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# $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ containing $\left[\mathrm{WO}_{6}\right]$ octahedra 

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A polycrystalline sample of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$, nonastrontium dilanthanum tetrakis[orthotungstate(VI)], was prepared by heating a compacted powder mixture of $\mathrm{SrCO}_{3}, \mathrm{WO}_{3}$, and $\mathrm{La}_{2} \mathrm{O}_{3}$ with an $\mathrm{Sr}: \mathrm{La}: \mathrm{W}$ molar ratio of 9:2:4 at 1473 K . X-ray crystal structure analysis was performed for a $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ single-crystal grain grown by reheating the sample at $1673 \mathrm{~K} . \mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ crystallizes with four formula units in the tetragonal space group $I 4_{1} / a$ and is isotypic with $\mathrm{Sr}_{11}\left(\mathrm{ReO}_{6}\right)_{4}$. Two W sites with site symmetries of $\overline{1}$ are located at the center of isolated $\left[\mathrm{WO}_{6}\right.$ ] octahedra, and four mixed $(\mathrm{Sr} / \mathrm{La})$ sites are surrounded by eight to twelve O atoms of the $\left[\mathrm{WO}_{6}\right]$ octahedra. The structure of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ can be described on the basis of the double-perovskite structure with $\left[\mathrm{WO}_{6}\right]$ and $\left[(\mathrm{Sr} / \mathrm{La}) \mathrm{O}_{x}\right]$ polyhedra alternately placed, and a vacancy ( $\square$ ).

## 1. Chemical context

The alkaline-earth ( $A$ ) rare-earth ( $L n$ ) tungstates $A_{9} L n_{2}\left(\mathrm{WO}_{6}\right)_{4}$ have attracted attention as host crystals of phosphors, and various luminescence properties of these tungstates doped with activators such as $\mathrm{Eu}^{3+}$ and $\mathrm{Mn}^{4+}$ have been evaluated. For example, emissions of $\mathrm{Eu}^{3+}$ at $\sim 615 \mathrm{~nm}$ excited by $\sim 395 \mathrm{~nm}$ wavelength light have been reported for $\mathrm{Sr}_{9} \mathrm{Gd}_{1.5} \mathrm{Eu}_{0.5}\left(\mathrm{WO}_{6}\right)_{4} \quad$ (Blasse \& Kemmler-Sack, 1983), $\mathrm{Ca}_{9} \mathrm{Gd}_{2-x} \mathrm{Eu}_{x}\left(\mathrm{WO}_{6}\right)_{4}$ (Zeng et al., 2013), $\mathrm{Ca}_{9} \mathrm{Eu}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ (Qin et al., 2012; Zeng et al., 2010), $\mathrm{Sr}_{9} \mathrm{Eu}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ (Qin et al., 2012; Blasse \& Kemmler-Sack, 1983; Zeng et al., 2010), and Ca9${ }_{x} \mathrm{Sr}_{x} \mathrm{Eu}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ (Zeng et al., 2009). $\mathrm{Mn}^{4+}$-doped $\mathrm{Sr}_{9} \mathrm{Y}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ (Shi et al., 2019) and $\mathrm{Mn}^{4+} / \mathrm{Mg}^{2+}$-doped $\mathrm{Sr}_{9} \mathrm{Y}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ (Zhou et al., 2020) were also studied, and deep-red luminescence with broad emission maxima at $\sim 680 \mathrm{~nm}$ were observed under excitation by light with a wavelength of 365 nm .

Unit-cell parameters of a tetragonal cell with $a=$ 11.664 (2) A, $c=16.335$ (4) $\AA$ (Smirnov et al., 1987) and $a=$ 16.44 (7) $\AA, c=16.32$ (3) $\AA($ Kemmler-Sack \& Ehmann, 1981) have been reported for $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$. However, details of the crystal structure, including atom positions, have not been clarified up to now. $\mathrm{Sr}_{9} \mathrm{Ln}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ compounds prepared by substituting $\operatorname{Ln}$ (a rare-earth element) for La in $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ have also been reported. These materials have tetragonal symmetry for $L n=\mathrm{La}, \mathrm{Pr}$, and Nd ; cubic (high-temperature phase) and tetragonal (low-temperature phase) symmetry for $\mathrm{Sm}, \mathrm{Eu}$, and Gd; monoclinic symmetry for Tb and Dy ; and cubic symmetry for Ho, Er, Tm, and Y (Kemmler-Sack \& Ehmann, 1981). The Sr atoms of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ can also be replaced with Ca or Ba. For $\mathrm{Ca}_{9} L n_{2}\left(\mathrm{WO}_{6}\right)_{4}(L n=\mathrm{Nd}, \mathrm{Sm}, \mathrm{Eu}$, $\mathrm{Gd}, \mathrm{Tb}, \mathrm{Dy}$ ), lattice parameters of a tetragonal unit-cell with $11.05 \leq a \leq 11.13 \AA$ and $16.37 \leq c \leq 16.42 \AA$ and space group
$I 4_{1} / a$ have been reported (Smirnov et al., 1987). $\mathrm{Ba}_{9} \operatorname{Ln}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ compounds $(L n=\mathrm{La}, \mathrm{Nd}, \mathrm{Sm}, \mathrm{Eu})$ are cubic $(8.50 \leq a \leq$ 8.56 Å; Betz et al., 1982). The crystal structures of $\mathrm{Sr}_{9} \mathrm{Gd}_{2}\left(\mathrm{WO}_{6}\right)_{4}[F m \overline{3}, a=16.47013(6) \AA]$ and $\mathrm{Ba}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ [Fm $\overline{3}, a=17.12339$ (15) Å] have been fully analyzed (Ijdo et al., 2016). However, atomic positions for the tetragonal structures of $\mathrm{Ca}_{9}{L n_{2}\left(\mathrm{WO}_{6}\right)_{4}(L n=\mathrm{Nd}, \mathrm{Sm}, \mathrm{Eu}, \mathrm{Gd}, \mathrm{Tb}, \mathrm{Dy}) ~}_{\text {( }}$ compounds have not been determined.

Here, we report on synthesis and crystal structure analysis of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$.

## 2. Structural commentary

The unit-cell parameters of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ determined in the present investigation are consistent with those reported in previous studies (Smirnov et al., 1987; Kemmler-Sack \& Ehmann, 1981). Fig. 1 displays the principal building units in the crystal structure of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$. W1 (multiplicity and Wyckoff letter $8 d$ with site symmetry $\overline{1}$ ) and W2 $(8 c, \overline{1})$ each are located at the center of a $\left[\mathrm{WO}_{6}\right]$ octahedron. The $\left[\mathrm{WO}_{6}\right]$ octahedra are isolated and surrounded by mixed-occupied (Sr,La) atoms. As detailed in Table 1, the interatomic distances between W and O are 1.901 (4)-1.934 (4) $\AA$ (average: $1.922 \AA$ ) for $\mathrm{W} 1-\mathrm{O}$ and 1.891 (4)-1.967 (4) $\AA$ (average: $1.925 \AA$ ) for $\mathrm{W} 2-\mathrm{O}$. The bond-valence sums (BVS; Brown \& Altermatt, 1985) for W1 and W2, as calculated using the parameters for $\mathrm{W}-\mathrm{O}\left(R_{0}=1.921, B=0.37\right)$ (Brese \& O'Keeffe, 1991), are 5.994 and 5.957 valence units, respectively. These values are consistent with the valence state +VI for W .

