	C11—H11A	0.9800
O2—C19	1.201 (4)	C11—H11B	0.9800
O3—C19	1.325 (4)	C11—H11C	0.9800
O3—C10	1.486 (18)	C11′—H11D	0.9800
O3—C10′	1.499 (15)	C11′—H11E	0.9800
O4—C14	1.370 (4)	C11′—H11F	0.9800
O4—C18	1.420 (4)	C12—C13	1.3835
C1—C7	1.502 (4)	C12—C17	1.389 (3)
C1—H1A	0.9800	C13—C14	1 388 (4)
C1—H1B	0.9800	C13—H13	0.9500
C1—H1C	0.9800	C14-C15	1.372(5)
C_2	1 350 (4)	C_{15}	1.372(5) 1.392(5)
$C_2 = C_3$	1.330(4) 1.487(4)	C15 H15	0.9500
$C_2 = C_4$	1.407(4)	C16 C17	1.382(4)
$C_3 = C_2 0$	1.491(4)	C_{10}	1.382 (4)
C4 - C8	1.495(3)		0.9300
C5—C12	1.520(3)		0.9500
C5—C6	1.527 (4)	CI8—HI8A	0.9800
C5—H5	1.0000		0.9800
	1.353 (4)	CI8—HI8C	0.9800
C6—C19	1.468 (4)	C20—H20A	0.9800
C8—H8A	0.9800	C20—H20B	0.9800
C8—H8B	0.9800	C20—H20C	0.9800
C9—S1—C2	91.44 (13)	C11—C10—H10B	110.9
C9—N1—C3	115.6 (2)	H10A—C10—H10B	108.9
C9—N1—C5	119.6 (2)	C11'—C10'—O3	107.3 (13)
C3—N1—C5	123.6 (2)	C11'—C10'—H10C	110.3
C9—N2—C7	116.3 (2)	O3—C10′—H10C	110.3
C19—O3—C10	127.2 (10)	C11'—C10'—H10D	110.3
C19—O3—C10′	108.8 (8)	O3—C10′—H10D	110.3
C14—O4—C18	117.5 (3)	H10C—C10′—H10D	108.5
C7—C1—H1A	109.5	C10′—C11′—H11D	109.5
C7—C1—H1B	109.5	C10′—C11′—H11E	109.5
H1A—C1—H1B	109.5	H11D—C11′—H11E	109.5
C7—C1—H1C	109.5	C10′—C11′—H11F	109.5
H1A—C1—H1C	109.5	H11D—C11′—H11F	109.5
H1B-C1-H1C	109.5	H11E—C11′—H11F	109.5
$C_{3}-C_{2}-C_{4}$	127.6 (3)	C_{13} C_{12} C_{17}	119 90 (16)
C_{3} C_{2} S_{1}	1112(2)	C_{13} C_{12} C_{13}	119.30 (16)
C_{4} C_{2} S_{1}	111.2(2) 121.2(2)	C17 - C12 - C5	120.8(2)
C_{2} C_{3} N1	1121.2(2) 1125(2)	C_{12} C_{12} C_{13} C_{14}	120.5(2)
$C_2 = C_3 = C_2 O_1$	112.3(2) 127.7(3)	$C_{12} = C_{13} = C_{14}$	120.33 (17)
$C_2 = C_3 = C_{20}$	127.7(3) 110.8(2)	C12 - C13 - III3	119.7
01 C4 C2	119.0(2) 121.0(2)	$C_1 + C_1 - C_1 $	117.1
01 - 04 - 02	121.9(3) 122.2(4)	04 - 014 - 013	123.4(3)
$C_1 = C_4 = C_8$	122.3(4)	04 - 014 - 013	114.9 (3)
12-14-18	$113.\delta(3)$	C13 - C14 - C13	119.7 (3)
NI-05-012	110.26 (19)		119.9 (3)
NI-C5-C6	108.5 (2)	C14—C15—H15	120.1

C12—C5—C6	112.6 (2)	C16—C15—H15	120.1
N1—C5—H5	108.5	C17—C16—C15	120.8 (3)
С12—С5—Н5	108.5	C17—C16—H16	119.6
С6—С5—Н5	108.5	C15—C16—H16	119.6
C7—C6—C19	121.2 (3)	C16—C17—C12	119.2 (3)
C7—C6—C5	122.3 (2)	С16—С17—Н17	120.4
C19—C6—C5	116.5 (3)	С12—С17—Н17	120.4
C6—C7—N2	122.2 (3)	O4—C18—H18A	109.5
C6-C7-C1	125.6(3)	O4-C18-H18B	109.5
N2-C7-C1	112.1 (3)	H18A—C18—H18B	109.5
C4—C8—H8A	109 5	04-C18-H18C	109.5