The $\mathrm{Sr} / \mathrm{La}$ occupancies for $(\mathrm{Sr} / \mathrm{La}) 1(16 f, 1),(\mathrm{Sr} / \mathrm{La}) 2(16 f$, 1), ( $\mathrm{Sr} / \mathrm{La}$ ) 3 ( $8 e, 2 .$. ), and ( $\mathrm{Sr} / \mathrm{La}) 4$ ( $4 a, \overline{4} .$. ) are $0.6384 /$ 0.3616 (19), 0.8913/0.1087 (18), 0.948/0.052 (4), and 0.985/ 0.015 (7), respectively. The interatomic distances between $(\mathrm{Sr} /$ La ) and O and the coordination numbers of the cations are


Figure 1
The principal building units in the crystal structure of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ with displacement ellipsoids drawn at the $99 \%$ probability level. Symmetry codes refer to Table 1.

Table 1
Selected bond lengths ( $\AA$ ).

| Sr1/La1-O6 ${ }^{\text {i }}$ | 2.333 (4) | Sr3/La3-O1 ${ }^{\text {x }}$ | 3.220 (4) |
| :---: | :---: | :---: | :---: |
| $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 2$ | 2.438 (4) | Sr4/La4-O1 | 2.607 (4) |
| Sr1/La1-O2 ${ }^{\text {ii }}$ | 2.453 (4) | Sr4/La4-O1 ${ }^{\text {vi }}$ | 2.607 (4) |
| $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 4^{\text {iii }}$ | 2.458 (4) | Sr4/La4-O1 ${ }^{\text {xi }}$ | 2.607 (4) |
| Sr1/La $1-\mathrm{O}{ }^{\text {iv }}$ | 2.728 (4) | $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 1^{\text {ix }}$ | 2.607 (4) |
| Sr1/La1-O3 ${ }^{\text {iii }}$ | 2.765 (5) | Sr4/La4-O4 | 2.998 (5) |
| Sr1/La1-O3 | 2.849 (5) | Sr4/La4-O4 ${ }^{\text {xi }}$ | 2.998 (5) |
| $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 1^{\text {iii }}$ | 2.861 (4) | $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4{ }^{\text {ix }}$ | 2.998 (5) |
| Sr2/La $2-\mathrm{O}^{\text {v }}$ | 2.470 (4) | $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4^{\text {vi }}$ | 2.998 (5) |
| $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 1^{\text {vi }}$ | 2.548 (4) | Sr4/La $4-\mathrm{O}^{\text {i }}$ | 3.131 (4) |
| $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 6$ | 2.599 (4) | Sr4/La4-O5 ${ }^{\text {xii }}$ | 3.131 (4) |
| $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 2{ }^{\text {vii }}$ | 2.603 (4) | Sr4/La4-O5 ${ }^{\text {v }}$ | 3.131 (4) |
| Sr2/La2-O1 | 2.642 (4) | Sr4/La4-O5 ${ }^{\text {viii }}$ | 3.131 (4) |
| Sr2/La2-O5 | 2.652 (4) | W1-O3 | 1.901 (4) |
| Sr2/La2-O5 ${ }^{\text {v }}$ | 2.704 (4) | $\mathrm{W} 1-\mathrm{O}{ }^{\text {xiii }}$ | 1.901 (4) |
| Sr2/La2-O4 | 2.777 (4) | $\mathrm{W} 1-\mathrm{O} 6^{\text {viii }}$ | 1.930 (4) |
| Sr2/La $2-\mathrm{O} 4{ }^{\text {v }}$ | 2.877 (5) | $\mathrm{W} 1-\mathrm{O} 6^{\text {xiv }}$ | 1.930 (4) |
| Sr3/La3-O6 ${ }^{\text {i }}$ | 2.557 (4) | W1-O2 | 1.934 (4) |
| Sr3/La3-O6 ${ }^{\text {viii }}$ | 2.557 (4) | $\mathrm{W} 1-\mathrm{O} 2^{\text {xiii }}$ | 1.934 (4) |
| Sr3/La3-O5 ${ }^{\text {viii }}$ | 2.596 (4) | $\mathrm{W} 2-\mathrm{O} 4^{\mathrm{xi}}$ | 1.891 (4) |
| Sr3/La3-O5 ${ }^{\text {i }}$ | 2.596 (4) | W2-O4v | 1.891 (4) |
| Sr3/La3-O3 | 2.660 (4) | $\mathrm{W} 2-\mathrm{O} 1^{\mathrm{xv}}$ | 1.917 (4) |
| $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 3^{\text {ix }}$ | 2.660 (4) | W2-O1 | 1.917 (4) |
| $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 4^{\text {ix }}$ | 2.773 (4) | $\mathrm{W} 2-\mathrm{O} 5^{\mathrm{xi}}$ | 1.967 (4) |
| Sr3/La3-O4 | 2.773 (4) | $\mathrm{W} 2-\mathrm{O} 5^{\text {v }}$ | 1.967 (4) |
| $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 1^{\text {iii }}$ | 3.220 (4) |  |  |
|  |  |  |  |
|  |  |  |  |

2.333 (4)-2.861 (4) A (average: $2.611 \AA$ ) and 8 for (Sr/La) $1-$ O; 2.470 (4)-2.877 (5) A (average: $2.660 \AA$ ) and 8 for ( $\mathrm{Sr} /$ La) 2-O; 2.557 (4)-3.220 (4) $\AA$ (average: $2.761 \AA$ ) and 10 for (Sr/La)3-O; and 2.607 (4)-3.131 (4) A (average: $2.912 \AA$ ) and 12 for $(\mathrm{Sr} / \mathrm{La}) 4-\mathrm{O}$. As the La occupancy increases, the $(\mathrm{Sr} / \mathrm{La})-\mathrm{O}$ interatomic distance decreases.

The crystal structures of alkaline-earth and rare-earth tungstates are often described in relation to the doubleperovskite structure type (Kemmler-Sack \& Ehmann, 1981; Betz et al., 1982; Blasse \& Kemmler-Sack, 1983; King et al., 2010; Ijdo et al., 2016). In the double-perovskite $\left(A_{2} B B^{\prime} \mathrm{O}_{6}\right)$ structure, $B$ and $B^{\prime}$ atoms alternately occupy the $B$ site of the perovskite $\left(A B \mathrm{O}_{3}\right)$ structure. The $B$ site is at the center of an octahedron formed by O atoms, and the vertex-sharing [ $\mathrm{BO}_{6}$ ] and $\left[B^{\prime} \mathrm{O}_{6}\right]$ octahedra regularly align in the $A_{8}$ simple cubic lattice frame in the double-perovskite structure. In case of the structure of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$, a $(\mathrm{Sr} / \mathrm{La}, \square)_{8}$ distorted simple lattice can be derived by connecting the Sr-rich sites of $(\mathrm{Sr} / \mathrm{La}) 2,(\mathrm{Sr} / \mathrm{La}) 3$, and $(\mathrm{Sr} / \mathrm{La}) 4$ and a vacancy site at $(1 / 2,3 / 4$, $1 / 8$ ), as shown in Fig. 2. In the distorted lattice, the [ $\mathrm{WO}_{6}$ ] octahedra and the $\left[(\mathrm{Sr} / \mathrm{La}) 1 \mathrm{O}_{8}\right]$ polyhedra are alternately located by sharing four vertices and two edges of the [( $\mathrm{Sr} /$ $\mathrm{La}) 1 \mathrm{O}_{8}$ ] polyhedra (Fig. 2).

The crystal structure of $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ is isotypic with those of $\mathrm{Sr}_{11}\left(\mathrm{ReO}_{6}\right)_{4}[a=11.6779$ (1), $c=16.1488$ (2); Bramnik et al., 2000], $\mathrm{Ba}_{11}\left(\mathrm{OsO}_{6}\right)_{4}[a=12.2414$ (1), $c=16.6685$ (1); Wakeshima \& Hinatsu, 2005], $\mathrm{La}_{9} \operatorname{Sr}\left(\mathrm{IrO}_{6}\right)_{4}[a=11.5955$ (11), $c=$ 16.2531 (15); Ferreira et al., 2018], and $\mathrm{Sr}_{11}\left(\mathrm{MoO}_{6}\right)_{4}[a=$ 11.6107 (6), $c=16.4219$ (13); Löpez et al., 2016].


Figure 2
[ $\mathrm{WO}_{6}$ ] octahedra and $\left[(\mathrm{Sr} / \mathrm{La}) 1 \mathrm{O}_{8}\right.$ ] polyhedra alternately distributed in the distorted $(\mathrm{Sr} / \mathrm{La} 2-4, \square)_{8}$ lattice as illustrated for the planes parallel to (001) in (a) and (110) in (b). Note that [ $\mathrm{WO}_{6}$ ] octahedra and [ $\left.(\mathrm{Sr} / \mathrm{La}) 1 \mathrm{O}_{8}\right]$ polyhedra are connected to each other by vertex- or edge-sharing.

## 3. Synthesis and crystallization

Raw powdered materials of $\mathrm{SrCO}_{3}$ (Hakushin Chemical Laboratory, $98 \%$ ), $\mathrm{WO}_{3}$ (Furuuchi Chemical, $99.99 \%$ ), and $\mathrm{La}_{2} \mathrm{O}_{3}$ (FUJIFILM Wako Pure Chemical, $99.99 \%$; calcined at 1273 K in advance) were weighed in a Sr:La:W molar ratio of 9:2:4, mixed in an agate mortar, and pressed into a cylindrical pellet with a diameter of 6 mm . The pellet was placed on a Pt plate in an alumina crucible with a lid (Nikkato, SSA-S) and heated to 1473 K at a rate of $300 \mathrm{~K} \mathrm{~h}^{-1}$ in a furnace. This temperature was maintained for 10 h , and the power to the heater of the furnace was then shut off. After the sample had cooled to room temperature, the sintered pellet was crushed, pressed into a pellet, and heated again under the same conditions. This procedure was performed three times. Part of

Table 2
Experimental details.

| Crystal data |  |
| :--- | :--- |
| Chemical formula | $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ |
| $M_{\mathrm{r}}$ | 2185.80 |
| Crystal system, space group | Tetragonal, $I 4_{1} / a$ |
| Temperature (K) | 300 |
| $a, c(\AA)$ | $11.6365(3), 16.3040(4)$ |
| $V\left(\AA^{3}\right)$ | $2207.69(13)$ |
| $Z$ | 4 |
| Radiation type | $\mathrm{Mo} \mathrm{K} \mathrm{\alpha}$ |
| $\mu\left(\mathrm{~mm}^{-1}\right)$ | 46.16 |
| Crystal size (mm) | $0.05 \times 0.04 \times 0.03$ |
|  |  |
| Data collection |  |
| Diffractometer | Bruker D8 QUEST |
| Absorption correction | Multi-scan $(S A D A B S ;$ Krause $e t$ |
|  | al., 2015) |
| $T_{\text {min }}, T_{\text {max }}$ | $0.20,0.33$ |
| No. of measured, independent and | $62981,2106,1972$ |
| $\quad$ observed $[I>2 \sigma(I)]$ reflections |  |
| $R_{\text {int }}$ | 0.048 |
| (sin $\theta / \lambda)_{\text {max }}\left(\AA \AA^{-1}\right)$ | 0.770 |
|  |  |
| Refinement |  |
| $R\left[F^{2}>2 \sigma\left(F^{2}\right)\right], w R\left(F^{2}\right), S$ | $0.025,0.046,1.37$ |
| No. of reflections | 2106 |
| No. of parameters | 97 |
| No. of restraints | 1 |
| $\Delta \rho_{\text {max }}, \Delta \rho_{\text {min }}\left(\mathrm{e} \AA \AA^{-3}\right)$ | $1.14,-1.50$ |

Computer programs: APEX3 and SAINT (Bruker, 2018), SHELXT2014/5 (Sheldrick, 2015a), SHELXL2018/3 (Sheldrick, 2015b), VESTA (Momma \& Izumi, 2011) and publCIF (Westrip, 2010).
the sintered pellet was then placed on a Pt plate in an alumina crucible, heated at 1673 K for 6 h , and cooled to room temperature at a rate of $-400 \mathrm{~K} \mathrm{~h}^{-1}$. The obtained crystalline sample was an aggregate consisting of $\sim 50 \mu \mathrm{~m}$ single-crystalline grains. A single crystal selected from the aggregate was placed on top of a glass fiber for X-ray structure analysis. Another single crystal was embedded in resin, mirror polished, and carbon coated in preparation for chemical analysis using an electron microprobe analyzer (EPMA; JEOL JXA-8200). The chemical composition determined by EPMA was Sr : 23.2 (4), La: 4.8 (1), W: 10.3 (3), and O: 61.7 (5) wt\%. The Sr:La:W:O atomic ratio of 9.1 (1): 1.9 (1): 4.0 (1): 24.0 (2) calculated from the composition is consistent with the chemical formula $\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$.

## 4. Refinement

The results of the crystal structure analysis are summarized in Table 2. An initial structure model with two W sites, four Sr sites, and six O sites using isotropic displacement parameters showed residual electron density distribution around the four Sr sites. These sites were changed to $\mathrm{Sr} / \mathrm{La}$ mixed sites, and their occupancies were refined under consideration of full occupancy, resulting in an Sr:La:W:O atomic ratio of 35.6:8.4:16:96. Given the charge balance, the numbers of Sr and La atoms in the unit cell was constrained to be 36 and 8 , respectively.

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## supporting information

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$\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$ containing $\left[\mathrm{WO}_{6}\right]$ octahedra

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## Computing details

Data collection: APEX3 (Bruker, 2018); cell refinement: SAINT (Bruker, 2018); data reduction: SAINT (Bruker, 2018); program(s) used to solve structure: SHELXT2014/5 (Sheldrick, 2015a); program(s) used to refine structure:
SHELXL2018/3 (Sheldrick, 2015b); molecular graphics: VESTA (Momma \& Izumi, 2011); software used to prepare material for publication: publCIF (Westrip, 2010).