C4-C8-H8B	109.5	H18A - C18 - H18C	109.5
H8A - C8 - H8B	109.5	H18B-C18-H18C	109.5
C4 - C8 - H8C	109.5	$0^{2}-C^{19}-O^{3}$	109.5 120.5(3)
H8A - C8 - H8C	109.5	02 - C19 - C6	120.3(3)
	109.5	$O_2 = C_1 + C_0$	127.3(4) 112.2(3)
$N_2 = C_0 = N_1$	127.9 (3)	$C_3 = C_{10} = C_0$	112.2 (3)
$N_2 = C_9 = N_1$	127.9(3) 122.8(2)	C_{3} C_{20} H_{20R}	109.5
$N_2 = C_2 = S_1$	122.0(2) 100.2(2)	L_{20} L_{20} L_{20} L_{20} L_{20}	109.5
11 - 0 - 51	109.3(2) 104.5(18)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	109.5
$O_2 = C_1 O_2 = U_1 O_4$	104.3 (18)	C_{3} C_{20} $H_{20}C_{20}$	109.5
C_{11} C_{10} H_{10A}	110.9	$H_{20}A = C_{20} = H_{20}C$	109.5
C10 $H10A$	110.9	H20B-C20-H20C	109.5
03-C10-H10B	110.9		
C0 S1 $C2$ $C3$	0.6(2)	C3 N1 C9 S1	-0.6(3)
$C_{9} = S_{1} = C_{2} = C_{3}$	-176.3(2)	$C_{5} = N_{1} = C_{5} = S_{1}$	167.21(17)
$C_{2} = S_{1} = C_{2} = C_{4}$	170.3(2)	$C_{2} = N_{1} - C_{2} - S_{1}$	-178.8(2)
C4 - C2 - C3 - N1	1/3.0(3)	$U_2 = 0 = U_2 = 0_2$	
S1 C2 C2 N1	1.0.(2)	$C_2 = C_1 = C_0 = N_1$	1,0.0(2)
S1—C2—C3—N1	-1.0 (3)	C2—S1—C9—N1	-0.02(19)
S1—C2—C3—N1 C4—C2—C3—C20 S1—C2—C3—C20	-1.0 (3) -6.0 (5)	C2—S1—C9—N1 C19—O3—C10—C11	-0.02 (19) -122.6 (13)
S1-C2-C3-N1 C4-C2-C3-C20 S1-C2-C3-C20	-1.0 (3) -6.0 (5) 177.3 (2)	C2—S1—C9—N1 C19—O3—C10—C11 C10′—O3—C10—C11	-0.02 (19) -122.6 (13) -64 (3)
S1—C2—C3—N1 C4—C2—C3—C20 S1—C2—C3—C20 C9—N1—C3—C2	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3)	C2—S1—C9—N1 C19—O3—C10—C11 C10′—O3—C10—C11 C19—O3—C10′—C11′ C19—O3—C10′—C11′	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \end{array}$
S1—C2—C3—N1 C4—C2—C3—C20 S1—C2—C3—C20 C9—N1—C3—C2 C5—N1—C3—C2	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2)	C2—S1—C9—N1 C19—O3—C10—C11 C10'—O3—C10—C11 C19—O3—C10'—C11' C10—O3—C10'—C11'	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \end{array}$
S1—C2—C3—N1 C4—C2—C3—C20 S1—C2—C3—C20 C9—N1—C3—C2 C5—N1—C3—C2 C9—N1—C3—C2 C9—N1—C3—C20	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2)	C2—S1—C9—N1 C19—O3—C10—C11 C10'—O3—C10—C11 C19—O3—C10'—C11' C10—O3—C10'—C11' N1—C5—C12—C13	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.6 \ (2) \end{array}$
S1-C2-C3-N1 C4-C2-C3-C20 S1-C2-C3-C20 C9-N1-C3-C2 C5-N1-C3-C2 C9-N1-C3-C20 C5-N1-C3-C20 C5-N1-C3-C20	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4)	C2—S1—C9—N1 C19—O3—C10—C11 C10′—O3—C10—C11 C19—O3—C10′—C11′ C10—O3—C10′—C11′ N1—C5—C12—C13 C6—C5—C12—C13	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \end{array}$