Nonastrontium dilanthanum tetrakis[orthotungstate(VI)]

## Crystal data

$\mathrm{Sr}_{9} \mathrm{La}_{2}\left(\mathrm{WO}_{6}\right)_{4}$
$M_{r}=2185.80$
Tetragonal, $I 4_{1} / a$
$a=11.6365$ (3) $\AA$
$c=16.3040(4) \AA$
$V=2207.69(13) \AA^{3}$
$Z=4$
$F(000)=3776$

## Data collection

Bruker D8 QUEST
diffractometer
Radiation source: sealed X-ray tube
Detector resolution: 7.3910 pixels $\mathrm{mm}^{-1}$
$\omega$ and $\sigma$ cans
Absorption correction: multi-scan
(SADABS; Krause et al., 2015)
$T_{\text {min }}=0.20, T_{\text {max }}=0.33$
$D_{\mathrm{x}}=6.576 \mathrm{Mg} \mathrm{m}^{-3}$
Mo $K \alpha$ radiation, $\lambda=0.71073 \AA$
Cell parameters from 9792 reflections
$\theta=3.5-33.2^{\circ}$
$\mu=46.16 \mathrm{~mm}^{-1}$
$T=300 \mathrm{~K}$
Granular, translucent colourless
$0.05 \times 0.04 \times 0.03 \mathrm{~mm}$

62981 measured reflections
2106 independent reflections
1972 reflections with $I>2 \sigma(I)$
$R_{\text {int }}=0.048$
$\theta_{\text {max }}=33.2^{\circ}, \theta_{\text {min }}=2.2^{\circ}$
$h=-17 \rightarrow 17$
$k=-17 \rightarrow 17$
$l=-25 \rightarrow 25$

## Refinement

Refinement on $F^{2}$
Least-squares matrix: full
$R\left[F^{2}>2 \sigma\left(F^{2}\right)\right]=0.025$
$w R\left(F^{2}\right)=0.046$
$S=1.37$
2106 reflections
97 parameters
1 restraint

```
\(w=1 /\left[\sigma^{2}\left(F_{\mathrm{o}}{ }^{2}\right)+62.4087 P\right]\)
    where \(P=\left(F_{\mathrm{o}}{ }^{2}+2 F_{\mathrm{c}}^{2}\right) / 3\)
\((\Delta / \sigma)_{\text {max }}=0.001\)
\(\Delta \rho_{\text {max }}=1.14 \mathrm{e} \AA^{-3}\)
\(\Delta \rho_{\text {min }}=-1.50 \mathrm{e}^{-3}\)
Extinction correction: SHELXL-2014/7
    (Sheldrick, 2015b),
    \(\mathrm{Fc}^{*}=\mathrm{kFc}\left[1+0.001 \mathrm{xFc}^{2} \lambda^{3} / \sin (2 \theta)\right]^{-1 / 4}\)
Extinction coefficient: 0.000055 (5)
```


# supporting information 

## Special details

Geometry. All esds (except the esd in the dihedral angle between two l.s. planes) are estimated using the full covariance matrix. The cell esds are taken into account individually in the estimation of esds in distances, angles and torsion angles; correlations between esds in cell parameters are only used when they are defined by crystal symmetry. An approximate (isotropic) treatment of cell esds is used for estimating esds involving l.s. planes.

Fractional atomic coordinates and isotropic or equivalent isotropic displacement parameters $\left(\AA^{2}\right)$

|  | $x$ | $y$ | $z$ | $U_{\text {iso }} * / U_{\text {eq }}$ | Occ. ( $<1)$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Sr1 | $0.20878(3)$ | $0.22538(3)$ | $0.53417(2)$ | $0.00769(8)$ | $0.6384(19)$ |
| La1 | $0.20878(3)$ | $0.22538(3)$ | $0.53417(2)$ | $0.00769(8)$ | $0.3616(19)$ |
| Sr2 | $0.23647(4)$ | $0.04341(4)$ | $0.11357(3)$ | $0.00718(9)$ | $0.8913(18)$ |
| La2 | $0.23647(4)$ | $0.04341(4)$ | $0.11357(3)$ | $0.00718(9)$ | $0.1087(18)$ |
| Sr3 | 0.0000 | 0.2500 | $0.36535(4)$ | $0.00934(14)$ | $0.948(4)$ |
| La3 | 0.0000 | 0.2500 | $0.36535(4)$ | $0.00934(14)$ | $0.052(4)$ |
| Sr4 | 0.0000 | 0.2500 | 0.1250 | $0.0267(4)$ | $0.985(7)$ |
| La4 | 0.0000 | 0.2500 | 0.1250 | $0.0267(4)$ | $0.015(7)$ |
| W1 | 0.0000 | 0.0000 | 0.5000 | $0.00522(6)$ |  |
| W2 | 0.0000 | 0.0000 | 0.0000 | $0.00502(6)$ |  |
| O1 | $0.0101(3)$ | $0.0266(3)$ | $0.1158(2)$ | $0.0093(7)$ |  |
| O2 | $0.0795(3)$ | $0.0786(3)$ | $0.5877(2)$ | $0.0099(7)$ |  |
| O3 | $0.1059(4)$ | $0.0651(4)$ | $0.4243(3)$ | $0.0137(8)$ |  |
| O4 | $0.1383(4)$ | $0.1321(4)$ | $0.2554(3)$ | $0.0148(8)$ |  |
| O5 | $0.3675(3)$ | $0.1315(3)$ | $0.2308(2)$ | $0.0109(7)$ |  |
| O6 | $0.4011(3)$ | $0.1285(3)$ | $0.0246(2)$ | $0.0096(7)$ |  |

Atomic displacement parameters $\left(\AA^{2}\right)$

|  | $U^{11}$ | $U^{22}$ | $U^{33}$ | $U^{12}$ | $U^{13}$ | $U^{23}$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Sr1 | $0.00728(15)$ | $0.00640(15)$ | $0.00939(16)$ | $0.00166(12)$ | $-0.00049(12)$ | $0.00060(12)$ |
| La1 | $0.00728(15)$ | $0.00640(15)$ | $0.00939(16)$ | $0.00166(12)$ | $-0.00049(12)$ | $0.00060(12)$ |
| Sr2 | $0.00722(17)$ | $0.00602(17)$ | $0.00830(18)$ | $-0.00036(14)$ | $0.00015(14)$ | $-0.00025(14)$ |
| La2 | $0.00722(17)$ | $0.00602(17)$ | $0.00830(18)$ | $-0.00036(14)$ | $0.00015(14)$ | $-0.00025(14)$ |
| Sr3 | $0.0127(3)$ | $0.0080(3)$ | $0.0074(3)$ | $-0.0024(2)$ | 0.000 | 0.000 |
| La3 | $0.0127(3)$ | $0.0080(3)$ | $0.0074(3)$ | $-0.0024(2)$ | 0.000 | 0.000 |
| Sr4 | $0.0091(3)$ | $0.0091(3)$ | $0.0620(10)$ | 0.000 | 0.000 | 0.000 |
| La4 | $0.0091(3)$ | $0.0091(3)$ | $0.0620(10)$ | 0.000 | 0.000 | 0.000 |
| W1 | $0.00463(11)$ | $0.00540(11)$ | $0.00562(11)$ | $-0.00008(8)$ | $0.00033(8)$ | $0.00085(8)$ |
| W2 | $0.00472(11)$ | $0.00554(11)$ | $0.00480(11)$ | $0.00064(8)$ | $-0.00001(8)$ | $-0.00041(8)$ |
| O1 | $0.0062(14)$ | $0.0135(17)$ | $0.0081(16)$ | $-0.0004(12)$ | $-0.0012(12)$ | $-0.0019(13)$ |
| O2 | $0.0116(16)$ | $0.0106(16)$ | $0.0073(16)$ | $-0.0022(13)$ | $0.0000(13)$ | $-0.0007(13)$ |
| O3 | $0.0128(17)$ | $0.0134(18)$ | $0.0149(19)$ | $0.0023(14)$ | $0.0071(14)$ | $0.0062(14)$ |
| O4 | $0.0184(19)$ | $0.0141(18)$ | $0.0118(18)$ | $-0.0098(15)$ | $0.0025(15)$ | $-0.0006(15)$ |
| O5 | $0.0117(17)$ | $0.0112(17)$ | $0.0098(17)$ | $0.0032(13)$ | $0.0018(13)$ | $0.0006(13)$ |
| O6 | $0.0097(16)$ | $0.0092(16)$ | $0.0098(16)$ | $0.0027(12)$ | $-0.0009(13)$ | $-0.0005(13)$ |

Geometric parameters (A, ${ }^{\circ}$ )

| Sr1/La1-O6 ${ }^{\text {i }}$ | 2.333 (4) | Sr3/La3-O1 ${ }^{\text {xi }}$ | 3.220 (4) |
| :---: | :---: | :---: | :---: |
| Sr1/La1-O2 | 2.438 (4) | Sr3/La3-W2 $2^{\text {xi }}$ | 3.4641 (4) |
| Sr1/La1-O2 ${ }^{\text {ii }}$ | 2.453 (4) | Sr3/La3-W2 $2^{\text {iii }}$ | 3.4641 (4) |
| Sr1/Lal-O4iii | 2.458 (4) | Sr4/La4-O1 | 2.607 (4) |
| Sr1/La1-O5iv | 2.728 (4) | Sr4/La4-O1 ${ }^{\text {vii }}$ | 2.607 (4) |
| Sr1/La1-O3 ${ }^{\text {iii }}$ | 2.765 (5) | Sr4/La4-O1 ${ }^{\text {xii }}$ | 2.607 (4) |
| Sri/La1-O3 | 2.849 (5) | Sr4/La4-O1 ${ }^{\text {x }}$ | 2.607 (4) |
| Sr1/La - O1 ${ }^{\text {iii }}$ | 2.861 (4) | Sr4/La4-O4 | 2.998 (5) |
| Sr1/La1-Sr2/La2 ${ }^{\text {v }}$ | 3.4446 (6) | Sr4/La4-O4xii | 2.998 (5) |
| Sr1/La1-Sr2/La2 ${ }^{\text {v }}$ | 3.4446 (6) | Sr4/La4-O4 ${ }^{\text {x }}$ | 2.998 (5) |
| Sr1/La 1 -W $1^{\text {iii }}$ | 3.5630 (4) | Sr4/La4-O4 ${ }^{\text {vii }}$ | 2.998 (5) |
| Sr1/La1-W1 | 3.6181 (4) | Sr4/La4-O5 ${ }^{\text {i }}$ | 3.131 (4) |
| Sr2/La2-O3 ${ }^{\text {vi }}$ | 2.470 (4) | Sr4/La4-O5xiii | 3.131 (4) |
| Sr2/La2-O1 ${ }^{\text {vii }}$ | 2.548 (4) | $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 5^{\text {vi }}$ | 3.131 (4) |
| Sr2/La2-O6 | 2.599 (4) | Sr4/La4-O5 ${ }^{\text {ix }}$ | 3.131 (4) |
| Sr2/La2-O2 ${ }^{\text {viii }}$ | 2.603 (4) | W1-03 | 1.901 (4) |
| Sr2/La2-O1 | 2.642 (4) | W1-O3 ${ }^{\text {xiv }}$ | 1.901 (4) |
| Sr2/La2-O5 | 2.652 (4) | W1-O6 ${ }^{\text {ix }}$ | 1.930 (4) |
| $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5^{\text {vi }}$ | 2.704 (4) | W1- $\mathrm{O}{ }^{\text {v }}$ | 1.930 (4) |
| Sr2/La2-O4 | 2.777 (4) | W1-O2 | 1.934 (4) |
| Sr2/La2-O4 $4^{\text {vi }}$ | 2.877 (5) | W1-O2 $2^{\text {xiv }}$ | 1.934 (4) |
| Sr2/La2-W2 ${ }^{\text {iii }}$ | 3.2790 (4) | W1-Sr1/La1 ${ }^{\text {xv }}$ | 3.5629 (4) |
| Sr2/La2-W2 | 3.3549 (4) | W1-Sr1/La1 ${ }^{\text {vi }}$ | 3.5629 (4) |
| Sr2/La2-Sr1 ${ }^{\text {viii }}$ | 3.4446 (6) | W1-Sr2/La2 ${ }^{\text {ix }}$ | 3.6177 (4) |
| Sr3/La3-O6 ${ }^{\text {i }}$ | 2.557 (4) | W1-Sr2/La2 ${ }^{\text {v }}$ | 3.6177 (4) |
| Sr3/La3-O6 ${ }^{\text {ix }}$ | 2.557 (4) | W2-O4 ${ }^{\text {xii }}$ | 1.891 (4) |
| Sr3/La3-O5 $5^{\text {ix }}$ | 2.596 (4) | W2-O4 ${ }^{\text {vi }}$ | 1.891 (4) |
| Sr3/La3-O5 ${ }^{\text {i }}$ | 2.596 (4) | W2-O1 ${ }^{\text {xvi }}$ | 1.917 (4) |
| Sr3/La3-O3 | 2.660 (4) | W2-O1 | 1.917 (4) |
| Sr3/La3-O3 ${ }^{\text {x }}$ | 2.660 (4) | W2-O5xii | 1.967 (4) |
| Sr3/La3-O4 ${ }^{\text {x }}$ | 2.773 (4) | W2-O5 ${ }^{\text {vi }}$ | 1.967 (4) |
| Sr3/La3-O4 | 2.773 (4) | W2-Sr2/La2 ${ }^{\text {xii }}$ | 3.2790 (4) |
| Sr3/La3-O1 ${ }^{\text {iii }}$ | 3.220 (4) | W2-Sr2/La2 ${ }^{\text {vi }}$ | 3.2790 (4) |
| O6 ${ }^{\text {i }}$ Sr1/La1-O2 | 108.65 (13) | W2 ${ }^{\text {xi }}$ - $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{W} 2^{\text {iii }}$ | 114.236 (19) |
| O6--Sr1/La1-O2i | 83.84 (13) | O1-Sr4/La4-O1 ${ }^{\text {vii }}$ | 90.189 (10) |
| $\mathrm{O} 2-\mathrm{Sr1} 1 \mathrm{La} 1-\mathrm{O} 2^{\text {ii }}$ | 86.10 (14) | O1-Sr4/La4-O1 ${ }^{\text {xii }}$ | 90.189 (10) |
| O6--Sr1/La1-O44ii | 139.77 (14) | O1 ${ }^{\text {vii }}$-Sr4/La4-O1 $1^{\text {xii }}$ | 173.41 (17) |
| $\mathrm{O} 2-\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 4^{\text {iii }}$ | 101.40 (14) | $\mathrm{O} 1-\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{Ol}^{\text {x }}$ | 173.41 (17) |
| $\mathrm{O} 2{ }^{\text {iii }}-\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 4^{\text {iii }}$ | 125.03 (13) | O1 ${ }^{\text {vii }}$-Sr4/La4-O1 ${ }^{\text {x }}$ | 90.189 (10) |
| $\mathrm{O} 6^{\mathbf{i}}-\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 5^{\text {iv }}$ | 83.02 (13) | O1 ${ }^{\text {xii }}$-Sr4/La4-O1 ${ }^{\text {x }}$ | 90.189 (10) |
| O2-Sr1/La1-O5 ${ }^{\text {iv }}$ | 163.00 (12) | O1-Sr4/La4-O4 | 63.92 (11) |
| $\mathrm{O} 2{ }^{\text {iii }}-\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 5^{\mathrm{iv}}$ | 82.86 (13) | O1 ${ }^{\text {vii }}$-Sr4/La4-O4 | 56.25 (11) |
| O4iii-Sr1/La1-O5 ${ }^{\text {iv }}$ | 74.87 (14) | O1 ${ }^{\text {xii }}$-Sr4/La4-O4 | 118.30 (11) |
| O6 ${ }^{\text {i }}$ - Sr1/La $1-\mathrm{O}^{\text {iii }}$ | 146.51 (13) | $\mathrm{O1}{ }^{\times}-\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4$ | 121.40 (11) |
| $\mathrm{O} 2-\mathrm{Sr1/La} 1-\mathrm{O}^{\text {iii }}$ | 74.94 (12) | O1-Sr4/La4-O4x ${ }^{\text {xii }}$ | 56.25 (11) |