S1-C2-C3-N1 C4-C2-C3-C20 S1-C2-C3-C20 C9-N1-C3-C2 C5-N1-C3-C2 C9-N1-C3-C20 C5-N1-C3-C20 C5-N1-C3-C20 C3-C2-C4-O1	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4) 0.5 (5)	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ N1 \\ -C5 \\ -C12 \\ -C13 \\ C6 \\ -C5 \\ -C12 \\ -C13 \\ N1 \\ -C5 \\ -C12 \\ -C17 \\ C17 \\ -C17 $	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ 72.0 \ (2) \end{array}$
S1—C2—C3—N1 C4—C2—C3—C20 S1—C2—C3—C20 C9—N1—C3—C2 C5—N1—C3—C2 C9—N1—C3—C20 C5—N1—C3—C20 C5—N1—C3—C20 C3—C2—C4—O1 S1—C2—C4—O1	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4) 0.5 (5) 176.9 (3)	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10' \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ N1 \\ -C5 \\ -C12 \\ -C13 \\ C12 \\ -C13 \\ N1 \\ -C5 \\ -C12 \\ -C17 \\ C6 \\ -C5 \\ -C12 \\ -C17 \\ C15 \\ -C12 \\ -C17 \\ -C17 \\ -C15 \\ -C12 \\ -C17 \\ -C17 \\ -C15 \\ -C12 \\ -C17 \\ -C$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C2 \\ C9 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ C3 & -C2 & -C4 & -C8 \\ \hline\end{array}$	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4) 0.5 (5) 176.9 (3) -177.6 (3)	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ N1 \\ -C5 \\ -C12 \\ -C13 \\ C6 \\ -C5 \\ -C12 \\ -C13 \\ N1 \\ -C5 \\ -C12 \\ -C17 \\ C6 \\ -C5 \\ -C12 \\ -C17 \\ C17 \\ -C12 \\ -C13 \\ -C14 \\ \end{array}$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ C3 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ \end{array}$	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4) 0.5 (5) 176.9 (3) -177.6 (3) -1.2 (4)	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10' \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10' \\ -C11' \\ -C12 \\ -C13 \\ -C11' \\ -C12 \\ -C13 \\ -C14 \\ C5 \\ -C12 \\ -C14 \\ -$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ C3 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ C9 & -N1 & -C5 & -C12 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \end{array}$	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C19 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -C11' \\ -C12 \\ -C11 \\ -C12 \\ -C13 \\ -C14 \\ C5 \\ -C12 \\ -C14 \\ -C14 \\ -C15 \\ -C15 \\ -C12 \\ -C15 \\$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ C9 & -N1 & -C5 & -C12 \\ C3 & -N1 & -C5 & -C12 \\ C3 & -N1 & -C5 & -C12 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \end{array}$	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ C10 \\ -O3 \\ -C10' \\ -C11' \\ -C11' \\ -C12 \\ -C13 \\ -C11' \\ -C12 \\ -C13 \\ -C14 \\ C5 \\ -C12 \\ -C13 \\ -C14 \\ -C14 \\ -C15 \\ C18 \\ -O4 \\ -C14 \\ -C13 \\ -C13 \\ -C13 \\ -C13 \\ -C13 \\ -C14 \\ -C13 \\ -C13 \\ -C14 \\ -C13 \\ -C13 \\ -C13 \\ -C14 \\ -C13 \\ -C14 \\ -C13 \\ -C13 \\ -C13 \\ -C13 \\ -C13 \\ -C14 \\ -C13 \\ -C14 \\ -C13 \\ -C13 \\ -C14 \\ -C14 \\ -C13 \\ -C14 \\ -C14 \\ -C14 \\ -C13 \\ -C14 \\ -C14 \\ -C13 \\ -C14 \\ -C14 \\ -C14 \\ -C13 \\ -C14 \\ $	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ C9 & -N1 & -C5 & -C12 \\ C3 & -N1 & -C5 & -C12 \\ C9 & -N1 & -C5 & -C6 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \end{array}$	$\begin{array}{c} C2 &= S1 &= C9 &= N1 \\ C19 &= O3 &= C10 &= C11 \\ C10' &= O3 &= C10' &= C11' \\ C10 &= O3 &= C10' &= C11' \\ C10 &= O3 &= C10' &= C11' \\ N1 &= C5 &= C12 &= C13 \\ C6 &= C5 &= C12 &= C13 \\ C6 &= C5 &= C12 &= C17 \\ C6 &= C5 &= C12 &= C17 \\ C17 &= C12 &= C13 &= C14 \\ C5 &= C12 &= C13 &= C14 \\ C18 &= O4 &= C14 &= C13 \\ C12 &= C13 &= C14 &= O4 \\ \end{array}$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ C9 & -N1 & -C5 & -C12 \\ C3 & -N1 & -C5 & -C6 \\ C3 & -N1 & -C5 & -C6 \\ \end{array}$	-1.0 (3) -6.0 (5) 177.3 (2) 1.1 (3) -166.2 (2) -177.4 (2) 15.4 (4) 0.5 (5) 176.9 (3) -177.6 (3) -1.2 (4) -103.6 (2) 63.1 (3) 20.1 (3) -173.1 (2)	$\begin{array}{c} C2 &= S1 &= C9 &= N1 \\ C19 &= O3 &= C10 &= C11 \\ C10' &= O3 &= C10' &= C11' \\ C10 &= O3 &= C10' &= C11' \\ N1 &= C5 &= C12 &= C13 \\ C6 &= C5 &= C12 &= C13 \\ N1 &= C5 &= C12 &= C17 \\ C6 &= C5 &= C12 &= C17 \\ C17 &= C12 &= C17 \\ C18 &= O4 &= C14 &= C15 \\ C18 &= O4 &= C14 &= C15 \\ C12 &= C13 &= C14 &= C15 \\ C12 &= C13 &= C14 &= C15 \\ \end{array}$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \end{array}$
$\begin{array}{c} S1 & -C2 & -C3 & -N1 \\ C4 & -C2 & -C3 & -C20 \\ S1 & -C2 & -C3 & -C20 \\ C9 & -N1 & -C3 & -C2 \\ C5 & -N1 & -C3 & -C20 \\ C5 & -N1 & -C3 & -C20 \\ C3 & -C2 & -C4 & -O1 \\ S1 & -C2 & -C4 & -O1 \\ C3 & -C2 & -C4 & -O1 \\ C3 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ S1 & -C2 & -C4 & -C8 \\ C9 & -N1 & -C5 & -C12 \\ C3 & -N1 & -C5 & -C6 \\ C3 & -N1 & -C5 & -C6 \\ N1 & -C5 & -C6 & -C7 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \\ -173.1 (2) \\ -15.3 (3) \end{array}$	$\begin{array}{c} C2 &= S1 &= C9 &= N1 \\ C19 &= O3 &= C10 &= C11 \\ C10' &= O3 &= C10' &= C11' \\ C10 &= O3 &= C10' &= C11' \\ N1 &= C5 &= C12 &= C13 \\ C6 &= C5 &= C12 &= C13 \\ N1 &= C5 &= C12 &= C17 \\ C6 &= C5 &= C12 &= C17 \\ C17 &= C12 &= C13 &= C14 \\ C5 &= C12 &= C13 &= C14 \\ C18 &= O4 &= C14 &= C15 \\ C18 &= O4 &= C14 &= C15 \\ C18 &= O4 &= C14 &= C15 \\ C12 &= C13 &= C14 &= O4 \\ C12 &= C13 &= C14 &= C15 \\ O4 &= C14 &= C15 &= C16 \\ \end{array}$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \\ -179.6 \ (3) \end{array}$
$\begin{array}{c} S1 &C2 &C3 &N1 \\ C4 &C2 &C3 &C20 \\ S1 &C2 &C3 &C20 \\ C9 &N1 &C3 &C2 \\ C5 &N1 &C3 &C20 \\ C5 &N1 &C3 &C20 \\ C3 &C2 &C4 &O1 \\ S1 &C2 &C4 &O1 \\ C3 &C2 &C4 &C8 \\ S1 &C2 &C4 &C8 \\ C9 &N1 &C5 &C12 \\ C3 &N1 &C5 &C6 \\ C3 &N1 &C5 &C6 \\ N1 &C5 &C6 &C7 \\ C12 &C5 &C6 &C7 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \\ -173.1 (2) \\ -15.3 (3) \\ 107.0 (3) \end{array}$	$\begin{array}{c} C2 &= S1 &= C9 &= N1 \\ C19 &= O3 &= C10 &= C11 \\ C10' &= O3 &= C10' &= C11' \\ C10 &= O3 &= C10' &= C11' \\ N1 &= C5 &= C12 &= C13' \\ C6 &= C5 &= C12 &= C13 \\ N1 &= C5 &= C12 &= C17 \\ C6 &= C5 &= C12 &= C17 \\ C17 &= C12 &= C13 &= C14 \\ C5 &= C12 &= C13 &= C14 \\ C18 &= O4 &= C14 &= C13 \\ C18 &= O4 &= C14 &= C13 \\ C18 &= O4 &= C14 &= C13 \\ C12 &= C13 &= C14 &= C15 \\ O4 &= C14 &= C15 &= C16 \\ C13 &= C14 &= C15 &= C16 \\ \end{array}$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \\ -179.6 \ (3) \\ 2.5 \ (5) \end{array}$
$\begin{array}{c} S1 &C2 &C3 &N1 \\ C4 &C2 &C3 &C20 \\ S1 &C2 &C3 &C20 \\ C9 &N1 &C3 &C2 \\ C5 &N1 &C3 &C20 \\ C5 &N1 &C3 &C20 \\ C3 &C2 &C4 &O1 \\ S1 &C2 &C4 &O1 \\ S1 &C2 &C4 &C8 \\ S1 &C5 &C6 \\ C3 &N1 &C5 &C6 \\ N1 &C5 &C6 &C7 \\ N1 &C5 &C6 &C7 \\ N1 &C5 &C6 &C19 \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \\ -173.1 (2) \\ -15.3 (3) \\ 107.0 (3) \\ 166.4 (2) \end{array}$	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C11 \\ -C5 \\ -C12 \\ -C13 \\ -C12 \\ -C13 \\ -C14 \\ -C13 \\ -C14 \\ -C15 \\ -C14 \\ -C15 \\ -C16 \\ -C16 \\ -C17 \\ -C17 \\ -C16 \\ -C17 \\ -C16 \\ -C17 \\ -C17 \\ -C10 \\ -C17 \\ -C10 \\ -C11 \\ -C15 \\ -C16 \\ -C17 \\ -C17 \\ -C10 \\ -C11 \\ -C15 \\ -C16 \\ -C17 \\ -C17 \\ -C11 \\ -C17 \\ -C11 \\ -C11 \\ -C17 \\ -C11 \\ -C11 \\ -C17 \\ -C11 \\ -C17 \\ -C11 \\ -C17 \\ -C11 \\ -C1$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \\ -179.6 \ (3) \\ 2.5 \ (5) \\ -0.1 \ (5) \end{array}$