| $\mathrm{O} 2{ }^{\text {ii }}$ - $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 3{ }^{\text {iii }}$ |
| :---: |
| O4 ${ }^{\text {iii }}$-Sr1/La1-O3 ${ }^{\text {iii }}$ |
| O5 ${ }^{\text {iv }}$ - $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 3^{\text {iii }}$ |
| O6 ${ }^{\text {i }}$-Sr1/La1-O3 |
| O2-Sr1/La1-O3 |
| O2 ${ }^{\text {iii- }} \mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 3$ |
| O4 ${ }^{\text {iii }}$-Sr1/La1-O3 |
| O5 ${ }^{\text {iv }}$-Sr1/La1-O3 |
| O3iii-Sr1/La1-O3 |
| O6 ${ }^{\text {i }}$ - $\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 1^{\text {iii }}$ |
| O2-Sr1/La1-O1 ${ }^{\text {iii }}$ |
| $\mathrm{O} 2{ }^{\text {ii }}$ - Sr1/La1-O1 $1^{\text {iii }}$ |
| O4 ${ }^{\text {iii }}-\mathrm{Sr} 1 / \mathrm{La} 1-\mathrm{O} 1^{\text {iii }}$ |
| O5 ${ }^{\text {iv }}$ - Sr1/La1-O1 ${ }^{\text {iii }}$ |
| O3 ${ }^{\text {iii }}$-Sr1/La1-O1 ${ }^{\text {iii }}$ |
| O3-Sr1/La1-O1 ${ }^{\text {iii }}$ |
| Sr2/La2 ${ }^{\text {v }}$-Sr1/La1- |
| W1 ${ }^{\text {iii }}$-Sr1/La1-W1 |
| $\mathrm{O} 3{ }^{\text {vi }}-\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 1^{\text {vii }}$ |
| O3 ${ }^{\text {vi }}$-Sr2/La2-O6 |
| O1 ${ }^{\text {vii- }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 6$ |
| $\mathrm{O} 3{ }^{\text {vi }}-\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 2^{\text {viii }}$ |
| $\mathrm{O} 1{ }^{\text {vii }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 2{ }^{\text {viii }}$ |
| O6-Sr2/La2-O2 ${ }^{\text {viii }}$ |
| O3 ${ }^{\text {vi }}$-Sr2/La2-O1 |
| O1 ${ }^{\text {vii }}$ - $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 1$ |
| O6-Sr2/La2-O1 |
| $\mathrm{O} 2{ }^{\text {viii- }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 1$ |
| O3 ${ }^{\text {vi}}-\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5$ |
| O1 ${ }^{\text {vii- }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5$ |
| O6-Sr2/La2-O5 |
| O2 ${ }^{\text {viii }}$-Sr2/La2-O5 |
| O1—Sr2/La2-O5 |
| O3 ${ }^{\text {vii }}$ - $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5^{\text {vi }}$ |
| $\mathrm{O1}^{\text {vii }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5^{\text {vi }}$ |
| O6-Sr2/La2-O5 ${ }^{\text {vi }}$ |
| $\mathrm{O} 2{ }^{\text {viii }}$ - $\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5^{\text {vi }}$ |
| $\mathrm{O} 1-\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 5^{\text {vi }}$ |
| O5-Sr2/La2-O5 ${ }^{\text {vi }}$ |
| O3 ${ }^{\text {vi }}$-Sr2/La2-O4 |
| $\mathrm{O} 1^{\text {vii }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 4$ |
| O6-Sr2/La2-O4 |
| $\mathrm{O} 2{ }^{\text {viii }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 4$ |
| O1-Sr2/La2-O4 |
| O5-Sr2/La2-O4 |
| O5 ${ }^{\text {vi- }}$ Sr2/La2-O4 |
| $\mathrm{O} 3^{\text {vi }}-\mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 4{ }^{\text {vi }}$ |
| $\mathrm{O} 1^{\text {vii }} \mathrm{Sr} 2 / \mathrm{La} 2-\mathrm{O} 4^{\text {vi }}$ |

62.93 (12)
66.83 (13)
88.51 (12)
89.34 (13)
60.49 (12)
141.63 (12)
82.66 (13)
133.77 (12)
118.90 (13)
73.37 (12)
123.73 (12)
146.75 (12)
67.80 (12)
70.80 (11)
133.60 (11)
63.35 (11)
61.565 (10)
107.502 (10)
143.76 (14)
137.69 (13)
74.95 (12)
77.47 (13)
127.58 (12)
60.75 (12)
71.74 (13)
90.70 (17)
140.44 (12)
141.44 (12)
101.06 (13)
63.69 (12)
80.29 (12)
81.63 (12)
126.30 (12)
118.64 (12)
76.11 (12)
78.82 (12)
117.51 (12)
61.87 (12)
138.23 (9)
83.96 (13)
59.86 (12)
128.74 (12)
132.50 (13)
66.80 (12)
59.51 (12)
109.81 (13)
64.87 (13)
132.31 (11)

| O1 ${ }^{\text {vii }}$-Sr4/La4-O4 $4^{\text {xii }}$ | 121.40 (11) |
| :---: | :---: |
| O1 ${ }^{\text {xii }}$-Sr4/La4-O4 ${ }^{\text {xii }}$ | 63.92 (11) |
| O1 ${ }^{\text {x }}$-Sr4/La4-O4 $4^{\text {xii }}$ | 118.30 (11) |
| O4-Sr4/La4-O4 ${ }^{\text {xii }}$ | 120.17 (10) |
| O1—Sr4/La4-O4 ${ }^{\text {x }}$ | 121.40 (11) |
| $\mathrm{O} 1^{\text {vii }} \mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4^{\text {x }}$ | 118.30 (11) |
| $\mathrm{O} 1^{\text {xii }}-\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4^{\text {x }}$ | 56.25 (11) |
| O1 ${ }^{\text {x }}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4^{\text {x }}$ | 63.92 (11) |
| O4-Sr4/La4-O4 ${ }^{\text {x }}$ | 89.71 (17) |
| O4 ${ }^{\text {xii }}$-Sr4/La4-O4 ${ }^{\text {x }}$ | 120.17 (10) |
| O1—Sr4/La4-O4 ${ }^{\text {vii }}$ | 118.30 (11) |
| O1 ${ }^{\text {vii }}$-Sr4/La4-O4 $4^{\text {vii }}$ | 63.92 (11) |
| O1 $1^{\text {xii }}$-Sr4/La4-O4 ${ }^{\text {vii }}$ | 121.40 (11) |
| $\mathrm{O} 1^{\mathrm{x}}-\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 4^{\text {vii }}$ | 56.25 (11) |
| O4-Sr4/La4-O4 ${ }^{\text {vii }}$ | 120.17 (10) |
| O4 ${ }^{\text {xii }}$-Sr4/La4-O4 ${ }^{\text {vii }}$ | 89.71 (17) |
| $\mathrm{O} 4{ }^{\mathrm{x}}$ - Sr4/La4-O4 $4^{\text {vii }}$ | 120.17 (10) |
| O1—Sr4/La4-O5 ${ }^{\text {i }}$ | 117.41 (11) |
| O1 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {i }}$ | 56.35 (11) |
| O1 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {i }}$ | 117.90 (11) |
| O1 ${ }^{\text {x }}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{OF}^{\text {i }}$ | 68.03 (11) |
| O4-Sr4/La4-O5 ${ }^{\text {i }}$ | 53.49 (10) |
| O4 ${ }^{\text {xii }}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O}^{\text {i }}$ | 173.65 (10) |
| $\mathrm{O} 4{ }^{\mathrm{x}}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O}^{\text {i }}$ | 62.02 (10) |
| O4 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {i }}$ | 94.03 (11) |
| O1-Sr4/La4-O5xiii | 117.90 (11) |
| O1 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {xiii }}$ | 117.41 (11) |
| O1 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {xiii }}$ | 68.03 (11) |
| O1 ${ }^{\text {x }}$ - Sr4/La4-O5xiii | 56.35 (11) |
| O4-Sr4/La4-O5 ${ }^{\text {xiii }}$ | 173.65 (10) |
| O4 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {xiii }}$ | 62.02 (10) |
| O4 ${ }^{\text {x }}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 5^{\text {xiii }}$ | 94.03 (11) |
| O4 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {xiii }}$ | 53.49 (10) |
| O5- ${ }^{\text {i }}$ - $4 / \mathrm{La} 4-\mathrm{O} 5^{\text {xiii }}$ | 124.29 (9) |
| O1-Sr4/La4-O5 ${ }^{\text {vi }}$ | 56.35 (11) |
| O1 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 68.03 (11) |
| O1 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 117.41 (11) |
| O1 ${ }^{\text {x }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 117.90 (11) |
| O4-Sr4/La4-O5 ${ }^{\text {vi }}$ | 94.03 (11) |
| O4 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 53.49 (10) |
| $\mathrm{O} 4 \times-\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O} 5^{\text {vi }}$ | 173.65 (10) |
| O4 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 62.02 (10) |
| O5 ${ }^{\text {i }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 124.29 (9) |
| O5 ${ }^{\text {xiii }}$-Sr4/La4-O5 ${ }^{\text {vi }}$ | 82.71 (14) |
| O1—Sr4/La4-O5 ${ }^{\text {ix }}$ | 68.03 (11) |
| O1 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 117.90 (11) |
| O1 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 56.35 (11) |
| O1 ${ }^{\text {x }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 117.41 (11) |


104.51 (12)
87.33 (12)
58.90 (11)
163.87 (12)
57.69 (11)
123.12 (9)
121.613 (13)
155.754 (16)
78.905 (11)
90.91 (18)
169.96 (12)
82.12 (12)
82.12 (12)
169.96 (12)
105.66 (18)
89.14 (13)
60.52 (12)
93.66 (13)
111.89 (12)
60.52 (12)
89.14 (13)
111.89 (12)
93.66 (13)
137.62 (19)
116.21 (12)
117.76 (12)
61.78 (12)
72.02 (12)
154.56 (13)
64.19 (13)
117.76 (12)
116.21 (12)
72.02 (12)
61.78 (12)
64.19 (13)
154.56 (13)
99.40 (19)
64.45 (11)
115.34 (11)
125.14 (11)
55.05 (11)
60.43 (11)
119.46 (11)
126.84 (11)
53.37 (11)
115.34 (11)
64.45 (11)
55.05 (11)