$\begin{array}{c} \text{S1}-\text{C2}-\text{C3}-\text{N1} \\ \text{C4}-\text{C2}-\text{C3}-\text{C20} \\ \text{S1}-\text{C2}-\text{C3}-\text{C20} \\ \text{C9}-\text{N1}-\text{C3}-\text{C2} \\ \text{C5}-\text{N1}-\text{C3}-\text{C2} \\ \text{C9}-\text{N1}-\text{C3}-\text{C20} \\ \text{C5}-\text{N1}-\text{C3}-\text{C20} \\ \text{C5}-\text{C2}-\text{C4}-\text{O1} \\ \text{S1}-\text{C2}-\text{C4}-\text{O1} \\ \text{S1}-\text{C2}-\text{C4}-\text{O1} \\ \text{C3}-\text{C2}-\text{C4}-\text{C8} \\ \text{S1}-\text{C2}-\text{C4}-\text{C8} \\ \text{S1}-\text{C2}-\text{C4}-\text{C8} \\ \text{C9}-\text{N1}-\text{C5}-\text{C12} \\ \text{C3}-\text{N1}-\text{C5}-\text{C12} \\ \text{C3}-\text{N1}-\text{C5}-\text{C6} \\ \text{C3}-\text{N1}-\text{C5}-\text{C6} \\ \text{N1}-\text{C5}-\text{C6} \\ \text{C7} \\ \text{C12}-\text{C5}-\text{C6}-\text{C7} \\ \text{N1}-\text{C5}-\text{C6}-\text{C19} \\ \text{C12}-\text{C5}-\text{C6}-\text{C19} \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \\ -173.1 (2) \\ -15.3 (3) \\ 107.0 (3) \\ 166.4 (2) \\ -71.2 (3) \end{array}$	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ -C11 \\ -C12 \\ -C11 \\ -C12 \\ -C13 \\ -C11 \\ -C12 \\ -C13 \\ -C14 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C12 \\ -C12 \\ -C12 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C1$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -136.62 \ (19) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \\ -179.6 \ (3) \\ 2.5 \ (5) \\ -0.1 \ (5) \\ -1.1 \ (5) \end{array}$
$\begin{array}{c} \text{S1} - \text{C2} - \text{C3} - \text{N1} \\ \text{C4} - \text{C2} - \text{C3} - \text{C20} \\ \text{S1} - \text{C2} - \text{C3} - \text{C20} \\ \text{C9} - \text{N1} - \text{C3} - \text{C2} \\ \text{C5} - \text{N1} - \text{C3} - \text{C2} \\ \text{C5} - \text{N1} - \text{C3} - \text{C20} \\ \text{C5} - \text{N1} - \text{C3} - \text{C20} \\ \text{C5} - \text{C3} - \text{C2} - \text{C4} - \text{O1} \\ \text{S1} - \text{C2} - \text{C4} - \text{O1} \\ \text{S1} - \text{C2} - \text{C4} - \text{O1} \\ \text{C3} - \text{C2} - \text{C4} - \text{C8} \\ \text{S1} - \text{C2} - \text{C4} - \text{C8} \\ \text{S1} - \text{C2} - \text{C4} - \text{C8} \\ \text{C9} - \text{N1} - \text{C5} - \text{C12} \\ \text{C3} - \text{N1} - \text{C5} - \text{C12} \\ \text{C9} - \text{N1} - \text{C5} - \text{C6} \\ \text{C3} - \text{N1} - \text{C5} - \text{C6} \\ \text{N1} - \text{C5} - \text{C6} - \text{C7} \\ \text{N1} - \text{C5} - \text{C6} - \text{C7} \\ \text{N1} - \text{C5} - \text{C6} - \text{C19} \\ \text{C12} - \text{C5} - \text{C6} - \text{C19} \\ \text{C19} - \text{C6} - \text{C7} - \text{N2} \\ \end{array}$	$\begin{array}{c} -1.0 (3) \\ -6.0 (5) \\ 177.3 (2) \\ 1.1 (3) \\ -166.2 (2) \\ -177.4 (2) \\ 15.4 (4) \\ 0.5 (5) \\ 176.9 (3) \\ -177.6 (3) \\ -1.2 (4) \\ -103.6 (2) \\ 63.1 (3) \\ 20.1 (3) \\ -173.1 (2) \\ -15.3 (3) \\ 107.0 (3) \\ 166.4 (2) \\ -71.2 (3) \\ -179.1 (3) \end{array}$	$\begin{array}{c} C2 \\ -S1 \\ -C9 \\ -N1 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C19 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ C10 \\ -O3 \\ -C10 \\ -C11 \\ -C11 \\ -C12 \\ -C11 \\ -C12 \\ -C13 \\ -C12 \\ -C13 \\ -C14 \\ -C14 \\ -C15 \\ -C14 \\ -C15 \\ -C16 \\ -C16 \\ -C17 \\ -C16 \\ -C17 \\ -C12 \\ -C16 \\ -C17 \\ -C16 \\ -C17 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C17 \\ -C12 \\ -C12 \\ -C12 \\ -C13 \\ -C14 \\ -C15 \\ -C16 \\ -C17 \\ -C12 \\ -C12 \\ -C17 \\ -C16 \\ -C17 \\ -C12 \\ -C13 \\ -C12 \\ -C17 \\ -C16 \\ -C17 \\ -C17 \\ -C16 \\ -C17 \\ -C17 \\ -C16 \\ -C17 \\ -C16 \\ -C17 \\ -C1$	$\begin{array}{c} -0.02 \ (19) \\ -122.6 \ (13) \\ -64 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -173.7 \ (13) \\ 52 \ (3) \\ -173.6 \ (219) \\ 102.0 \ (2) \\ 42.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -78.8 \ (3) \\ 2.6 \ (3) \\ -178.2 \ (2) \\ 6.5 \ (5) \\ -175.5 \ (3) \\ 178.1 \ (2) \\ -3.8 \ (4) \\ -179.6 \ (3) \\ 2.5 \ (5) \\ -0.1 \ (5) \\ -1.1 \ (5) \\ -0.2 \ (4) \end{array}$

supporting information

C19—C6—C7—C1	-1.8 (5)	C10—O3—C19—O2	14.9 (17)
C5—C6—C7—C1	-180.0 (3)	C10′—O3—C19—O2	-11.8 (9)
C9—N2—C7—C6	6.6 (4)	C10—O3—C19—C6	-164.6 (16)
C9—N2—C7—C1	-171.1 (2)	C10′—O3—C19—C6	168.8 (8)
C7—N2—C9—N1	-0.9 (4)	C7—C6—C19—O2	-15.5 (6)
C7—N2—C9—S1	177.68 (19)	C5—C6—C19—O2	162.8 (4)
C3—N1—C9—N2	178.1 (2)	C7—C6—C19—O3	163.9 (3)
C_{5} N1- C_{9} N2 C5-N1-C9-N2	-14.1(4)	C5—C6—C19—O3	-17.8 (4)

Hydrogen-bond geometry (Å, °)

D—H···A	D—H	H···A	D····A	<i>D</i> —H··· <i>A</i>
C18—H18B···S1 ⁱ	0.98	2.87	3.822 (3)	162

Symmetry code: (i) x, y, z-1.