| O4-Sr4/La4-O5 ${ }^{\text {ix }}$ | 62.02 (10) |
| :---: | :---: |
| O4 ${ }^{\text {xii }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 94.03 (11) |
| O4 ${ }^{\text {x }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 53.49 (10) |
| O4 ${ }^{\text {vii }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 173.65 (10) |
| O5i-Sr4/La4-O5 ${ }^{\text {ix }}$ | 82.71 (14) |
| O5 ${ }^{\text {xiii }}$-Sr4/La4-O5 ${ }^{\text {ix }}$ | 124.29 (9) |
| O5 ${ }^{\text {vi}}$ - $\mathrm{Sr} 4 / \mathrm{La} 4-\mathrm{O}^{\text {ix }}$ | 124.29 (9) |
| O3-W1-O3 ${ }^{\text {xiv }}$ | 180.0 |
| $\mathrm{O} 3-\mathrm{W} 1-\mathrm{O} 6^{\text {ix }}$ | 86.73 (17) |
| $\mathrm{O} 3^{\text {xiv }}-\mathrm{W} 1-\mathrm{O} 6^{\text {ix }}$ | 93.27 (17) |
| $\mathrm{O} 3-\mathrm{W} 1-\mathrm{O}^{\text {v }}$ | 93.27 (17) |
| $\mathrm{O} 3{ }^{\text {xiv }}-\mathrm{W} 1-\mathrm{O}^{\text {v }}$ | 86.73 (17) |
| $\mathrm{O} 6^{\mathrm{ix}}-\mathrm{W} 1-\mathrm{O}^{\mathrm{v}}$ | 180.0 (2) |
| $\mathrm{O} 3-\mathrm{W} 1-\mathrm{O} 2$ | 88.94 (18) |
| $\mathrm{O} 3{ }^{\text {xiv }}-\mathrm{W} 1-\mathrm{O} 2$ | 91.06 (18) |
| O6 ${ }^{\text {ix }}-\mathrm{W} 1-\mathrm{O} 2$ | 94.18 (16) |
| O6 ${ }^{\text {v }}$-W1-O2 | 85.82 (16) |
| $\mathrm{O} 3-\mathrm{W} 1-\mathrm{O} 2^{\text {xiv }}$ | 91.07 (18) |
| $\mathrm{O} 3{ }^{\text {xiv }}-\mathrm{W} 1-\mathrm{O} 2{ }^{\text {xiv }}$ | 88.93 (18) |
| $\mathrm{O} 6^{\mathrm{ix}}-\mathrm{W} 1-\mathrm{O} 2^{\text {xiv }}$ | 85.82 (16) |
| $\mathrm{O} 6^{\mathrm{v}}-\mathrm{W} 1-\mathrm{O} 2{ }^{\text {xiv }}$ | 94.18 (16) |
| $\mathrm{O} 2-\mathrm{W} 1-\mathrm{O} 2^{\text {xiv }}$ | 180.0 |
| $\mathrm{Sr} 1 / \mathrm{La} 1^{\mathrm{xv}}-\mathrm{W} 1-\mathrm{Sr} 1 / \mathrm{La} 1^{\text {vi }}$ | 180.0 |
| Sr1/La1 ${ }^{\text {vi }}$-W1—Sr1/La1 ${ }^{\text {vi }}$ | 0.0 |
| Sr1/La1 ${ }^{\text {xv }}-\mathrm{W} 1-\mathrm{Sr} 1 / \mathrm{La} 1^{\text {xv }}$ | 0.0 |
| Sr1/La1 ${ }^{\text {vi }}$-W 1 - Sr $1 / \mathrm{La}^{\text {xv }}$ | 180.0 |
| $\mathrm{Sr} 1 / \mathrm{La} 1^{\mathrm{xv}}-\mathrm{W} 1-\mathrm{Sr} 2 / \mathrm{La} 2^{\text {ix }}$ | 114.745 (9) |
| Sr1/La1 ${ }^{\text {vi }}$-W1—Sr2/La2 ${ }^{\text {ix }}$ | 65.255 (9) |
| $\mathrm{Sr} 1 / \mathrm{La} 1^{\mathrm{xv}}-\mathrm{W} 1-\mathrm{Sr} 2 / \mathrm{La} 2^{\text {ix }}$ | 114.745 (9) |
| Sr1/La1 ${ }^{\text {xv }}-\mathrm{W} 1-\mathrm{Sr} 2 / \mathrm{La} 2^{v}$ | 65.255 (9) |
| Sr1/La1 ${ }^{\text {vi }}$-W1-Sr2/La2 ${ }^{\text {v }}$ | 114.745 (9) |
| $\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {ix }}-\mathrm{W} 1-\mathrm{Sr} 2 / \mathrm{La} 2^{\text {v }}$ | 180.000 (12) |
| O4 ${ }^{\text {xii }}-\mathrm{W} 2-\mathrm{O} 4^{\text {vi }}$ | 180.0 (3) |
| $\mathrm{O} 4{ }^{\text {xii }}-\mathrm{W} 2-\mathrm{O} 1^{\mathrm{xvi}}$ | 91.21 (17) |
| $\mathrm{O} 4{ }^{\text {vi }}-\mathrm{W} 2-\mathrm{O} 1^{\text {xvi }}$ | 88.79 (17) |
| O4 ${ }^{\text {xii }}$-W2-O1 | 88.80 (17) |
| $\mathrm{O} 4{ }^{\text {vi }}-\mathrm{W} 2-\mathrm{O} 1$ | 91.20 (17) |
| $\mathrm{O} 1^{\text {xvi }}$-W2-O1 | 180.0 |
| $\mathrm{O} 4{ }^{\text {xii }}-\mathrm{W} 2-\mathrm{O} 5^{\text {xii }}$ | 88.65 (18) |
| $\mathrm{O} 4{ }^{\text {vi}}-\mathrm{W} 2-\mathrm{O} 5^{\text {xii }}$ | 91.35 (18) |
| $\mathrm{O} 1{ }^{\text {xvi }}-\mathrm{W} 2-\mathrm{O} 5^{\text {xii }}$ | 90.08 (16) |
| O1-W2-O5 ${ }^{\text {xii }}$ | 89.92 (16) |
| $\mathrm{O} 4{ }^{\text {xii }}-\mathrm{W} 2-\mathrm{O} 5^{\text {vi }}$ | 91.35 (18) |
| $\mathrm{O} 4{ }^{\mathrm{vi}}-\mathrm{W} 2-\mathrm{O} 5^{\mathrm{vi}}$ | 88.65 (18) |
| $\mathrm{O} 1^{\text {xvi }}-\mathrm{W} 2-\mathrm{O} 5^{\text {vi }}$ | 89.92 (16) |
| O1-W2-O5 ${ }^{\text {vi }}$ | 90.08 (16) |
| $\mathrm{O} 5^{\text {xii }}-\mathrm{W} 2-\mathrm{O} 5^{\text {vi }}$ | 180.0 (3) |
| $\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {xii }}-\mathrm{W} 2-\mathrm{Sr} 2 / \mathrm{La} 2^{\text {vi }}$ | 180.0 |

## supporting information

| O5 ${ }^{\text {i }}$ - $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 1^{\text {xi }}$ | 125.14 (11) | $\mathrm{Sr} 2 / \mathrm{La} 2^{\text {xii }}-\mathrm{W} 2-\mathrm{Sr} 2 / \mathrm{La} 2^{\text {xii }}$ | 0.0 |
| :---: | :---: | :---: | :---: |
| O3-Sr3/La3-O1 ${ }^{\text {xi }}$ | 119.46 (11) | $\mathrm{Sr} 2 / \mathrm{La} 2^{\text {vi }}$-W2— $\mathrm{Sr} 2 / \mathrm{La} 2^{\text {xii }}$ | 180.00 (2) |
| O3 ${ }^{\text {x }}$ - Sr3/La3-O1 ${ }^{\text {xi }}$ | 60.43 (11) | $\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {vi }}-\mathrm{W} 2-\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {vi }}$ | 0.000 (11) |
| $\mathrm{O} 4{ }^{\text {x }} \mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O}^{\text {xi }}$ | 53.37 (11) | $\mathrm{Sr} 2 / \mathrm{La} 2^{\text {xii }}$-W2—Sr2/La2 | 102.7 |
| $\mathrm{O} 4-\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 1^{\text {xi }}$ | 126.84 (11) | $\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {vi }}$-W2-Sr2/La2 | 77.309 (8) |
| $\mathrm{O} 1^{\text {iii }}$ - $\mathrm{Sr} 3 / \mathrm{La} 3-\mathrm{O} 1^{\text {xi }}$ | 179.73 (14) | $\mathrm{Sr} 2 / \mathrm{La} 2{ }^{\text {xii }}$-W2-Sr2/La2 | 102.691 (8) |

Symmetry codes: (i) $-x+1 / 2,-y+1 / 2,-z+1 / 2$; (ii) $-y+1 / 4, x+1 / 4,-z+5 / 4$; (iii) $y+1 / 4,-x+1 / 4, z+1 / 4$; (iv) $y+1 / 4,-x+3 / 4,-z+3 / 4$; (v) $-x+1 / 2,-y, z+1 / 2$; (vi) $-y+1 / 4, x-1 / 4, z-1 / 4$; (vii) $-y+1 / 4, x+1 / 4,-z+1 / 4$; (viii) $-x+1 / 2,-y, z-1 / 2$; (ix) $x-1 / 2, y,-z+1 / 2$; (x) $-x,-y+1 / 2, z$; (xi) $-y-1 / 4, x+1 / 4, z+1 / 4$; (xii) $y-1 / 4,-x+1 / 4,-z+1 / 4$; (xiii) $y-1 / 4,-x+3 / 4, z-1 / 4$; (xiv) $-x,-y,-z+1$; (xv) $y-1 / 4,-x+1 / 4,-z+5 / 4$; (xvi) $-x,-y,-z$.

